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Additional Information

1 Two conformal projections for constant-height surface to plane mapping

2

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9

10 **Abstract.** Regions at high elevations may require specific mapping solutions other than the
11 conventional ellipsoid-to-grid projections which produce high discrepancies between ground and
12 projected distances. These particular solutions are known as low-distortion projections (LDPs).
13 They can be realized by making use of an Elevated Ellipsoid (EE) or a Constant-height Surface
14 (ChS) above the ellipsoid as the reference surface, or by means of a scaled projection. No
15 conformal projections have been derived so far for the ChS-to-plane transformation. This article
16 aims to solve this situation by deriving the formulation of Direct and Transverse Mercator-type
17 projections for ChS-to-plane conformal mapping.

18

19 **Author keywords:** Map projections; conformality; distortion; Low-distortion projections (LDPs);
20 constant-height surface.

21

22 **Introduction**

23 The design of map projections and the choice of corresponding parameters (e.g. true scale
24 parallels) are usually made to produce minimum distortions in the reference ellipsoid to plane
25 transformation for an area of interest. A preliminary computation has to be done before

26 projection in order to *reduce* or project the measurements, which are taken close to the earth
27 surface, onto the reference ellipsoid. This reduction process can take the form of a simple and
28 handy ground-to-ellipsoid scale factor. It is normally assumed that the earth surface and the
29 reference ellipsoid are relatively close to each other so that the requirement of low distortions in
30 the ellipsoid-to-plane transformation entails low distortions for the complete ground-to-plane
31 transformation. These distortions can be known and taken into account by the user in each
32 particular case, but the question is whether a particular projection which is optimal in terms of
33 ellipsoid-to-plane transformation can be considered optimal for the complete ground-to-plane
34 transformation or, on the contrary, be significantly improved for this latter purpose. This seems
35 to be the case of highly elevated regions, for which specific solutions, known as low-distortion
36 projections (LDPs) have been derived in the past (Billings 2013a, 2013b, Armstrong *et al.* 2017,
37 Dennis 2018, 2019).

38

39 The distance between two points reduced to the ellipsoid, which will be subsequently projected
40 onto the plane, is a clearly defined magnitude that is measured along the geodesic line passing
41 through both endpoints. Conversely, at a certain height, above or below the ellipsoid, the notion
42 of horizontal distance becomes ambiguous: *horizontal distance* may mean the distance
43 projected onto the local geodetic horizon of the first point, or the horizon of the second point, or
44 be defined for a sort of average height, or with an alternative definition. This type of ambiguity
45 can cause some confusion when using LDPs. To overcome this, an *elevated ellipsoid* (EE) of
46 semi-axes

$$47 \quad a' = a + h_0 \quad (1)$$

$$48 \quad b' = b + h_0 \quad (2)$$

49 can be used, where a and b are the semi-axes of the original reference ellipsoid and h_0 is the
50 desired elevation (Rollins and Meyer 2019). Alternatively, a scale factor can be applied to
51 semi-axis a while retaining the same eccentricity for the ellipsoid. This approach was already

52 used in the three Michigan zones of the State Plane Coordinate System of 1927 (Coast &
53 Geodetic Survey 1979; Burkholder 1980; Lusch 2005, Dennis 2018). These ideas have been
54 presented in other many different occasions (e.g. Burkholder 1993, Armstrong *et al.* 2017,
55 Rollins and Meyer 2019). However, some may find it difficult to use them: as an example, the
56 original implementation of the Wisconsin Coordinate Reference System (Wisconsin State
57 Cartographer's Office 2015) used an enlarged and elevated ellipsoid but was later replaced by
58 the approach of changing the projection scale only. This example may indicate that the strategy
59 of scaling the projection with no change in the reference ellipsoid is preferred at present since it
60 does not entail any increase of complexity, as with the EE and the Constant-height Surface
61 (ChS), while having a similar performance.

62

63 By contrast, Rollins and Meyer (2019) sustain that a ChS is a suitable elevated reference
64 surface for constructing LDPs in places at high elevations, while taking into account that the
65 LDP design should also consider the total linear distortion and not only height. Field distances
66 can be reduced to a ChS by using an adaptation of the widely used scale factor formula
67 $(1+h/R)^{-1}$ (Stem 1990) as $(1+(h-h_0)/R)^{-1}$ with h the mean ellipsoidal height of the endpoints, h_0
68 the ellipsoidal height of the ChS and R the mean of the radii of curvature in both points for the
69 particular direction. Being more specific, we will use R as the average of the Euler's radius of
70 curvature in both endpoints for the corresponding geodetic azimuths, although the result does
71 not depend strongly on the definition chosen for R .

72

73 A ChS is not an ellipsoid. No mapping from the reference ellipsoid to the grid, whether that
74 mapping is conformal or not, can be conformal if used to map from a ChS to the grid but only
75 *nearly conformal*, as shown in Rollins and Meyer (2019), since the curvatures on the ChS
76 cannot equal those on the ellipsoid in general. Indeed, this is true not only for ChSs but for all
77 models other than the reference ellipsoid, including EEs, gravitational equipotential surfaces,

78 planes, etc., since the curvatures of these surfaces differ from those of the reference ellipsoid.
79 As Rollins and Meyer (2019) say, there still could be a conformal direct mapping (ChS →
80 plane), which has not been presented so far.

