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Additional Information

Influence of plasticizers on thermal properties and

crystallization behaviour of poly(lactic acid) films obtained

by compression molding

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Key words: Poly(lactic acid), plasticizer, compression molded films, crystallization, glass transition temperature, stretchability.

Abstract

Neat and plasticized poly(lactic acid) (PLA) films were obtained by compression molding. Three different plasticizers, at concentrations of 5% and 10%, were used: poly(ethylene glycol) (PEG) 1000 and 4000 g/mol molecular weights and a commercial plasticizer, Palamoll®638. Crystallization behaviour and glass transition of PLA in the films were analysed using differential scanning calorimetry (DSC) and X-Ray diffraction. Films were also characterised in terms of structural, tensile, barrier and optical properties. The addition of the three plasticizers reduced the glass transition temperature (Tg) while promoting the crystallization of PLA in the compression molded films, depending on their type and concentration. PEG 4000 enhanced crystallization more than PEG 1000 and Palamoll®638, the latter being the one which induced the lowest degree of crystallization. The Tg values of the PLA amorphous phase was reduced by the addition of plasticizers, proportionally to their concentration. Nevertheless, all of the plasticized films exhibited similar elastic modulus and were less resistant to break and less extensible due to the greater induced crystallinity. PEG

- 4000 drastically reduced the film's stretchability whereas this effect was less marked when
- 25 Palamoll®638 was used.

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1. Introduction

- PLA is a linear aliphatic thermoplastic polyester derived from lactic acid and obtained from 28 100% renewable plant sources, such as corn starch or sugar. Best known for its 29 biodegradability, PLA is a good alternative to replace petroleum-based polymers, such as 30 polystyrene or polyethylene. Since the field of packaging is one of the major consumers of 31 plastics, it is becoming more and more necessary to use biodegradable polymers to limit 32 pollution associated with plastic wastes. PLA is biocompatible and has been approved by the 33 Food and Drug Administration (FDA) for direct contact with biological fluids¹. It can be 34 processed either by extrusion, injection molding, film casting or fibre spinning²⁻⁵. It also has 35 good transparency, higher than that of polyethylene terephthalate (PET) or polystyrene (PS), 36 and a high comparable mechanical strength. However, it is very brittle, with an elongation at 37 break (% ε) of less than 10%^{6,7}, which restricts its application as films for the packaging 38 industry. Plasticizers are widely used to improve the processability, flexibility and ductility of 39 polymers. In the case of amorphous or semi-crystalline polymers, such as PLA, an efficient 40 plasticizer not only has to reduce the glass transition temperature, but also to depress the 41 melting point and the crystallinity. Considerable efforts have been made to improve the 42 mechanical flexibility of PLA by blending it with compatible plasticizers or other soft 43 polymers. 44
- The use of various low molecular weight plasticizers, such as citrates or adipates⁸, leads to the migration of plasticizers within the PLA matrix, due to their high molecular mobility. To avoid this migration problem, many high molecular weight plasticizers including poly(ethylene glycol) (PEG), poly(propylene glycol), polyester diol or poly(diethylene

adipate) have been used^{2,9}. The plasticizing properties of PEG, with different molecular weights, in PLA matrices have been extensively studied. A large amount of these compounds is usually needed in order to be effective at promoting film plasticity, which can overcome the miscibility limit¹⁰, leading to phase separation, and negatively affecting the properties of the material. The aging of plasticized PLA also provoked the migration and phase separation of PEG¹¹. Hu et al.¹² observed crystallization of PEG 8000 when it was added as plasticizer in PLA at 30 % wt. in PLA matrices. This compound accelerated the PLA crystallization, depending on the cooling rate, and PEG crystallinity was proportional to PLA crystallinity. Sungsanit et al.¹³ also reported phase separation and crystallization of PEG 1000 above 15 % in the PLA blends. The impact resistance and crystallinity of PLA films rose in line with the increase in plasticizer content, whereas both a drop in glass transition temperature and less stiff films were observed. Similar results were obtained by Chieng et al. 14 using PEG 200 at different ratios in the PLA blends. The plasticization of the PLA with PEG 200 effectively lowers Tg as well as the cold-crystallization temperature, in line with the increase in the plasticizer content. Baiardo et al¹⁵ reported a very good correlation between mechanical properties of plasticized PLA and the Tg of the blend using PEGs with different molecular weights. The lower the T_g depression by the plasticizer, the more extensible the PLA material, although some deviations from the established tendencies were observed, which could be explained by the contribution of the degree of crystallinity of the samples. In this sense, it is remarkable that, whereas the thermal history of the samples was erased to obtain thermal parameters, tensile properties were analyzed in the samples with their own thermal history of unknown crystallinity. The contribution of the crystalline fraction to the mechanical properties of PLA has not been reported.

