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Escriche Roberto, MI.; Oroian, M.; Visquert Fas, M.; Gras Romero, ML.; Vidal Brotons, DJ. (2016). Rheological properties of honey from Burkina Faso: loss modulus and complex viscosity modelling. *International Journal of Food Properties*. 19(11):2575-2586. doi:10.1080/10942912.2015.1136938



The final publication is available at

<http://doi.org/10.1080/10942912.2015.1136938>

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Additional Information

1 **RHEOLOGICAL PROPERTIES OF HONEY FROM BURKINA FASO: LOSS**
2 **MODULUS AND COMPLEX VISCOSITY MODELLING**

3 *Shortened title: Rheological properties of honey from Burkina Faso*

4 **Isabel Escriche¹, Mircea Oroian², Mario Visquert¹, María L. Gras¹ & Daniel Vidal¹**

5 ¹Institute of Food Engineering for Development (IUIAD). Food Technology Department (DTA).
6 Universitat Politècnica de València. Valencia, Spain

7 ²Faculty of Food Engineering, Stefan cel Mare University of Suceava, Suceava, Romania

8 *Corresponding author: Isabel Escriche, iescrich@tal.upv.es;

9 Tel.: +34-963877366; fax: +34-963877369;

10
11 **Abstract**

12 This study evaluates the rheological behaviour of Burkina Faso honey and the use of exponential
13 and polynomial models to predict the influence of chemical composition and temperature on the
14 viscoelastic parameters: complex viscosity (η^*) and loss modulus (G''). Samples were first
15 characterized evaluating: water activity, HMF, sugars (fructose, glucose and sucrose), electrical
16 conductivity, moisture and colour. Dynamic rheological properties were obtained at different
17 temperatures (5, 10, 15, 20, 25, 30 and 40°C). All the honeys displayed Newtonian behaviour.
18 Complex viscosity and loss modulus can be predicted based on the chemical composition and
19 temperature using polynomial models ($R^2 > 98.00\%$).

20
21 **Keywords:** honey, rheology, complex viscosity, loss modulus
22
23

24 **Introduction**

25 In Burkina Faso, situated in West Africa, beekeeping activities have increased in the last years,
26 thanks in part to the installation of beekeeping promotion centres, sponsored by beekeeper
27 organizations [1]. These activities are helping in the production of honey and therefore, are playing
28 an important role in society by creating sustainable livelihoods. The current development in
29 Burkina honey production is reflected in the number of scientific papers published in recent years.
30 For example, different authors studied the impact of storage conditions on the physicochemical
31 characteristics of Burkina Faso honey [1]; the impact of climatic changes on nectar considering
32 honey production by honeybee colonies in a specific zone of Burkina Faso [2]; the compliance of
33 international standards related to the importation and sale of honey in Burkina Faso [2].

34 As far the authors know, there is no research related to the rheological properties of honey from
35 this country. Knowledge about the rheological behaviour of viscous food stuff is useful in quality
36 and process control [3]. The importance of measuring the rheological properties of honey is
37 reflected in the volume of research published in the last decade about honey from different
38 countries [4, 5]. For this reason, the aim of this study was to predict the influence of chemical
39 composition and temperature on the viscoelastic parameters of honey (complex viscosity (η^*) and
40 loss modulus (G'')) using the exponential model and the polynomial model. As honey rheology is
41 directly related to different chemical parameters [3, 5, 6], samples were first characterized from a
42 chemical point of view.

43 **Materials and methods**

44 **Honey samples**

45 Honey (18 samples) from three different places (Kampène, Bouroum-Bouroum and Passena) in the
46 Poni region situated in the Southwestern region of Burkina Faso were provided by beekeepers. As

47 the rheological parameters of honeys can be influenced by the presence of crystals and air bubbles
48 [7, 8], they were warmed up to 55 °C before being used, and kept in flasks at 30 °C to remove air
49 bubbles that could interfere with rheological studies [4].

50 **Physicochemical analyses**

51 The physicochemical properties (HMF, moisture, electrical conductivity) and Pfund colour, were
52 determined according to the harmonised methods of the international honey commission [9]. Water
53 activity (a_w) was measured at 25 °C (± 0.2 °C) using an electronic dewpoint water activity meter,
54 Aqualab Series 4 model TE (Decagon Devices, Pullman, Washington, USA), equipped with a
55 temperature-controlled system [10]. Sugars content (glucose, fructose and sucrose) were analysed
56 in a HPAEC-PAD high-resolution ionic chromatograph with a pulsed amperometric detector
57 (PAD) (Bioscan, Methrom, Switzerland) and a Metrosep Carb chromatographic column (styrene
58 divinyl benzene copolymer, 4.6 \times 250 mm). Carbohydrates were eluted with NaOH 0.1N at a flow
59 rate of 1 mL min⁻¹ [11].