81

82 The present paper overcomes this situation by presenting:

- 83 • A Direct Mercator-type conformal projection (for use in very low-latitude areas)
- 84 • A Transverse Mercator-type conformal projection (for general use except near the poles)

85

86

87 **Constant-height Surface to grid conformal projections**

88 A ChS is not an ellipsoid (neither the original ellipsoid to a scale different from 1 nor the
89 elevated ellipsoid referred to before) but a different closed surface that is constructed by
90 prolonging the normals at every point of the ellipsoid a distance h_0 . The radii of curvature of the
91 normal sections in the north-south direction and east-west directions are, respectively (Rollins
92 and Meyer, 2019)

$$93 \quad \rho' = \rho + h_0 \quad (3)$$

$$94 \quad \nu' = \nu + h_0 \quad (4)$$

95 where ρ and ν are the principal radii of curvature of the original reference ellipsoid, which are
96 given, respectively, by

$$97 \quad \rho = \frac{a(1-e^2)}{(1-e^2\sin^2\varphi)^{3/2}} \quad (5)$$

$$98 \quad \nu = \frac{a}{\sqrt{1-e^2\sin^2\varphi}} \quad (6)$$

99 with major semi-axis a , eccentricity e and geodetic latitude of the point φ .

100

101 We derive in the following subsections two conformal Mercator-type projections for ChS-to-
 102 plane mapping by elaborating on the original ideas that led to the formulae of
 103 Direct and Transverse Mercator-type projections of the reference ellipsoid.

104

105 ***Direct Mercator-type conformal projection for ChS to plane***

106 The Direct Mercator projection for the transformation (ellipsoid \rightarrow plane) is obtained by

107
$$x = a\Delta\lambda \tag{7}$$

108
$$y = a\psi \tag{8}$$

109 where a is the major semi-axis of the ellipsoid, $\Delta\lambda$ is the increment of geodetic longitude with
 110 respect to the origin of longitudes (i.e. $\Delta\lambda = \lambda - \lambda_0$ where λ is the point longitude and λ_0 is the
 111 central meridian longitude) and ψ is the isometric latitude, also called Mercator parameter
 112 (Osborne, 2013, p.111 Eq. 6.1), which can be defined as

113
$$\psi = \int_0^\varphi \frac{\rho}{\nu \cos\varphi} d\varphi \tag{9}$$

114 For the case of the ellipsoid the integral results in

115
$$\psi = \ln \left| \tan \left(\frac{\pi}{4} + \frac{\varphi}{2} \right) \left(\frac{1 - e \sin\varphi}{1 + e \sin\varphi} \right)^{e/2} \right| \tag{10}$$

116 with e the eccentricity of the ellipsoid and φ the geodetic latitude.

117 Now we apply this idea to construct a conformal projection for the transformation (ChS \rightarrow
 118 plane). Using primed symbols for the ChS and unprimed for the reference ellipsoid, we obtain,
 119 analogously to Eq. (9)

120
$$\psi' = \int_0^\varphi \frac{\rho'}{\nu \cos\varphi} d\varphi \tag{11}$$

121 or considering Eqs. (3) and (4)

122
$$\psi' = \int_0^\varphi \frac{\rho + h_0}{(\nu + h_0) \cos\varphi} d\varphi \tag{12}$$

123 with the expressions for ρ and ν given in Eqs. (5) and (6).

124 It is convenient to introduce the following change of variable

125
$$e_2 = \frac{e^2}{1 + \frac{h_0}{a}} \quad (13)$$

126 which will simplify to e^2 for the case of zero elevation.

127 Although a solution in closed form can be found for the integral in Eq.(12), it is handier to use
 128 the following expression obtained after expanding ψ' in powers of e_2

129
$$\psi' = \ln \left| \frac{\cos \frac{\varphi}{2} + \sin \frac{\varphi}{2}}{\cos \frac{\varphi}{2} - \sin \frac{\varphi}{2}} \right| - e_2 \sin \varphi - \left(\frac{1}{3} + \frac{1}{2} \frac{h_0}{a} \right) e_2^2 \sin^3 \varphi - \left(\frac{1}{5} + \frac{21}{40} \frac{h_0}{a} \right) e_2^3 \sin^5 \varphi - \frac{1}{7} e_2^4 \sin^7 \varphi \quad (14)$$

130 where the terms amounting to less than 0.00001" for latitudes up to 80° and heights up to
 131 4000m have been disregarded.

132 The Direct Mercator (conformal) projection for the transformation (ChS → plane) is then given
 133 by the formulation

134
$$x = a \Delta \lambda \quad (15)$$

135
$$y = a \psi' \quad (16)$$

136 with ψ' given in Eq. (14). If desired, a scale coefficient k_0 could be applied at the equator. To do
 137 so Eqs. (15) and Eq. (16) need be multiplied by k_0 . Not including k_0 in the formulas (i.e. $k_0 = 1$)
 138 means the projection has unit linear scale factor at the Equator.

139 An algorithm for the inverse computation of geodetic coordinates from grid coordinates can be
 140 found in the Appendix.