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Other compounds, such as hazelnut and cocoa extract, can also act as plasticizers for PLA¹⁶, as well as keratins and brown alpaca fibres ¹⁷. Likewise, PLA was toughened by blending

with a PEG-based polyester, poly (polyethylene glycol-co-citric acid)¹⁸, which greatly improved elongation at break and the impact resistance as compared with the same amount of the corresponding PEG.

The presence of compatible plasticizers enhances the free volume of the chains which induces

molecular mobility. This reduces the glass transition temperature but it can also favour the crystallization process in semi-crystalline polymers. These two phenomena have opposing effects on the ductility of the polymer and can be dependent on the molecular structure of plasticizer, and the associated intrinsic viscosity, and the molecular interactions with the polymer chains. Likewise, the processing conditions, with different heating and cooling rates, determine the crystallinity degree of the polymer, which in turn affects the mechanical performance of the material. In this study, two extensively studied plasticizers (PEG 1000, PEG 4000) and one new one (Palamoll®638), in two different ratios (5 and 10 %), were melt blended with PLA to obtain films by compression molding and their effect on the crystallization and thermal behaviour of the PLA during film processing was analysed, as well as their impact on the tensile and barrier properties of the obtained films. The relatively low amount of plasticizers was considered in order to avoid phase separation of these compounds in the films, as described in previous studies. The overall migration values of both un-plasticized and plasticized films in aqueous food simulants were also analysed for the purposes of determining the influence of plasticizers on the potential film compound release into food systems.

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2. Materials and methods

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2. 1. Materials

PLA resin (LL700, density of 1.25 g/cm³) was purchased from Ercros (Spain). Poly(ethylene glycol) 1000 and 4000 g/mol molecular weights (PEG 1000 and PEG 4000) were obtained from Sigma–Aldrich (Germany). Palamoll®638 was purchased from BASF (Germany). This commercial polymeric plasticizer is derived from adipic acid, 1,2 propane diol and 1 octanol, with a high viscosity of 7000-9500 mPa.s (at 20°C), listed for food contact applications and it is practically insoluble in water and oils.

2. 2. Film preparation

PLA was first dried at 60°C for 24 h to remove residual water. PLA and plasticizers (10% w/w) were then hot-mixed in a two-roll mill (ModelLRM-M-100, Labtech Engineering, Thailand) at 200°C and 10 rpm for 20 min to ensure a good homogenization of plasticizers with the polymer. Nevertheless, this relatively long time could provoke chain scission in the polymer. The resulting paste was then compression molded in a hydraulic press (Model LP20, Labtech Engineering, Thailand). 3 g of sample were placed onto steel sheets and pre-heated at 200°C for 4 min. Then, compression was performed at 200°C and 100 bars for 4 min, followed by a cooling cycle of 3 min until the temperature reached about 70°C. The obtained films were maintained in desiccators with silica-gel at room temperature until analyses were carried out.

2. 3. Film characterization

2. 3. 1. Film thickness

- A hand-held digital micrometer (Electronic Digital Micrometer, Comecta S.A., Barcelona, Spain) was used to measure film thickness to the closest 0.001mm, at 6 random positions
- around the film prior to mechanical test analyses.

2. 3. 2. Thermal properties

Differential scanning calorimetry analyses were carried out using a DSC (1 StareSystem, 125 Mettler-Toledo, Inc., Switzerland). Small amounts (5–10 mg approx.) of samples were placed 126 into aluminium pans (Seiko Instruments, P/N SSC000C008) and sealed. Samples were heated 127 from room temperature to 200°C at 10K/min in order to analyse phase transitions in the PLA 128 film. Samples were kept a 200°C for 5min, cooled to -10°C at -50K/min, kept at -10°C for 129 5min and heated again to 200°C at 10K/min; finally they were cooled to 25°C at -100K/min. 130 An empty aluminium pan was used as reference. The same method was used to analyse 131 melting properties of PEG 1000 and PEG 4000. Each sample was analysed in duplicate. 132 A thermo-gravimetric analyser (TGA/SDTA 851e, Mettler Toledo, Schwarzenbach, 133 Switzerland) was used to characterize thermal degradation. The analysis was performed from 134 room temperature to 600°C at 10°C/min under a nitrogen flow (50 mL/min). Each sample was 135 analysed in duplicate. The initial degradation temperature (Tonset), i.e. the temperature at 136 which 5% mass loss is registered, was recorded. The temperature at which the maximum 137 degradation rate was observed (T_{max}) was also determined. Each sample was analysed in 138 duplicate. 139

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2. 3. 3. Microstructure

The microstructural analysis of the cross-sections of the films was carried out by means of a scanning electron microscope (JEOL JSM-5410, Japan). Film pieces, 0.5 x 0.5 cm² in size, were cryofractured from films and fixed on copper stubs, gold coated, and observed using an accelerating voltage of 10 kV. Observations were taken in duplicate for each formulation.