60 **Viscoelastic measurement**

61 A RheoStress 1 rheometer (Thermo Haake, Germany) was used to determine the dynamic
62 rheological properties of honey samples at different temperatures (5, 10, 15, 20, 25, 30 and 40°C),
63 by means of a parallel plate system (\varnothing 60 mm) with a gap of 500 μ m. The measurement at each
64 temperature was carried out twice using a fresh sample of honey. The sample was loaded, and left
65 for 5 min to allow the sample to reach the desired temperature. With the aim of determining the
66 linear viscoelastic range, stress sweeps were run at 1Hz first. Then, the frequency sweeps were
67 performed over the range $\omega=0.62$ – 62.83 rad/s at 1 Pa stress. The 1 Pa stress was in the linear
68 viscoelastic range. The experimental data were used to calculate storage (or elastic) modulus (G'),

69 loss (viscous) modulus (G''), and complex viscosity (η^*) using Rheowin Job software (v. 2.93,
70 Haake).

71 **Results and discussion**

72 **Physicochemical characterization**

73 Different physicochemical parameters were analysed: HMF, moisture, electrical conductivity,
74 Pfund colour, water activity content, and sugars content (glucose, fructose and sucrose).

75 The HMF content (widely recognized as an indicator of freshness) ranged between 1.02-35.60
76 mg/kg. All samples were in agreement with the Council Directive relating to honey [12], because
77 in all cases the values of this parameter were lower than 40 mg/kg. However, in some cases the
78 value was close to this limit, too high considering that they were raw honeys. These values were
79 lower than those reported in honey from Burkina Faso [1, 2]. The moisture varied from 17.9 to 22.1
80 g/100g, in some samples exceeding the 20g/100g limit established by the Council Directive
81 relating to honey [12]. The high electrical conductivity (between 683 and 1022 $\mu\text{S}/\text{cm}$) and Pfund
82 colour values (91 to 150) of the samples indicates that the great majority of the analysed honeys
83 could be considered to be honeydew. These values were in the same range with those reported by
84 other authors in Burkina Faso honey [1, 2]. With respect to water activity, the values ranged
85 between 0.61-0.66, higher than the values reported by other authors [13]. The inverted sugar and
86 sucrose content had a range of 62-78 g/100g, and 1-2 g/100g, respectively, meeting the Council
87 Directive relating to honey [12].

88 **Rheological properties of honey**

89 Figure 1 shows the rheograms for three honeys, each from one of the different areas studied in the
90 Poni region of Burkina Faso: 1. Kampène, 2. Bouroum-Bouroum and 3. Passena. It can be

91 observed that the rheological parameters analysed (complex viscosity (η^*), loss modulus (G'') and
92 storage modulus (G')) are strongly influenced by temperature. The values of the rheological
93 parameters (G' , G'' , η) increased with the frequency applied to the sample, showing that G'' had
94 a greater magnitude than G' . Regarding the complex viscosity, the values were not influenced by
95 the frequency applied. Therefore, it can be ascertain that the honey behaved as a Newtonian fluid
96 (fig. 1) as in the case of honey from other countries such as Romania [4] and Spain [5, 14].

97 In general, G' is less important than G'' due to its low value with respect to G'' ($G'' > G'$) [15].
98 Consequently, different authors noted that the elastic behaviour of honey seems to be less
99 important than its viscous behaviour [16]. The rheological properties of honey can also be affected
100 by other factors such as sugars and other polymeric compounds [4, 17]. In particular, as these
101 sugars have different rheological properties, the rheological behaviour can be greatly affect by the
102 sugar content (glucose and fructose)

103 The data for loss modulus and viscosity will be used to obtain the best prediction model.
104 Exponential and polynomial models will be applied, and presented below, to predict the influence
105 of chemical composition and temperature on these two viscoelastic parameters.

106 **Viscosity modelling**

107 *Effect of Temperature*

108 The influence of temperature on the complex viscosity of honey is described using the Arrhenius
109 model, which is:

$$110 \quad \eta^* = \eta_0^* \cdot \exp\left[-\frac{E_a}{RT}\right] \quad (\text{eq. 1})$$

111 Where: η_0 is a constant, R is the gas constant [$\text{kJ}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$], and E_a activation energy (an energy
112 barrier to flowing) [$\text{kJ}\cdot\text{mol}^{-1}$], T – absolute temperature [K]. With respect to activation energies,
113 their magnitude ranged between 41.07–48.58 kJ/mol. These values are strongly influenced by the
114 moisture content; decreasing with the increase in the moisture content. The activation energies for
115 the Burkina Faso honey presented in this study are smaller than those reported in the case of
116 Romanian honeys [4] and in Spanish honeys [3, 5] due to the high moisture content of Burkina
117 Faso honey to the honeys from Romania and Spain. The data were fitted well to the Arrhenius
118 model (the regression coefficients are around 0.99).