141

142 This projection is conformal, therefore its linear distortion is the same in every direction from a
 143 point. We can do an easy check of conformality by computing the linear distortions in the
 144 meridian and the parallel for different values of the latitude φ and height h_0 . The results depicted
 145 in Table 1 have been obtained by the corresponding expressions Eqs. (45) and (46) given in the
 146 Appendix (though the latter is the recommended expression due to its simplicity). We only find
 147 negligible discrepancies, i.e. close to the machine working precision for low latitudes and still
 148 negligible for mid or high latitudes. It must be noted, however, that this projection is only of

149 practical use within a very narrow bound near the equator (advisably below 2° of latitude at the
 150 most) due to the very large distortions introduced. For general use, except very near the poles,
 151 a suitable projection is introduced in the following section.

152

153 *Table 1 here*

154

155

156 ***Transverse Mercator-type conformal projection for ChS to plane***

157 For constructing the Transverse Mercator projection we initially resort to the idea that is
 158 generally used for the derivation of the formulae for the ellipsoid-to-plane transformation (see
 159 e.g. Osborne, 2013) now applied to the ChS-to-plane transformation. Let f' be a complex
 160 function mapping the complex plane $(\psi', \Delta\lambda)$ onto the complex plane (y,x)

161
$$y + ix = f'(\psi' + i\Delta\lambda) =$$
 162
$$= f'(\psi') + i\Delta\lambda f'^{(1)}(\psi') - \frac{\Delta\lambda^2}{2} f'^{(2)}(\psi') - i\frac{\Delta\lambda^3}{6} f'^{(3)}(\psi') + \frac{\Delta\lambda^4}{24} f'^{(4)}(\psi') + i\frac{\Delta\lambda^5}{120} f'^{(5)}(\psi') - \frac{\Delta\lambda^6}{720} f'^{(6)}(\psi') +$$
 163
$$\dots \tag{17}$$

164 where we have used the expansion around the central meridian, i.e. $(\psi' + i0)$ or simply written
 165 ψ' , so that $f'^{(n)}(\psi')$ denotes the n th derivative of f' evaluated at ψ' . If function f' and its derivatives
 166 $f'^{(n)}$ exist and are nonzero then the resulting transformation will be conformal.

167 Equating real and imaginary parts on both sides of Eq. (17) we obtain

168
$$x = \Delta\lambda f'^{(1)}(\psi') - \frac{\Delta\lambda^3}{6} f'^{(3)}(\psi') + \frac{\Delta\lambda^5}{120} f'^{(5)}(\psi') + \dots \tag{18}$$

169
$$y = f'(\psi') - \frac{\Delta\lambda^2}{2} f'^{(2)}(\psi') + \frac{\Delta\lambda^4}{24} f'^{(4)}(\psi') - \frac{\Delta\lambda^6}{720} f'^{(6)}(\psi') + \dots \tag{19}$$

170 Now we apply the condition that the central meridian ($\Delta\lambda = 0$, therefore $x = 0$ $y = f'(\psi')$) be a
 171 line of scale coefficient k_0

172
$$y = f'(\psi') = k_0 \int_0^\varphi \rho' d\varphi \tag{20}$$

173 This has the effect of univocally defining function f' . Substituting Eq. (3) into Eq. (20) yields

$$174 \quad f'(\psi') = k_0 \int_0^\varphi (\rho + h_0) d\varphi = k_0 \int_0^\varphi \rho d\varphi + k_0 h_0 \varphi \quad (21)$$

175 The first term in the right-hand side is k_0 times the length of meridian arc from the equator to
176 latitude φ on the reference ellipsoid, which is called $m(\varphi)$ in Osborne (2013), so that

$$177 \quad f'(\psi') = k_0 m(\varphi) + k_0 h_0 \varphi \quad (22)$$

178 in contrast with

$$179 \quad f(\psi) = k_0 m(\varphi) \quad (23)$$

180 which is the function f used in the Transverse Mercator for ellipsoid-to-plane transformation.

181 Hence

$$182 \quad f'(\psi') = f(\psi) + k_0 h_0 \varphi \quad (24)$$

183 Now we compute the corresponding derivatives of function f' given by Eq. (24).

$$184 \quad f'^{(1)}(\psi') = \frac{df'(\psi')}{d\psi'} = \frac{df'(\psi')}{d\psi} \frac{d\psi}{d\psi'} = \left(\frac{df(\psi)}{d\psi} + k_0 h_0 \frac{d\varphi}{d\psi} \right) \frac{d\psi}{d\psi'} \quad (25)$$

185 The first term inside the right-hand side parenthesis is the first derivative of the function f with
186 respect to variable ψ which is used in the standard Transverse Mercator for ellipsoid-to-plane
187 transformation, i.e. $f^{(1)}(\psi)$, and

$$188 \quad \frac{d\varphi}{d\psi} = \frac{\nu \cos \varphi}{\rho} \quad (26)$$

189 as it can be derived from Eq. (9). It can be demonstrated that no significant error is committed if

190 we take $\frac{d\psi}{d\psi'}$ as unity given that we will multiply these derivatives by increments of longitude

191 much smaller than one ($\Delta\lambda \ll 1 \approx 57.2957795^\circ$). Therefore

$$192 \quad f'^{(1)}(\psi') = f^{(1)}(\psi) + k_0 h_0 \frac{\nu \cos \varphi}{\rho} \quad (27)$$