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2. 3. 4. X-ray diffraction

A diffractometer (XRD, Bruker AXS/D8 Advance) was used to record the X-ray diffraction patterns. All the samples were analysed at room temperature, between $2\theta = 5^{\circ}$ and $2\theta = 30^{\circ}$ using K α Cu radiation (λ : 1.542 Å), 40 kV and 40 mA with a step size of 0.05°. For this analysis, samples were cut into 4 x 4 cm². Each sample was analysed in duplicate.

2.3.5. Tensile properties

A texture analyser (TA-XT plus, Stable Micro Systems, Surrey, United Kingdom) was used to measure the mechanical properties of films. Strips of films (25 mm wide and 100 mm long) were mounted in the tensile grips (A/TG model) and stretched at a rate of 50 mm/min until breaking. The elastic modulus (EM), tensile strength at break (TS) and percentage of elongation at break (% ε) were determined from stress-strain curves, obtained from force-deformation data. The experiments were carried out at 25°C and eight replicates were made for each film.

- 162 2. 3. 6. Water Vapour Permeability (WVP) and Oxygen Permeability (OP)
- The WVP of films was measured using a modification of the ASTM E96-95 gravimetric method¹⁹, using Payne permeability cups (Elcometer SPRL, Hermelle/s Argenteau, Belgium) of 3.5 cm diameter. For each formulation, the measurements were replicated four times and the WVP was calculated following the methodology described by Gennadios et al.²⁰, at 25°C and a 53-100% relative humidity (RH) gradient, which was generated using an oversaturated Mg(NO₃)₂ solution and pure distilled water. To determine the WVP, the cups were weighed periodically for 4 days after the steady state was reached using an analytical balance $(\pm 0.00001 \text{ g})$. The slope obtained from the weight loss vs. time was used to calculate WVP, according to ASTM (1995).

The OP of the films was determined by using the ASTM F1927 method²¹, using OXTRAN SL 2/21 MOCON equipment (U.S.A.). Measurements were carried in duplicate at 23°C and 50% RH. Film thickness was considered in all samples to obtain the oxygen permeability values.

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- 2. 3. 7. Optical properties
- 178 The optical properties of the films were determined in film samples by means of a
- spectrocolorimeter (CM-3600d, MinoltaCo., Tokyo, Japan) with a 10 mm diameter window.
- The internal transmittance (T_i) of the films was determined, as an indicator of the
- transparency of the films, by applying the Kubelka-Munk theory²² for multiple scattering to
- the reflection spectra, following the methodology described by Pastor et al.²³.

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- 2. 3. 8. *Ultraviolet*–*visible spectrophotometry (UV–VIS)*
- UV-VIS absorption spectra of the samples $(4.5 \times 1.2 \text{ cm}^2)$ were recorded in the wavelength
- range of 250–700 nm using a Thermo Scientific (Evolution 201) UV–VIS spectrophotometer.

- 2.3.9. Overall migration (OM) in aqueous food simulants
- Overall migration tests were carried out for plasticized and unplasticized films, following the
- current legislation²⁴. Film samples with a total area of 15 cm² were immersed in 25 mL of
- different simulants: simulant A (ethanol 10% in water, simulating foods which are hydrophilic
- in nature) and simulant B (acetic acid 3% in water, simulating hydrophilic foods with pH
- below 4.5). All the samples were kept in contact with the simulants for 10 days at 20°C, to
- simulate any food contact under frozen or refrigerated conditions. After incubation, the film
- samples were removed from the simulants, which were evaporated to dryness. The migration

value in each case was taken as the residue weight. The results were expressed as mg per dm² of film. All the tests were run in duplicate.

2. 3. 10. Statistical analysis

StaTgraphics Plus for Windows 5.1 (Manugistics Corp., Rockville, MD, U.S.A.) was used to carry out statistical analyses of data through an analysis of variance (ANOVA). Fisher's least significant difference (LSD) was used at the 95% level.

3. Results and discussion

3. 1. Characterization of amorphous and crystalline phases of the films.

The degree of crystallization of compression molded films with and without plasticizers was analysed from the first heating scan of DSC, taking the X-Ray diffraction pattern of the films into account. Figure 1 shows the thermograms obtained for both neat PLA films and those containing 5% of plasticizers. Glass transition was observed in all cases, followed by a crystallization exotherm and the subsequent melting endotherm of the polymer. An excess enthalpy of relaxation (ΔH_{ex}) was observed as an endotherm at the glass transition. As observed by other authors for PLA³, this has been associated with the physical aging of the material, since ΔH_{ex} increases as the material ages. Likewise, a small exotherm prior to the melting endotherm was observed in all the samples, which is characteristic of a solid-solid transition²⁵. This corresponds to the disorder-to-order (α' -to- α) phase transition, in which the chain packing of the crystal lattice becomes more ordered. This thermal behaviour of the films indicates that a large part of the polymer is in an amorphous state after compression molding under the conditions applied (fast cooling rate after thermocompression). Then, after glass transition, crystallization occurs when the temperature rises to nearly 100°C. Afterwards, the

polymer melts at about 175°C, but prior to that, the α ' crystal fraction crystallizes into the α form (small exotherm before melting).