119 *Effect of Concentration*

120 The influence of the concentration (C), expressed in °Brix, on the complex viscosity of honey was
121 described by power-law (eq. 2):

$$122 \quad \eta^* = \eta_1^* C^{a_1} \quad (\text{eq. 2})$$

123 and exponential models (eq.3) [15]:

$$124 \quad \eta^* = \eta_2^* \exp(a_2 C) \quad (\text{eq. 3})$$

125 Where: C is the concentration in °Brix and η_1, η_2, a_1, a_2 are constants. The model parameters have
126 been computed using non-linear regression. According to the regression coefficients values (R^2)
127 both models are suitable for predicting the influence of concentration on complex viscosity of
128 honey.

129 In order to calculate the model constants, the viscosity data were fitted to equations 2-3 by non-
130 linear regression. The resulting values of the constants are presented in table 1. The coefficients of
131 regression (R^2) are very similar, so the two models are suitable for describing the effect of the

132 soluble solids on honey viscosity. However, using the absolute average deviation it seems that the
133 power law model is more suitable for predicting the influence of concentration on the complex
134 viscosity of honey.

135 For a given temperature, the activation energy (E_a) for flow is influenced by soluble solid content,
136 which can be described by several models [18]. In the present work, two models have been used
137 (eq.4 and eq.5).

$$138 \quad E_a = A_1 C^{B_1} \quad (\text{eq. 4})$$

$$139 \quad E_a = A_2 \exp(B_2 C) \quad (\text{eq. 5})$$

140 Where, A_1 , A_2 , B_1 and B_2 are constants. The activation energies and the model parameters were
141 computed by non-linear regression. The coefficients of regression (R^2) of the two models proposed
142 above are the same. Computing the absolute average deviation of the activation energies, it can be
143 observed that the exponential model was better than the power law model in describing the
144 dependency of E_a on °Brix concentration.

145 *Combined effect of temperature and concentration*

146 In practise, it is useful to obtain a general equation of the combined influence of the temperature
147 and concentration on complex viscosity of honey [19]. Figure 2 shows the combined influence of
148 temperature and concentration on honey viscosity.

149 In this paper two models of complex viscosity of honey were investigated (eq. 6 and eq.7):

$$150 \quad \eta^* = \eta_3^* \exp(E_1 C + E_a / RT) \quad (\text{eq. 6})$$

$$151 \quad \eta^* = \eta_4^* C^{E_2} \exp(E_a / RT) \quad (\text{eq. 7})$$

152 The parameter data used in the two equations were fitted to these models by the non-linear
 153 regression, and the values of the model constants were determined. The complex viscosity
 154 predictions with temperature and °Brix concentration achieve coefficients of regression between
 155 0.644 and 0.898 (table 2). The AAD certifies that the suitable model corresponds to eq. 6.
 156 Therefore, for the interval of °Brix concentrations and temperatures (T) studied, the following
 157 equation (eq.8) is suggested for evaluating honey viscosity:

$$158 \quad \eta^* = 3.98 \cdot 10^{-17} \cdot \exp(0.275 * C + 420.03 / RT) \quad (\text{eq. 8})$$

159 *Polynomial modelling of viscosity*

160 The data model which predicts the complex viscosity of honey according to its chemical
 161 composition (sugars, non-sugars components, moisture content, etc.) and temperature was made
 162 using a 3rd degree polynomial equation with seven variables. The measured and predicted values
 163 were compared to check the appropriateness of the model. The equation of the model is as given
 164 (eq. 9):

$$165 \quad \eta_{pred}^* = b_0 + \sum_{i=0}^n b_i x_i + \sum_{i=1}^n b_{ii} x_i^2 + \sum_{i=1}^n b_{iii} x_i^3 + \sum_{i<j<k} b_{ijk} x_i x_j x_k + \sum_{i<j} b_{ij} x_i x_j + \sum_{i<j} b_{ij} x_i^2 x_j + \sum_{i<j} b_{ij} x_i x_j^2 \quad (\text{eq. 9})$$

166 Where: η_{pred}^* is the loss modulus predicted, b_0 is a constant that fixes the response at the central
 167 point of the experiments, b_i – regression coefficient for the linear effect terms, b_{ij} – interaction
 168 effect terms, b_{ii} – quadratic effect terms and b_{iii} – cubic effect terms. The operating region and the
 169 levels of the design variables, key factors, are shown as actual and coded values in table 3.