193 For computing subsequent derivatives we can take ν equal to ρ in the last term. Then

$$194 \quad f'^{(2)}(\psi') = \frac{df'^{(1)}(\psi')}{d\psi'} = \frac{df'^{(1)}(\psi')}{d\psi} \frac{d\psi}{d\psi'} = \left(\frac{df^{(1)}(\psi)}{d\psi} + k_0 h_0 \frac{d(\cos \varphi)}{d\psi} \right) \frac{d\psi}{d\psi'} = f^{(2)}(\psi) + k_0 h_0 \frac{d(\cos \varphi)}{d\varphi} \frac{d\varphi}{d\psi} =$$

$$195 \quad = f^{(2)}(\psi) - k_0 h_0 \sin \varphi \frac{\nu \cos \varphi}{\rho} \quad (28)$$

216 where again we have taken $\frac{d\psi}{d\psi'}$ as unity, and we can take ν equal to ρ in the last term, so that

$$217 \quad f'^{(2)}(\psi') = f^{(2)}(\psi) - k_0 h_0 \sin\varphi \cos\varphi \quad (29)$$

218 Similarly

$$219 \quad f'^{(3)}(\psi') = \frac{df'^{(2)}(\psi')}{d\psi'} = \frac{df^{(2)}(\psi)}{d\psi} \frac{d\psi}{d\psi'} = \left(\frac{df^{(2)}(\psi)}{d\psi} - k_0 h_0 \frac{d(\sin\varphi \cos\varphi)}{d\psi} \right) = f^{(3)}(\psi) - k_0 h_0 \frac{d(\sin\varphi \cos\varphi)}{d\varphi} \frac{d\varphi}{d\psi} =$$

$$220 \quad = f^{(3)}(\psi) - k_0 h_0 (\cos^2\varphi - \sin^2\varphi) \frac{\nu \cos\varphi}{\rho} \quad (30)$$

221 where again $\frac{d\psi}{d\psi'}$ has been taken as unity and we can take ν equal to ρ in the last term.

222 Therefore

$$223 \quad f'^{(3)}(\psi') = f^{(3)}(\psi) - k_0 h_0 (\cos^2\varphi - \sin^2\varphi) \cos\varphi \quad (31)$$

224 Now, for computation of subsequent derivatives the influence of the last term can be neglected

225 as well as $\frac{d\psi}{d\psi'}$ be taken as unity, so that

$$226 \quad f'^{(4)}(\psi') = f^{(4)}(\psi) \quad (32)$$

$$227 \quad f'^{(5)}(\psi') = f^{(5)}(\psi) \quad (33)$$

$$228 \quad f'^{(6)}(\psi') = f^{(6)}(\psi) \quad (34)$$

229 Inserting the function Eq. (24) and its derivatives – Eqs. (27), (29), and (30) to (34) – into Eqs.

230 (18) and (19) and recalling that

$$231 \quad x_e = \Delta\lambda f^{(1)}(\psi) - \frac{\Delta\lambda^3}{6} f^{(3)}(\psi) + \frac{\Delta\lambda^5}{120} f^{(5)}(\psi) + \dots \quad (35)$$

$$232 \quad y_e = f(\psi) - \frac{\Delta\lambda^2}{2} f^{(2)}(\psi) + \frac{\Delta\lambda^4}{24} f^{(4)}(\psi) - \frac{\Delta\lambda^6}{720} f^{(6)}(\psi) + \dots \quad (36)$$

233 are the equations for the ellipsoid-to-plane Transverse Mercator projection, we can obtain the

234 corresponding equations for the ChS-to-plane Transverse Mercator projection as

$$235 \quad x = x_e + \Delta\lambda k_0 h_0 \frac{\nu \cos\varphi}{\rho} + \frac{\Delta\lambda^3}{6} k_0 h_0 (\cos^2\varphi - \sin^2\varphi) \cos\varphi \quad (37)$$

$$236 \quad y = y_e + k_0 h_0 \varphi + \frac{\Delta\lambda^2}{2} k_0 h_0 \sin\varphi \cos\varphi \quad (38)$$

217 Needless to say, the coordinates of the standard ellipsoid-to-plane Transverse Mercator
218 projection (x_e, y_e) have to had been computed with the same design parameters (k_0 , false
219 easting, false northing...) than the corresponding coordinates of the ChS-to-plane Transverse
220 Mercator projection (x, y) . Obviously, (x, y) are simplified to (x_e, y_e) for zero height h_0 .

221 As it is demonstrated in the Appendix the scale factor of the ChS-to-plane Transverse Mercator
222 projection is independent of height h_0 and therefore equal to the scale factor of the standard
223 ellipsoid-to-plane Transverse Mercator projection.

$$224 \quad k = k_e \quad (39)$$

225 An algorithm for the inverse computation of geodetic coordinates from grid coordinates can also
226 be found in the Appendix.

227

228 **Conclusions**

229 Direct and Transverse Mercator-type projections for ChS-to-plane conformal mapping have
230 been derived. The formulation has been kept relatively simple and approximate enough to
231 guarantee a degree of conformality of the order of 10^{-9} or better for the sensible range of
232 application (latitudes from 0 to 80° , heights from 0 to 3000m, increments of longitudes up to 3°).
233 While the Direct Mercator projection is of very limited use since its distortions become too large
234 except for a very thin band (advisably below 2°) centered in the equator, the Transverse
235 Mercator projection presented is of general use except very near the poles (less than 5° or 10°)
236 and can be applied to highly elevated areas, such as the mountainous western regions of the
237 United States, where conventional ellipsoid-to-plane projections may produce intolerable
238 discrepancies between ground and grid distances.