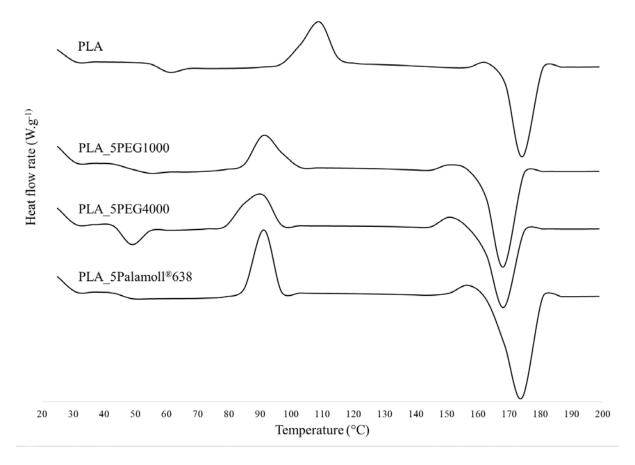


Figure 1. DSC thermograms of neat PLA and PLA with 5% of plasticizers at the first heating.

As shown in Table 1, the onset glass transition temperature (T_{g0}) of PLA significantly decreased after the addition of plasticizers, regardless of their type; the higher the concentration of plasticizer, the greater the decrease in T_{g0} . This indicates that the compounds used effectively plasticize the amorphous phase of the polymer, depending on their concentration, reducing the interchain forces of the polymer and increasing its free volume, thus enhancing the rubbery character. No notable differences in the plasticizing effect of the different compounds used were observed despite their different molecular weight, since a similar T_g decrease was obtained at a determined concentration of each compound. It is

remarkable that, in no case did PEG crystallization occur in the films, as deduced from the DSC curves where no melting of PEG was observed. Melting properties of pure PEG 1000 and PEG 4000, determined by DSC, gave melting temperature values of 38°C and 56°C (within the range of the film analyses) with melting enthalpies of 181 and 210 J/g, respectively. Therefore, a good miscibility of the plasticizers and polymer, at the used ratios, was observed in all cases, exhibiting no phase separation. Table 1 also gives the crystallization temperature (T_c), crystallization enthalpy (ΔH_c), melting temperature (T_m) and melting enthalpy (ΔH_m) , determined from the respective exothermic and endothermic peaks of the registered first heating scan. Taking into account the temperature at which crystallization occurs in the heating step, α and α ' crystals could be formed, according to previous studies about the influence of the temperature on PLA crystallization²⁶. Yasuniwa et al.²⁷ carried out the isothermal crystallization of PLA at various crystallization temperatures and elucidated that the crystallization behaviour discretely changes at crystallization temperatures below and above 113 and 135°C, respectively and a double melting behaviour was observed when crystallization occurred between 113 and 135°C. The observed α'-to-α transition could be partly attributed to the crystalline forms present in the thermocompressed films, in line with the fast cooling applied. In fact, the X-ray diffraction patterns of all the samples (Figure 2) presented the main peak at $2\theta = 16.5$, which is characteristic of the α ' crystals of the PLA, slightly displaced at low angle with respect to the α form $(2\theta = 16.8)^{28}$. A broad amorphous band can also be observed in every sample, in line with the presence of amorphous polymer regions in the films.

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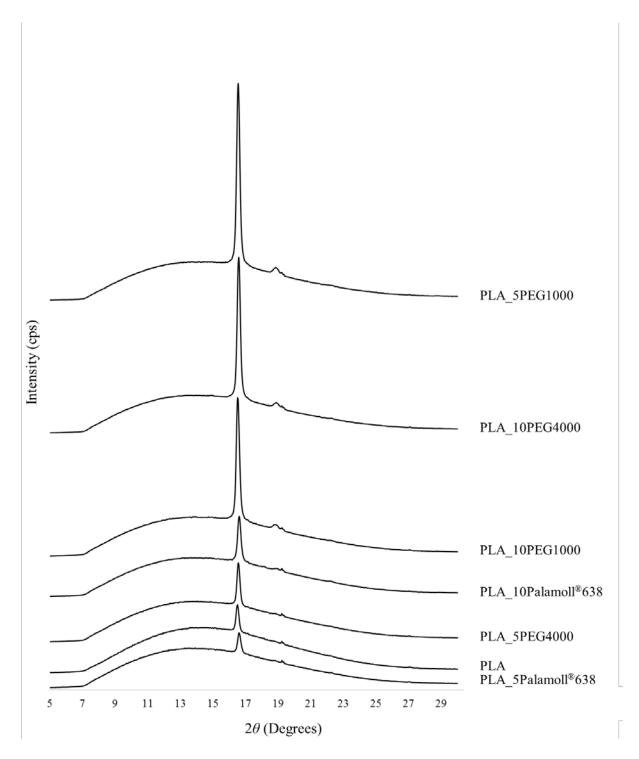


Figure 2. X-Ray diffraction patterns of neat and plasticized PLA films.