170 A 3rd order polynomial equation with 7 variables for viscosity was obtained as follows based on
 171 the design variables (eq.10):

172 $\log(\eta^*) = 0.59 - 1.53 \cdot X_1 + 1.36 \cdot X_2 - 0.34 \cdot X_7 + 0.05 \cdot X_7^2 + 0.13 \cdot X_1 \cdot X_7 - 0.10 \cdot X_2 \cdot X_7 - 0.16 \cdot X_7^3 + 0.38 \cdot X_1 \cdot X_7^2$
 173 $- 0.33 \cdot X_2 \cdot X_7^2 + 1.27 \cdot X_3 \cdot X_7^2 + 1.07 \cdot X_4 \cdot X_7^2$ (eq. 10)

173 The coefficient of regression of the proposed model (P=0.005) represents 99.38 % (R² adjusted
 174 98.87%, ADD = 16.60). In figure 3 the measured and predicted values of viscosity are represented.
 175 According to equation 10, it can be observed that moisture content and non-sugar substances do not
 176 influence the equation. Fructose and temperature have a negatively linear influence while glucose
 177 has a positive one.

178 **Loss modulus modelling**

179 *Influence of Temperature*

180 The influence of temperature on honey loss modulus was also studied using the Arrhenius model.

181 $G'' = G_0'' \cdot \exp\left[-\frac{E_a}{RT}\right]$ (eq.11)

182 Where: G₀ is a constant, R is the gas constant [kJ·mol⁻¹·K⁻¹], and E_a activation energy (the energy
 183 barrier to flowing) [kJ·mol⁻¹], T – absolute temperature [K]. The activation energy (E_a) values,
 184 calculated by the Arrhenius model ranged between 24.09 and 48.11 kJ/mol. G'' influenced the
 185 magnitude of the activation energy. The activation energy is negatively correlated with moisture.
 186 In terms of regression coefficients they were greater than 0.99 for all the samples analysed.

187 *Effect of Concentration*

188 The influence of the concentration (C, °Brix) on the honey loss modulus can be described by
 189 power-law (eq. 12):

190 $G'' = G_1'' C^{b_1''}$ (eq. 12)

191 and the exponential model (eq.13) [15]:

$$192 \quad G'' = G_2'' \exp(b_2'' C) \quad (\text{eq. 13})$$

193 Where: C is the concentration in °Brix and G_1'' , G_2'' , b_1'' , b_2'' are constants. With the aim of calculating
194 the model constants, the loss modulus data were fitted to equations 12-13 by non-linear regression.
195 The values of the parameters are presented in table 4. According to the ADD values, it seems that
196 the power law model is more suitable for predicting the loss modulus evolution than the
197 exponential model.

198 Considering the mean relative deviation, it appears that the exponential models are more suitable
199 for predicting the influence of the concentration on the magnitude of loss modulus. For a given
200 temperature, the activation energy for flow depends on the soluble solid content which can be
201 described using several models [18]. In the present work, two models were applied (eq. 14 and eq.
202 15):

$$203 \quad E_a = A_1'' C^{B_1''} \quad (\text{eq. 14})$$

$$204 \quad E_a = A_2'' \exp(B_2'' C) \quad (\text{eq. 15})$$

205 Where: A_1'' , A_2'' , B_1'' and B_2'' are constants. The E_a values and the concentration of the corresponding
206 honey were fitted to equations 14 and 15 by nonlinear regression in order to determine the model
207 parameter). The coefficients of regression (R^2) of the two models proposed above are the same (R^2
208 =0.91). The power law model is more suitable for predicting the activation energy value because
209 of the much lower ADD values (12.55 in the case of equation 15, and 30.56 in the case of equation
210 14).

211 *Combined effect of Temperature and Concentration*

212 It is advantageous to obtain an equation describing the combined effect of temperature and
 213 concentration on the viscoelastic parameter [19]. The combined effect of temperature and
 214 concentration on loss modulus is shown in figure 4.

215 The following models for loss modulus were investigated (equations 16 and 17):

$$216 \quad G'' = G_3'' \exp(E_1'' C + E_a / RT) \quad (\text{eq. 16})$$

$$217 \quad G'' = G_4'' C^{E_2''} \exp(E_a / RT) \quad (\text{eq. 17})$$

218 The loss modulus, concentration, and temperature data were fitted to these models by the nonlinear
 219 regression and the values of the model constants were calculated. The values of these constants
 220 are shown in table 5. In the case of the loss modulus predictions, according to the temperature and
 221 concentration, the regression coefficients ranged between 0.550 and 0.908. The ADD value
 222 indicates that eq. 16 was the most appropriated model in the case of Spanish honey [3]. Therefore,
 223 for the interval of ⁰Brix concentrations and temperatures (T) studied, the following equation (eq.
 224 18) is suggested to evaluate the loss modulus (G'') of honey:

$$225 \quad G'' = 4.22 \cdot 10^{-17} \cdot \exp(0.292 * C + 43.178 / RT) \quad (\text{eq. 18})$$