239

240 **Data Availability Statement**

241 Some or all data, models, or code that support the findings of this study are available from the
242 corresponding author upon reasonable request.

243

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246 that helped to improve the manuscript.

247

248 **Appendix. Additional derivations**

249 This section contains additional derivations for the two ChS-to-grid projections presented above.

250 In particular, the derivations provide the corresponding scale factors, demonstrate the fulfillment
251 of Cauchy-Riemann equations for conformality and present algorithms for the inverse
252 computation, namely the determination of latitude and longitude in the ChS of ellipsoid height h_0
253 from grid coordinates x, y .

254 ***Direct Mercator for ChS to plane***

255 Cauchy-Riemann equations are necessary and sufficient conditions for any projection to be
256 conformal (Snyder 1987, p.27). They can be written as

$$257 \begin{aligned} x_\lambda &= y_\psi \\ x_\psi &= -y_\lambda \end{aligned} \tag{40}$$

258 where $x_\lambda, y_\lambda, x_\psi, y_\psi$ are the partial derivatives of the functions defining the map projection with
259 respect to λ and ψ , being (x,y) and (λ, ψ) two isometric coordinate systems.

260 It is easy to demonstrate that the ChS-to-grid Direct Mercator projection, defined by Eqs. (15)
261 and (16), where the isometric latitude is denoted by ψ' , fulfills these conditions, since they
262 reduce to

$$263 \begin{aligned} a &= a \\ 0 &= 0 \end{aligned} \tag{41}$$

264 Similarly to Baselga (2018, 2019) we can define a scale factor k in the infinitesimal
 265 neighborhood of a point as the ratio of the projected distance on the grid defined by Eqs. (15)
 266 and (16), ds_g , to the original distance on the constant-height surface ds_{ChS} , which can be
 267 computed with the general expression

$$268 \quad k = \frac{ds_g}{ds_{ChS}} = \frac{\sqrt{(x_\varphi^2 + y_\varphi^2)d\varphi^2 + (x_\lambda^2 + y_\lambda^2)d\lambda^2 + 2(x_\varphi x_\lambda + y_\varphi y_\lambda)d\varphi d\lambda}}{\sqrt{(\rho + h_0)^2 d\varphi^2 + (\nu + h_0)^2 \cos^2 \varphi d\lambda^2}} \quad (42)$$

269 where x_φ , y_φ , x_λ , y_λ are the partial derivatives of the functions defining the map projection with
 270 respect to φ and λ , and $d\varphi$ and $d\lambda$ are the geographic coordinate differences between two
 271 infinitesimally close points, φ_i , λ_i and $\varphi_j = \varphi_i + d\varphi$, $\lambda_j = \lambda_i + d\lambda$.

272 Scale factors in the meridian and the parallel, k_m and k_p , can be respectively obtained with $d\lambda =$
 273 0 and $d\varphi = 0$ as

$$274 \quad k_m = \frac{\sqrt{x_\varphi^2 + y_\varphi^2}}{\rho + h_0} \quad (43)$$

$$275 \quad k_p = \frac{\sqrt{x_\lambda^2 + y_\lambda^2}}{(\nu + h_0)\cos\varphi} \quad (44)$$

276 For the case of the ChS-to-grid Direct Mercator projection, defined by Eqs. (15) and (16), these
 277 scale factors result in

$$278 \quad k_m = \frac{a\psi'_\varphi}{\rho + h_0} \quad (45)$$

$$279 \quad k_p = \frac{a}{(\nu + h_0)\cos\varphi} \quad (46)$$

280 where ψ'_φ denotes the partial derivative of the isometric latitude ψ' , given by Eq. (14), with
 281 respect to the geodetic latitude φ . The second expression is much simpler to compute than the
 282 first one and we know they must provide the same result since in any conformal projection the
 283 scale factor is direction independent, $k = k_m = k_p$ (Snyder 1987, p.24); therefore, we will prefer
 284 the latter expression for computing the scale factor due to its simplicity.

$$285 \quad k = \frac{a}{(\nu + h_0)\cos\varphi} \quad (47)$$

286 Just in case one might want to compute the first expression, for example for the purpose of
287 verification, the partial derivative ψ'_{φ} is equal to A in the Eq. (54) below.

288 Finally, while Eqs. (15) and (16) provide the direct formulation for the ChS-to-grid projection, the
289 inverse computation, that is, the determination of geodetic coordinates (φ, λ) from grid
290 coordinates (x, y) can be obtained as follows.