The degree of crystallinity of PLA (X_c film (%)) was estimated from the difference between the melting and crystallization enthalpies, by assuming that α crystals were formed, and considering the melting enthalpy of the fully α crystalline PLA phase (ΔH^0_m (α) = 96 J.g⁻¹),

reported by Kalish et al.²⁹. From this estimation (Table 1), a very low crystallinity degree (5%) was obtained in the PLA compression molded films, which notably increased when plasticizers were incorporated. In general, the greater the amount of plasticizer, the higher the degree of crystallinity obtained in the film. Likewise, it is remarkable that PEG 4000 was significantly more effective than PEG 1000 and Palamoll®638 to promote PLA crystallization. The values obtained are coherent with the X-Ray diffraction patterns, which exhibited different relative intensities for the peak at $2\theta = 16.5$. As concerns the melting temperature, films containing Palamoll®638 show a peak value that is very similar to that of the neat PLA film (175°C) whereas significantly lower values were obtained for films with PEG 1000 and PEG 4000, which indicates that the latter plasticizers also interact with the PLA lattice, reducing the melting point of about 5°C. The previous thermal history of the films was erased in the second heating scan in the DSC analysis, but the thermal behaviour was similar to that obtained in the first scan, with the same events appearing on the thermograms, except for the relaxation endotherm at Tg which does not appear because of the newly crystallized polymer. The fast cooling rate applied during the cooling scan (50°C/min) in DSC allowed for reproducing thermal behaviour of the thermocompressed films with their thermal history. The obtained values of T_g, T_c and T_m were similar to those obtained in the first heating scan, as well as the crystallization and melting enthalpy values (Table 2). The crystallization degree which occurred in the fast cooling scan was also estimated by the difference between exo and endo transitions and very small crystallization was determined for the neat PLA films. Nevertheless, crystallinity increased to a greater extent in this step when films contained plasticizers, in line with the promotion of molecular mobility. The higher the plasticizer concentration, the higher the crystallization rate. As observed in the first heating scan, PEG 4000 greatly enhanced PLA crystallization despite the scarce differences induced in the Tg compared to the other used plasticizers. The

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fact that plasticizers promote the crystalline form of thermocompressed PLA can be explained by the T_g reduction, which allows for enhanced molecular mobility at lower temperatures during the cooling step of the film, favouring the polymer chain rearrangement in crystalline forms. In fact, the crystallization temperature for all the plasticized films (Tables 1-2) was lower than for the neat PLA film and the reduction was in line with the $T_{\rm g}$ decrease, since crystallization occurred at 45-50 °C above T_g in every case. These results, valuable for lab scale production of films, could be far from those obtained at industrial level, mainly due to very different times of processing. In industry, the times of processing are considerably shorter and this will have an effect on film crystallinity. Nevertheless, a faster cooling of the polymer melt will lead to more amorphous material, since it is only above Tg that crystallization occurs extensively. The incorporation of plasticizers reduces the Tg and so, extends the time range for polymer crystallization during the cooling step, which suggests that a fast-cooling, quenching process must be implemented to optimize the plasticizer role. Film microstructure (Figure 3) revealed a rather brittle fracture in both plasticized and unplasticized PLA films, exhibiting no plastic deformation, as correspond to the sample fracture conditions, below the Tg values. No phase separation of plasticizers was observed in any case, which confirms the good integration of the compounds into the polymer matrix. Nevertheless, some qualitative differences, reflected in a higher frequency of stripes and white dots, can be observed in the fractured surface of samples with the different plasticizers, which could be attributed to certain local plasticization effect, affecting the fracture behaviour. The thermal stability of the PLA-based films is also coherent with the observed effect of plasticizers. The incorporation of plasticizers should reduce the thermal degradation temperature depending on how much they weaken the polymer network¹⁰, but the increase in

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the degree of crystallization should promote the opposite effect due to the higher energy of the matrix. Table 3 shows the obtained degradation temperatures (onset: T_{onset} and at the maximum rate: T_{max}) for the different films, where very small differences can be observed for the different samples. These range from 317°C to 324°C (onset) and from 337°C to 339°C (max) for all the samples. The opposite effect produced by the plasticizing of the amorphous region and the increase in crystallization only led to scarce changes in the thermo-stability of the films.