226 *Polynomial modelling of loss modulus*

227 The data model for the prediction of loss modulus (G'') of honey according to the chemical
 228 composition, moisture content and temperature was made using a 3rd degree polynomial equation
 229 with seven variables as in the case of honey viscosity. The equation of the model is (eq. 19):

$$230 \quad G''_{pred} = b_0 + \sum_{i=0}^n b_i x_i + \sum_{i=1}^n b_{ii} x_i^2 + \sum_{i=1}^n b_{iii} x_i^3 + \sum_{i<j<k} b_{ijk} x_i x_j x_k + \sum_{i<j} b_{ij} x_i x_j + \sum_{i<j} b_{ij} x_i^2 x_j + \sum_{i<j} b_{ij} x_i x_j^2 \quad (\text{eq. 19})$$

231 Where: G''_{pred} is the loss modulus predicted, b_0 is a constant that fixes the response at the central
232 point of the experiments, b_i – regression coefficient for the linear effect terms, b_{ij} – interaction
233 effect terms, b_{ii} – quadratic effect terms and b_{iii} – cubic effect terms. A 3rd order polynomial
234 equation with 7 variables for loss modulus was obtained, based on the design variables (table 4)
235 (eq. 20):

$$236 \quad G'' = 1.39 - 1.58 \cdot X_1 + 1.41 \cdot X_2 - 0.40 \cdot X_7 + 0.05 \cdot X_7^2 + 0.50 \cdot X_1 \cdot X_7 - 0.47 \cdot X_2 \cdot X_7 - 0.07 \cdot X_7^3 + 0.91 \cdot X_1 \cdot X_7^2 - 0.85 \cdot X_2 \cdot X_7^2 \quad (\text{eq. 20})$$

237 The regression coefficient for the polynomial model is 98.87 (R^2 adjusted 97.94, $P=0.005$, ADD
238 $= 19.34$). The measured and predicted values of loss modulus are plotted in figure 5. In the case of
239 equation 20 it can be observed that fructose and temperature have a linear negative influence
240 while glucose has a positive influence. The moisture content and non-sugar substances do not have
241 an influence on the model.

242 **Conclusions**

243 The Burkina Faso honey displayed Newtonian behavior at all the temperatures analysed (5, 10, 15,
244 20, 25, 30 and 40 °C). The loss modulus had a higher magnitude than the storage modulus,
245 displaying a solid-like behaviour. The response surface methodology was indeed a good tool for
246 predicting complex viscosity and loss modulus; correlation coefficients higher than 98% were
247 observed, 99.38% in the case of complex viscosity and 98.87% in the case of loss modulus.
248 Fructose and temperature have a negative linear influence on loss modulus and complex viscosity,
249 and therefore on the prediction of both of these factors, while glucose has a positive influence.

250

251 **Acknowledgments** The authors thank the Universitat Politècnica de València for funding the
252 project “Seguridad alimentaria en la Región Suroeste de Burkina Faso. Capacitación en
253 manipulación, transformación y conservación de alimentos locales, y contra la malnutrición
254 infantil (BONALIMENT2013)”, in the framework of the Program ADSIDEO of the Àrea de
255 Cooperació al Desenvolupament.

256

257 **References**

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305
306

307 **Figure Captions**

308

309 **Figure 1.** Rheological behaviour of honey from Burkina Faso. 1) Kampène, 2) Bouroum-
 310 Bouroum and 3) Passena. a) complex viscosity, b) loss modulus, c) elastic modulus

311 **Figure 2.** Influence of temperature and concentration on complex viscosity of honey from
 312 Burkina Faso

313 **Figure 3.** Measured vs. predicted values on complex viscosity of honey from Burkina Faso

314 **Figure 4.** Influence of temperature and concentration on loss modulus of honey from Burkina
 315 Faso

316 **Figure 5.** Measured vs. predicted values on loss modulus of honey from Burkina Faso

317

318 **Table1.** Effect of °Brix concentration (C) on the complex viscosity of honey from Burkina Faso
 319 at different temperatures (T)

Temperature (°C)	Power law				Exponential model			
	η_1	a_1	R^2	AAD	η_2	a_2	R^2	AAD
5	$3 \cdot 10^{-68}$	36.16	0.999	9.37	$2 \cdot 10^{-15}$	0.461	0.999	15.92
10	$8 \cdot 10^{-65}$	34.20	0.995	4.54	$7 \cdot 10^{-15}$	0.436	0.994	5.46
15	$6 \cdot 10^{-75}$	39.45	0.984	12.54	$2 \cdot 10^{-17}$	0.503	0.982	20.82

20	$1 \cdot 10^{-77}$	40.77	0.992	3.17	$5 \cdot 10^{-18}$	0.520	0.991	9.44
25	$2 \cdot 10^{-76}$	40.09	0.999	9.72	$7 \cdot 10^{-18}$	0.512	0.998	12.38
30	$1 \cdot 10^{-73}$	38.62	0.989	6.16	$3 \cdot 10^{-17}$	0.493	0.991	7.54
40	$7 \cdot 10^{-48}$	24.87	0.943	8.99	$2 \cdot 10^{-11}$	0.317	0.939	30.58
<i>ADD</i>				7.78				14.59