291 First, it is immediate to determine the increment of longitude with respect to the origin meridian
292 (of longitude λ_0) from Eq. (15) as

$$293 \quad \Delta\lambda = \frac{x}{a} \tag{48}$$

294 and then the geodetic longitude as

$$295 \quad \lambda = \lambda_0 + \Delta\lambda \tag{49}$$

296 It is also immediate to obtain the isometric latitude ψ' from Eq. (16) as

$$297 \quad \psi' = \frac{y}{a} \tag{50}$$

298 Now, to obtain the geodetic latitude φ from the isometric latitude ψ' we will use the following
299 fastly-convergent iterative procedure. First, the crude approximation

$$300 \quad \psi' \approx \varphi(1 - e_2) \tag{51}$$

301 obtained by first-order series expansion of Eq. (14) around $\varphi = 0$ permits to obtain a first
302 approximate value for the latitude, denoted here by φ_0

$$303 \quad \varphi_0 = \frac{\psi'}{1 - e_2} \tag{52}$$

304 where one should recall the definition of e_2 in Eq. (13).

305 A first-order series expansion of Eq. (14) this time around $\varphi = \varphi_0$ provides

$$306 \quad \psi' \approx \psi'_0 + A(\varphi - \varphi_0) \tag{53}$$

307 where ψ'_0 is obtained by substituting $\varphi = \varphi_0$ into Eq. (14) and

$$\begin{aligned}
308 \quad A &= \frac{\cos\left(\frac{\varphi_0}{2}\right)^2 + \sin\left(\frac{\varphi_0}{2}\right)^2}{\left(\cos\frac{\varphi_0}{2} - \sin\frac{\varphi_0}{2}\right)\left(\cos\frac{\varphi_0}{2} + \sin\frac{\varphi_0}{2}\right)} - e_2 \cos \varphi_0 - e_2^2 \left(1 + \frac{3h_0}{2a}\right) \cos \varphi_0 \sin^2 \varphi_0 - e_2^3 \left(1 + \frac{21h_0}{8a}\right) \cos \varphi_0 \sin^4 \varphi_0 - \\
309 \quad &e_2^4 \cos \varphi_0 \sin^6 \varphi_0 \tag{54}
\end{aligned}$$

310 A new latitude value can therefore be obtained by

$$311 \quad \varphi = \varphi_0 + \frac{\psi' - \psi'_0}{A} \tag{55}$$

312 This new value is now taken as initial latitude φ_0 for the subsequent iteration so that it is
313 introduced into Eq. (14) to obtain ψ'_0 and used in Eq. (54) to obtain a new value for A. Both of
314 them are introduced into Eq. (55) to obtain a refined latitude value. As said, this procedure
315 converges fast, usually in just two iterations for low latitudes, as with the numerical example
316 below, or a few more iterations for medium or high latitudes (where this projection is not
317 recommended, recall the corresponding high distortions shown for these latitudes in Table 1).

318 Some numerical values for an example of use of the ChS-to-grid Direct Mercator projection
319 follow: given the GRS80 ellipsoid ($a = 6378137$, $f = 1/298.257222101$, $e = \sqrt{2f - f^2}$), geodetic
320 coordinates $\varphi = 20^\circ$ and $\lambda = 6^\circ$, origin of longitudes $\lambda_0 = 3^\circ$, and ellipsoid height $h_0 = 2000\text{m}$ of
321 the ChS, the direct computation is solved by Eq. (15) and Eq. (14) into Eq. (16) resulting in $x =$
322 333958.472m and $y = 2258428.227\text{m}$. The scale factor, computed by means of Eq. (47), is
323 1.06342769 . The inverse computation, starting with these values for x and y , produce the initial
324 geodetic coordinates $\varphi = 20^\circ$ and $\lambda = 6^\circ$.

325

326 ***Transverse Mercator for ChS to plane***

327 It is easy to demonstrate that the ChS-to-grid Transverse Mercator projection, defined by Eqs.
328 (18) and (19), where the isometric latitude is denoted by ψ' , fulfills Cauchy-Riemann conditions,
329 Eq. (40), since the partial derivative of x , given in Eq. (18), with respect to λ

$$330 \quad x_\lambda = f'^{(1)}(\psi') - \frac{3}{6} \Delta \lambda^2 f'^{(3)}(\psi') + \frac{5}{120} \Delta \lambda^4 f'^{(5)}(\psi') - \dots \tag{56}$$

331 and the partial derivative of y , given in Eq. (19), with respect to ψ'

332
$$y_{\psi'} = f'^{(1)}(\psi') - \frac{\Delta\lambda^2}{2} f'^{(3)}(\psi') + \frac{\Delta\lambda^4}{24} f'^{(5)}(\psi') - \dots \quad (57)$$

333 produce the same series. Analogously, the partial derivative of x with respect to ψ'

334
$$x_{\psi'} = \Delta\lambda f'^{(2)}(\psi') - \frac{\Delta\lambda^3}{6} f'^{(4)}(\psi') + \frac{\Delta\lambda^5}{120} f'^{(6)}(\psi') - \dots \quad (58)$$

335 and the partial derivative of y with respect to λ

336
$$y_{\lambda} = -\frac{2}{2} \Delta\lambda f'^{(2)}(\psi') + \frac{4}{24} \Delta\lambda^3 f'^{(4)}(\psi') - \frac{6}{720} \Delta\lambda^5 f'^{(6)}(\psi') + \dots \quad (59)$$

337 are series equal except for a sign change, as required by the second condition of Cauchy-
338 Riemann, Eq. (40).