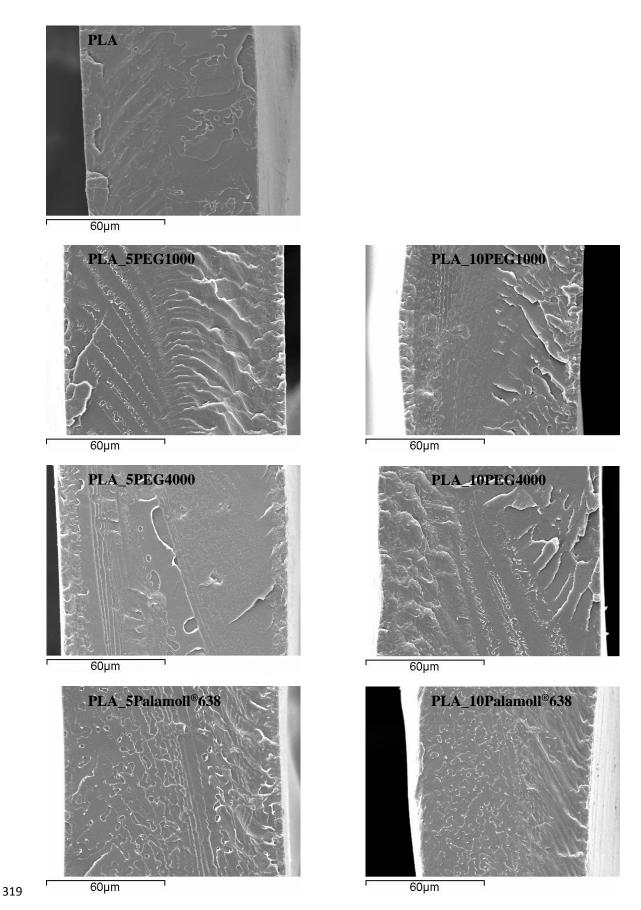


Figure 3. SEM images of the cross-sections of neat and plasticized PLA films.

3. 2. Influence of the changes induced by plasticizers on the film's physical properties

The tensile behaviour of the different PLA films can be observed in Figure 4. All of the plasticizers significantly reduced the film's stretchability, contrary to what was expected from the plasticization effect. The most marked reduction occurred for PEG 4000, whereas Palamoll®638 was the least effective.

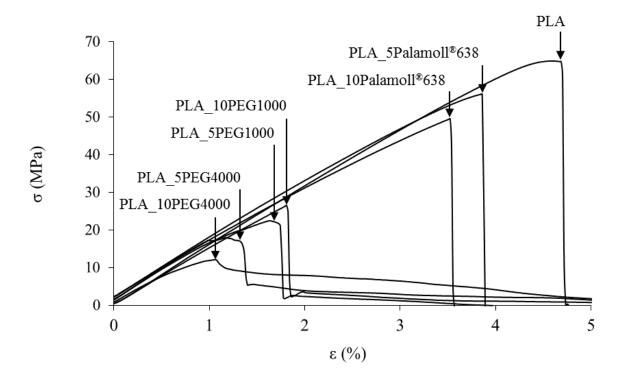


Figure 4. Tensile behaviour of neat and plasticized PLA films.

Table 4 shows the tensile parameters obtained for the different films, where similar values to those obtained by Wang et al.³⁰ can be observed for un-plasticized PLA (about 5%). All the formulations exhibited values of the elastic modulus in the same range, but tensile and deformation at break were notably reduced by the addition of plasticizer. Of the plasticized films, that containing Palamoll[®]638 showed the greatest resistance to break while that containing PEG 4000 exhibited the lowest value. The plasticizer concentration hardly affected

the tensile behaviour for a given compound, although a tendency to reduce the resistance to break when the concentration increased could be appreciated. This effect of the incorporated plasticizers can be explained by the reduction of the interchain attraction forces in the amorphous matrix, while a higher ratio of crystalline domains appeared when the plasticizer concentration increased. A different effect of each plasticizer suggests different molecular interactions between polymer chains and compound molecules. The water vapour permeability of the PLA films slightly increased when plasticizers were added, which can be explained by the decrease in the glass transition temperature of the amorphous phase, which facilitates all of the diffusion controlled processes. However, the reduction in the film barrier capacity will be limited by the increase in the crystalline fraction in the films. On the contrary, OP decreased in plasticized films with 5% of PEG 1000, but increased in the other cases, even overcoming the upper sensitivity limit of the used equipment. This behaviour can be explained by the overall enhancement of the hydrophilic character of the film amorphous phase when PEG 1000 molecules are present at low concentration, although plasticization effect predominates at the highest concentration level. The promotion of hydrophilic character decreases the oxygen solubility in the amorphous phase, thus limiting their permeation capacity. In the case of PEG 4000 and Palamoll®638, more non-polar in nature, the OP was enhanced at the two used concentration levels. On the other hand, all the films were highly transparent when exposed to wavelengths between 400 and 700 nm, as deduced from the high values of the internal transmittance shown in Table 4, and a very slight decrease in transparency with respect to the control film was provoked by the addition of plasticizers. Nevertheless, packaged food products are also submitted to UV irradiation, which may affect both the material and the foodstuff. Different published works have studied the behaviour of PLA films when exposed to UV-vis irradiation. Arrieta et al.³¹ found that cellulose nanoparticles were able to block the UV-light

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when added to PLA-PHB films whereas Cele et al.³² observed that clay nanoparticles reduced the transparency of films but no further discussion was considered in the UV range. For the obtained PLA films, a marked reduction in the UV light transmission was observed when they contained plasticizers as shown in Figure 5.