320

321

322 **Table 2.** Combined effect of °Brix concentration and temperature on the complex viscosity of
323 honey from Burkina Faso

Model	η [mPa·s]	E_i	E_a	R^2	<i>AAD</i>
$\eta^* = \eta_3 \exp(E_1 C + E_a / RT)$	$3.98 \cdot 10^{-17}$	0.275	420.03	0.898	43.40
$\eta^* = \eta_4 C^{E_2} \exp(E_a / RT)$	$7.10 \cdot 10^{-15}$	7.650	0.693	0.644	80.48

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326 **Table 3.** Correspondence between actual and coded values of design variables

Design variables	Symbol	Actual values of coded levels	
		-1	+1
Fructose (g/100g)	X_1	34.5	43
Glucose (g/100g)	X_2	27.0	32.0
Sucrose (g/100g)	X_3	1.0	12.5
Sugars (g/100g)	X_4	2.63	6.33
Moisture content (g/100g)	X_5	17.96	22.10
Non-sugar substances (g/100g)	X_6	1.57	1.84
Temperature (°C)	X_7	5	40

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328 **Table 4.** Effect of °Brix concentration (C) on the loss modulus of honey from Burkina Faso at
329 different temperatures (T)

Temperature (°C)	Power law model $G'' = G_1'' C^{b_1''}$				Exponential model $G'' = G_2'' \cdot \exp(b_1'' C)$			
	G_1'' [mPa]	b_1''	R^2	D	G_2'' [mPa]	b_2''	R^2	D
5	$2 \cdot 10^{-67}$	36.14	0.99	6.36	$1 \cdot 10^{-14}$	0.46	0.99	14.70
10	$3 \cdot 10^{-62}$	33.23	0.99	37.79	$1 \cdot 10^{-13}$	0.42	0.99	33.09
15	$3 \cdot 10^{-74}$	39.48	0.98	14.10	$1 \cdot 10^{-16}$	0.50	0.98	50.15
20	$5 \cdot 10^{-77}$	40.88	0.99	10.01	$3 \cdot 10^{-17}$	0.52	0.99	7.71
25	$3 \cdot 10^{-76}$	40.41	0.99	12.45	$3 \cdot 10^{-17}$	0.52	0.99	26.54

30	2·10 ⁻⁷³	38.95	0.99	13.22	1·10 ⁻¹⁶	0.50	0.99	17.22
40	7·10 ⁻⁶	3.22	0.87	3.24	0.35	0.04	0.87	10.85
<i>D - mean</i>				13.88				22.89

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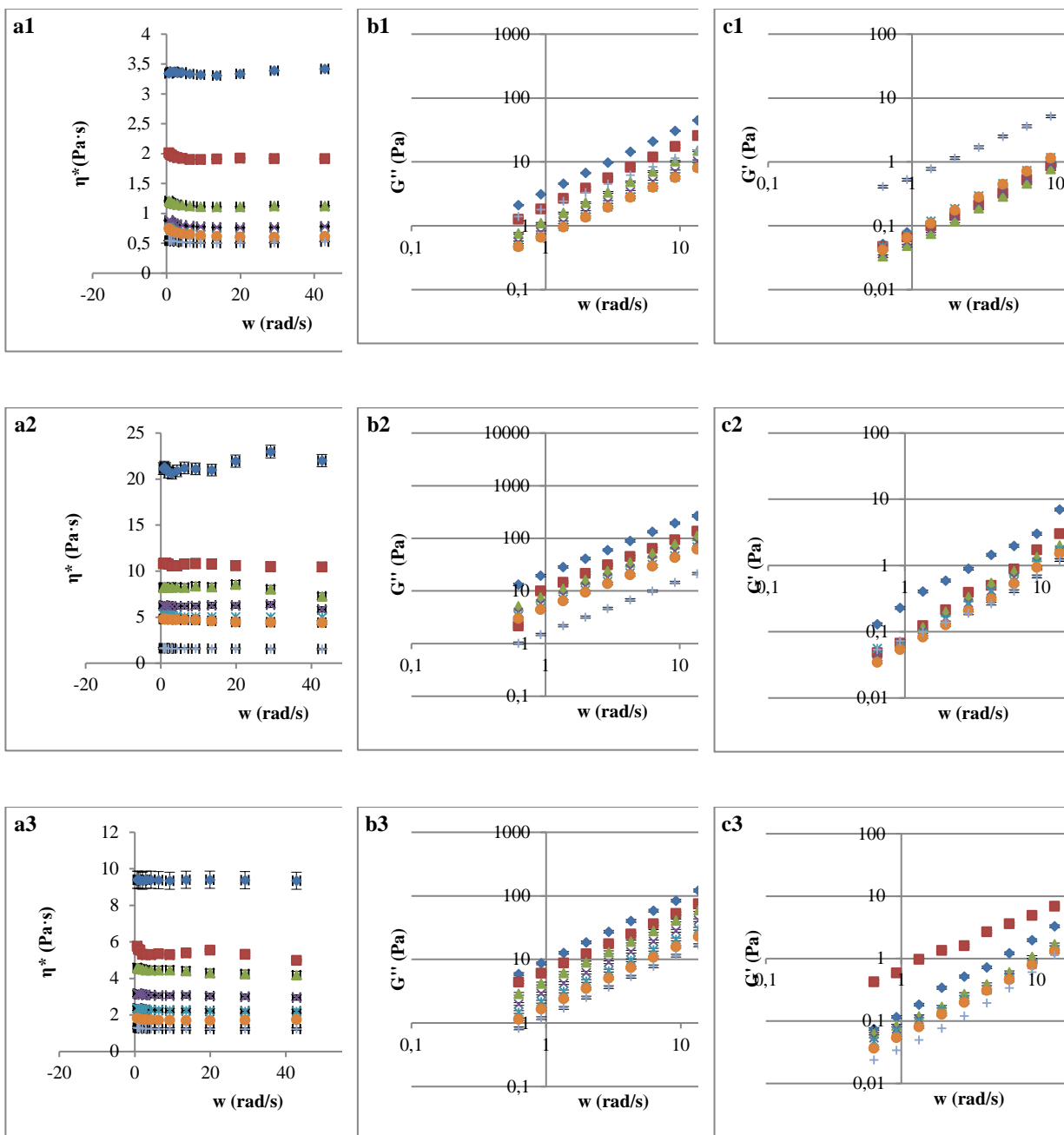