339

340 Now, we obtain the scale factor of the ChS-to-grid Transverse Mercator projection. As in Eq.

341 (42) the desired scale factor is defined as the ratio of the grid distance ds_g to the distance on the

342 constant-height surface ds_{ChS} . We can also compute other two differential distances: the

343 distance on the surface of the ellipsoid ds_e and the grid distance obtained using the formulation

344 of the standard Transverse Mercator projection ds_{g0} . Dividing and multiplying by these two

345 distances we can transform a little bit the equation for the scale factor

346
$$k = \frac{ds_g}{ds_{ChS}} = \frac{ds_g}{ds_{g0}} \frac{ds_{g0}}{ds_e} \frac{ds_e}{ds_{ChS}} \quad (60)$$

347 The transformation from the ellipsoid to the grid using the formulation of the standard

348 Transverse Mercator projection has a scale factor which we have previously denoted as k_e , this

349 is precisely the second factor required in the equation above

350
$$\frac{ds_{g0}}{ds_e} = k_e \quad (61)$$

351 The last factor in Eq. (60) is the ratio of the distance on the ellipsoid to the distance on the

352 constant-height surface. Using the first fundamental forms of the ellipsoid and the constant-

353 height surface we can write

354
$$\frac{ds_e}{ds_{ChS}} = \frac{\sqrt{\rho^2 d\varphi^2 + v^2 \cos^2 \varphi d\lambda^2}}{\sqrt{(\rho+h_0)^2 d\varphi^2 + (v+h_0)^2 \cos^2 \varphi d\lambda^2}} \quad (62)$$

355 Since the projection is conformal the distortion is independent of the direction (Snyder 1987,
 356 p.24). We can consider $d\lambda = 0$, for simplicity, to analyze the distortion along the meridian,
 357 therefore

$$358 \quad \frac{ds_e}{ds_{ChS}} = \frac{\rho}{\rho+h_0} \quad (63)$$

359 Finally, the first factor required in the right-hand side of Eq. (60) is the ratio of the distance using
 360 coordinates in the ChS Transverse Mercator grid, (x, y) in Eqs. (37) and (38), to the distance
 361 using coordinates in the standard Transverse Mercator grid, (x_e, y_e) . Using the corresponding
 362 first fundamental forms we can write

$$363 \quad \frac{ds_g}{ds_{go}} = \frac{\sqrt{dx^2+dy^2}}{\sqrt{dx_e^2+dy_e^2}} \quad (64)$$

364 where dx, dy denote differences in the ChS Transverse Mercator grid coordinates of two
 365 neighboring points in the same meridian (recall that we are considering $d\lambda = 0$) and analogously
 366 for dx_e, dy_e for their corresponding coordinates in the standard Transverse Mercator grid. These
 367 coordinate differences are due to a difference in latitude $d\varphi$ only, therefore $dy^2 \gg dx^2$ and
 368 $dy_e^2 \gg dx_e^2$, and no significant error is committed if for this ratio we make the consideration that
 369 $dx^2 + dy^2 \approx dy^2$ and $dx_e^2 + dy_e^2 \approx dy_e^2$.

370 Therefore, we have

$$371 \quad \frac{ds_g}{ds_{go}} = \frac{dy}{dy_e} \quad (65)$$

372 Considering Eq. (38) we can write

$$373 \quad dy = \frac{\partial y_e}{\partial \varphi} d\varphi + \frac{\partial}{\partial \varphi} (k_0 h_0 \varphi) d\varphi + \frac{\partial}{\partial \varphi} \left(\frac{\Delta \lambda^2}{2} k_0 h_0 \sin \varphi \cos \varphi \right) d\varphi \quad (66)$$

374 The last term can be safely neglected, being the increment of longitude with respect to the
 375 central meridian a value well below one ($\Delta \lambda \ll 1 \approx 57.2957795^\circ$). Therefore

$$376 \quad dy = \frac{\partial y_e}{\partial \varphi} d\varphi + k_0 h_0 d\varphi \quad (67)$$

377 Considering that

378 $dy_e = \frac{\partial y_e}{\partial \varphi} d\varphi$ (68)

379 Eq. (65) reads

380 $\frac{ds_g}{ds_{go}} = \frac{\frac{\partial y_e}{\partial \varphi} + k_0 h_0}{\frac{\partial y_e}{\partial \varphi}}$ (69)

381 To evaluate the derivative of coordinate y in the standard Transverse Mercator projection we
 382 recall that its leading term in y is the length along the meridian $m(\varphi)$ (Osborne 2013, p.122, Eq.
 383 7.29), that is $y_e \approx m(\varphi)$ or, if a central scale factor k_0 is used

384 $y_e \approx k_0 m(\varphi)$ (70)

385 For an infinitesimal change in latitude $d\varphi$ the corresponding meridian length can be computed
 386 as

387 $dm(\varphi) = \rho d\varphi$ (71)

388 With $\frac{dm(\varphi)}{d\varphi} = \rho$ from Eq. (71) we can compute from Eq. (70)

389 $\frac{\partial y_e}{\partial \varphi} = k_0 \frac{dm(\varphi)}{d\varphi} = k_0 \rho$ (72)

390 which, upon substitution in Eq. (69), yields

391 $\frac{ds_g}{ds_{go}} = \frac{k_0 \rho + k_0 h_0}{k_0 \rho} = \frac{\rho + h_0}{\rho}$ (73)