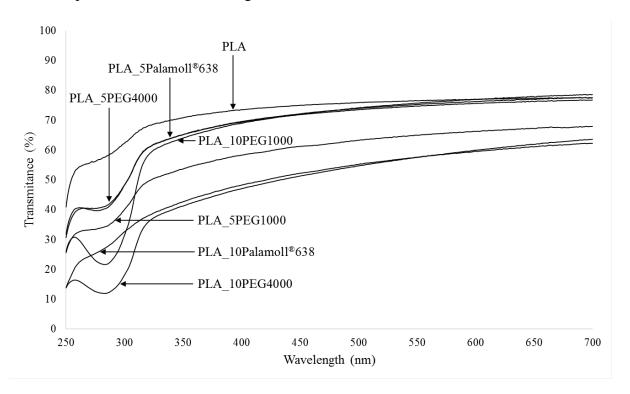


Figure 5. Transmittance of neat and plasticized PLA films in the UV-vis range.

The most significant differences in the film transmittance were found in the UV region, where Palamoll®638 and PEG containing films highly blocked the UV light. The main reduction of the transmittance started approximately at wavelengths below 340 nm, regardless of the formulation, in accordance with the observations of Cele et al.³². The highest blocking effect was found when the plasticizer content was 10%, thus indicating that this effect is directly related to the plasticizer content. Furthermore, both PEG were more effective at reducing the transmission of UV irradiation than Palamoll®638. The UV blocking effect of PEG also observed by Guha et al.³³.

As concerns overall migration of the PLA films in aqueous food simulants, the values of the different samples showed great variability in both A (10% ethanol in water) and B (3% aqueous acetic acid) simulants. This suggests that different factors such as the sample crystallinity degree could affect the total migration, since crystalline zones are usually less soluble than amorphous ones. The relative chemical affinity of plasticizers with the polymer and solvent determines the migration of these compounds to the simulant. In this sense, different migration levels are expected depending on the crystallinity degree of the samples, the type of plasticizer, its amount in the film and the type of simulant. In simulant A, the incorporation of PEG 4000 at 5% significantly decreased the OM levels of the films, whereas 10% Palamoll®638 greatly promoted it. In simulant B, unplasticized PLA exhibited higher migration, which can be attributed to the partial hydrolyses of the polyester and the release of more soluble monomers. However, the incorporation of 5% Palamoll[®]638 and 10 % PEG (1000 and 4000) reduced the migration of the films. In general, the incorporation of the studied plasticizers in PLA matrices, obtained by compression molding, did not enhance the migration of PLA in aqueous food simulants, except when Palamoll[®]638 was used at 10%, where total migration increased in simulant A. In contrast, in the other cases, the plasticizers did not significantly affect the migration capacity of the polymer or decrease it. It is remarkable that only some plasticized PLA films meet the requirements for total migration (10 mg/dm²) established by the EU Commission Regulation 2015/174²⁴ in simulants A and B.

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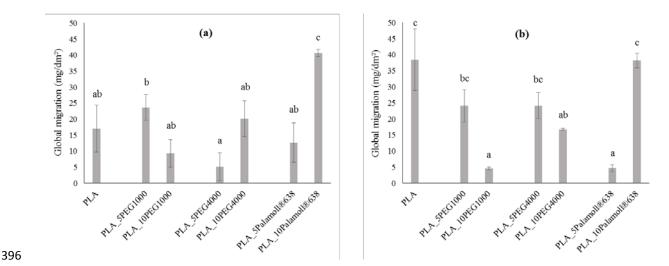


Figure 6. Overall migration values for different films in aqueous food simulants (A: 10% Ethanol (a) and B: 3% acetic acid (b)). Different letters within the same figure indicate significant differences among formulations (p<0.05).

Conclusion

Although a low degree of crystallinity was obtained (5%) in the PLA films obtained by compression molding, crystallization was promoted by the addition of plasticizers (PEG 1000, PEG 4000 and Palamoll®638); the greater their ratio, the higher the degree of crystallinity. All of the plasticizers reduced the glass transition temperature of the film's amorphous phase to a similar extent, proportionally to their concentration. Nevertheless, in no case did this imply an improved film ductility, since all of the plasticized films were less resistant to break and less extensible. The extent of the reduction in these parameters depended on the plasticizer used, Palamoll®638 being the one which promoted the smallest reduction in line with the lower degree of crystallization induced by this compound. So, the studied plasticizers, at 5-10 wt%, were not effective at reducing the film's brittleness, mainly due to the fact that they enhanced the polymer's crystallization at the same time as they reduced the glass transition temperature of the amorphous PLA. Further studies with other potential plasticizing substances would be required, taking into account the potential antagonistic effect of plasticizers, increasing the

- molecular mobility of the polymer chains which, at the same time, can promote polymer
- crystallization, all of which affects the mechanical performance of materials based on PLA.