Figure1.

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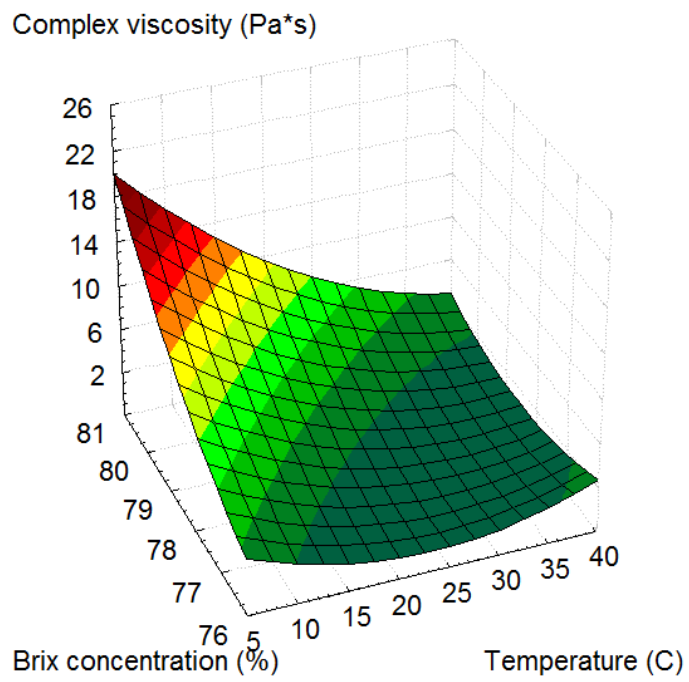


Figure 2.

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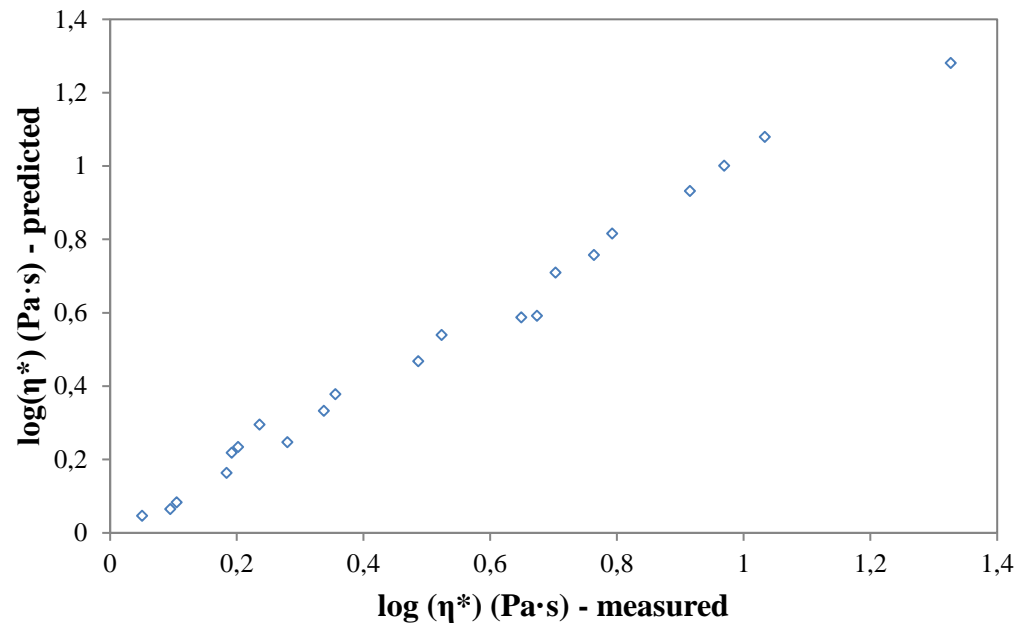


Figure 3.