392 Now, introducing Eqs. (73), (61) and (63) into (60) we obtain

393 $k = \frac{ds_g}{ds_{ChS}} = \frac{\rho + h_0}{\rho} k_e \frac{\rho}{\rho + h_0} = k_e$ (74)

394 That is, the scale factor of the ChS-to-plane Transverse Mercator projection is equal to the scale
 395 factor of the standard ellipsoid-to-plane Transverse Mercator projection. This result can be
 396 confirmed by an alternative computation procedure completely independent from the
 397 demonstration above which relies only on the defining equations of the projection: using
 398 numerical determination of partial derivatives of Eqs. (37) and (38) (i.e. by computing
 399 coordinates for small increments of latitude and longitude) and subsequent calculation of the
 400 scale factors by Eqs. (43) and (44) we obtain negligible discrepancies of the order of 10^{-9} or

401 below, partly attributable to the truncation in the series in Eqs. (37) and (38), which confirm this
 402 result.

403

404 Finally, while Eqs. (37) and (38) provide the direct formulation for the ChS-to-grid projection, the
 405 inverse computation, that is, the determination of geodetic coordinates (φ, λ) from grid
 406 coordinates (x, y) can be obtained as follows.

407 First, as a starting approximation we obtain initial latitude and longitude values (φ, λ) by means
 408 of the inverse formulas for the standard Transverse Mercator projection of the reference
 409 ellipsoid using (x, y) as if they were indeed (x_e, y_e) .

410 From Eqs. (37) and (38) we can write

$$411 \quad x_e = x - \Delta\lambda k_0 h_0 \frac{w \cos \varphi}{\rho} - \frac{\Delta\lambda^3}{6} k_0 h_0 (\cos^2 \varphi - \sin^2 \varphi) \cos \varphi \quad (75)$$

$$412 \quad y_e = y - k_0 h_0 \varphi - \frac{\Delta\lambda^2}{2} k_0 h_0 \sin \varphi \cos \varphi \quad (76)$$

413 Now we start the following simple iterative procedure: introducing the approximate latitude and
 414 longitude values obtained before in these two equations along with the known coordinates (x, y) ,
 415 we obtain new values (x_e, y_e) from which we can obtain refined values for the latitude and the
 416 longitude by means of the inverse formulas for the standard Transverse Mercator projection.
 417 This procedure has a fast convergence, for instance, for the following numerical example in the
 418 second iteration the coordinate differences are already of the order of 10^{-9} .

419 Some numerical values for an example of use of the ChS-to-grid Transverse Mercator
 420 projection follow: given the GRS80 ellipsoid ($a = 6378137$, $f = 1/298.257222101$, $e = \sqrt{2f - f^2}$),
 421 geodetic coordinates $\varphi = 40^\circ$ and $\lambda = 6^\circ$, origin of longitudes $\lambda_0 = 3^\circ$, and ellipsoid height $h_0 =$
 422 2000m of the ChS, central scale factor $k_0 = 0.9996$ and false easting of 500000m, the direct
 423 computation is solved by Eq. (37) and Eq. (38) resulting in $x = 756180.159$ m and $y =$
 424 4433466.111m. The scale factor, computed by means of Eq. (74), is 1.00040750. The inverse

425 computation, starting with these values for x and y , produce the initial geodetic coordinates $\varphi =$
426 40° and $\lambda = 6^\circ$.

427

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478 **Tables**

479 **Table 1.** Conformality test for Direct Mercator projection for ChS (of height h_0) to plane: k_m and k_p denote the linear
 480 distortion in the meridian and parallel directions, respectively. For comparison, the scale value of the Direct
 481 Mercator projection for the reference ellipsoid along the meridian k_{em} and its difference with respect to its scale
 482 along the parallel k_{ep} are also given.

Latitude (deg)	h_0 (m)	k_m	$k_m - k_p$	k_e	$k_{em} - k_{ep}$
0	0	1	0	1	0
0	1000	0.99984324	-1.11E-16	1	0
0	2000	0.99968653	0	1	0
0	3000	0.99952986	0	1	0
20	0	1.06376102	2.22E-15	1.06376102	2.22E-15
20	1000	1.06359432	2.66E-15	1.06376102	2.22E-15
20	2000	1.06342769	2.44E-15	1.06376102	2.22E-15
20	3000	1.06326110	2.22E-15	1.06376102	2.22E-15
40	0	1.30360069	3.02E-13	1.30360069	3.02E-13
40	1000	1.30339662	3.01E-13	1.30360069	3.02E-13
40	2000	1.30319261	3.01E-13	1.30360069	3.02E-13
40	3000	1.30298867	3.01E-13	1.30360069	3.02E-13
60	0	1.99497290	2.14E-12	1.99497290	2.14E-12
60	1000	1.99466095	2.14E-12	1.99497290	2.14E-12
60	2000	1.99434910	2.13E-12	1.99497290	2.14E-12
60	3000	1.99403735	2.13E-12	1.99497290	2.14E-12
80	0	5.74004558	2.07E-12	5.74004558	2.07E-12
80	1000	5.73914869	2.07E-12	5.74004558	2.07E-12
80	2000	5.73825208	2.07E-12	5.74004558	2.07E-12
80	3000	5.73735575	2.07E-12	5.74004558	2.07E-12

483