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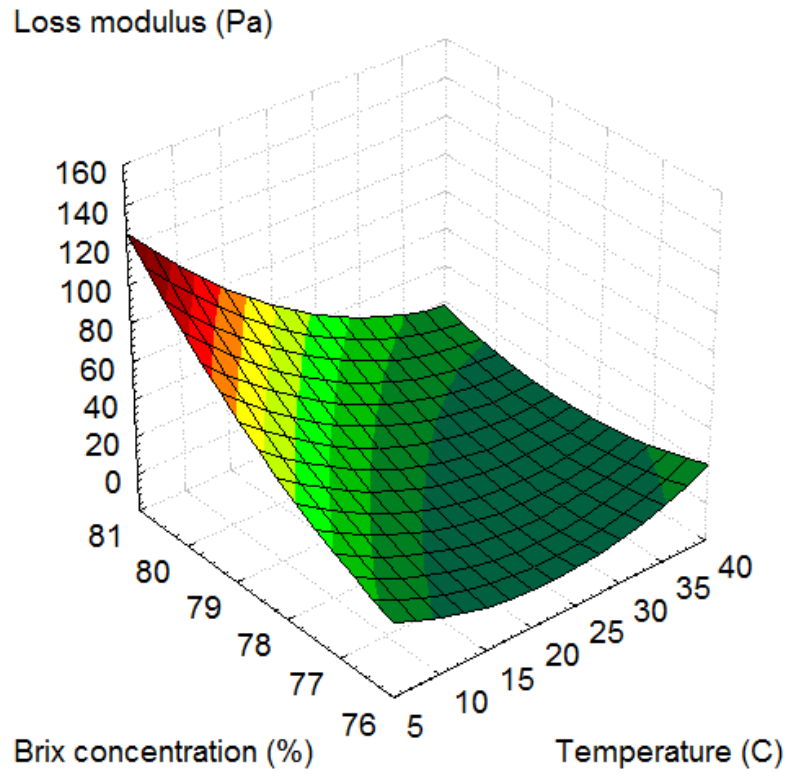
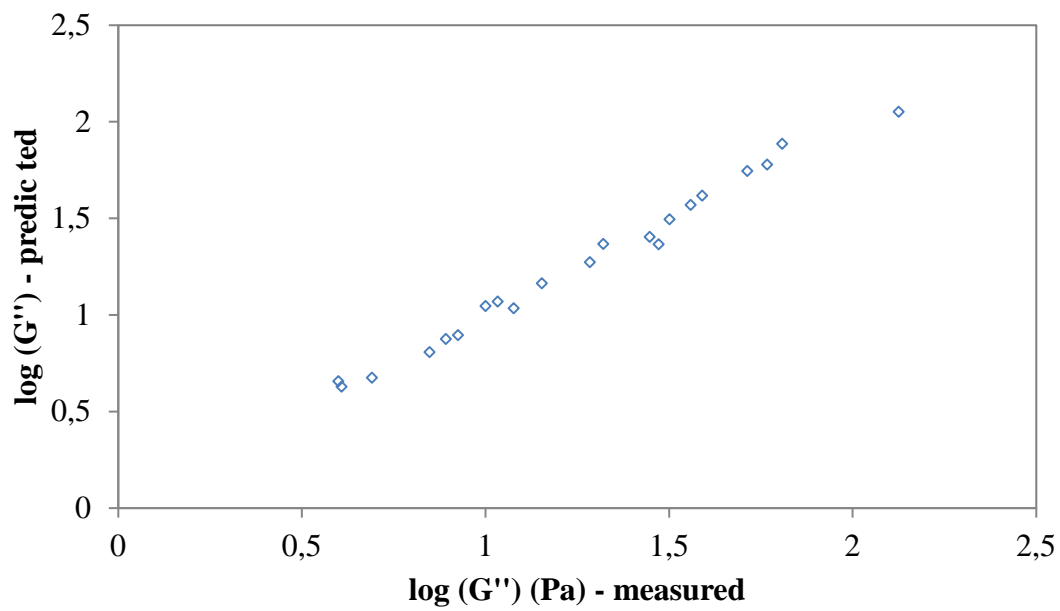


Figure 4.

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339 **Figure 5.**

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