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Table 1. Thermal data obtained by DSC measurements (first heating scan) for PLA films with different contents of plasticizers. Mean values ±standard deviation.

	T _{g0} ¹ (°C)	T _c ¹ (°C)	ΔH _c ¹ (J/g PLA)	ΔH _{ex} ¹ (J/g PLA)	T _m (°C)	$\Delta H_{\rm m}^{-1}$ (J/g PLA)	X _{c1} ¹ (%)	X _{c2} ¹ (%)	X _c film (%)
PLA	55.6 ±0.4 ^e	108.0 ±0.1 ^d	47.0 ±2.0 ^d	1.4 ±0.1 ab	175.7 ±0.1 ^d	52.3 ±0.3 ^a	49.0 ±3.0 ^d	54.5 ±0.1 ^a	5 ±3 a
PLA_5PEG1000	48.5 ±0.4 ^d	93.7 ±0.1 °	$37.8 \pm 0.2^{\text{ c}}$	3.8 ± 0.3 bc	169.9 ±0.4 b	60.0 ±0.4 °	39.4 ±0.2 °	62.5 ±0.6 °	23 ±1 ^b
PLA_10PEG1000	38.0 ±5.0 ^a	87.0 ±3.0 bc	30.8 ± 1.1 bc	3.0 ±2.0 abc	170.2 ±0.6 ^b	62.8 ±0.3 °	32.0 ±2.0 bc	65.4 ±0.5 °	33 ± 2 cd
PLA_5PEG4000	45.4 ±0.2 bcd	87.5 ±0.4 bc	$32.0 \pm 3.0^{\ bc}$	$4.3 \pm 0.5^{\ bc}$	170.8 ±0.0 ^b	60.5 ±0.3 °	33.0 ±4.0 bc	63.0 ±0.5 °	30 ±3 °
PLA_10PEG4000	$38.4 \pm 1.4^{~ab}$	75.0 ±3.0 ^a	17.0 ±4.0 ^a	$5.0 \pm 1.2^{\text{ c}}$	168.1 ±0.3 ^a	$61.0\pm2.0^{\text{ c}}$	17.0 ±6.0 ^a	63.0 ±3.0 °	46 ±2 e
PLA_5Palamoll®638	$46.2 \pm 1.2^{\ cd}$	91.8 ± 1.4 c	37.0 ±2.0 °	0.3 ±0.1 ^a	174.1 ±0.3 °	56.7 ± 0.5 b	$38.0\pm3.0^{\circ}$	$59.0 \pm 0.8^{\ b}$	21 ±2 ^b
PLA_10Palamoll [®] 638	39.0 ±2.0 abc	81.0 ±4.0 ab	26.0 ±2.0 ^b	$2.4\pm1.0^{~abc}$	173.4 ±0.2 °	62.9 ±0.5 °	27.0 ±3.0 ^b	65.5 ±0.7 °	$38\pm2^{\ d}$

 X_{c1} : degree of crystallization estimated from crystallization exotherm = $\Delta H_c / \Delta H_m^0$

 X_{c2} : degree of crystallization estimated from the melting endotherm = $\Delta H_m / \Delta H_m^0$

 X_c film: deduced from the difference between X_{c2} and X_{c1}

Different superscript letters within the same column indicate significant differences among formulations (p<0.05).

Table 2. Thermal data obtained by DSC measurements (second heating scan) for PLA films with different contents of plasticizers. Mean values ±standard deviation.

	${T_{g0}}^2(^{\circ}C)$	T_c^2 (°C)	$\Delta {H_c}^2 (J/g \; PLA)$	$\Delta {H_{ex}}^2 (J/g \; PLA)$	T_m^2 (°C)	$\Delta {H_m}^2 (J/g \; PLA)$	$X_{c1}^{2}(\%)$	$X_{c2}^{2}(\%)$	X _c cool (%)
PLA	57.1 ±0.1 ^d	108.0 ±0.2 ^d	46.0 ± 1.4^{d}	0.38 ±0.01 °	175.3 ±0.1 ^d	53.1 ±0.3 ^a	48.0 ± 2.0^{d}	55.3 ±0.4 ^a	7 ±2 a
PLA_5PEG1000	45.8 ± 0.2 bc	95.3 ±0.4 bc	39.4 ± 0.7^{cd}	$0.18 \pm 0.02^{\ b}$	169.4 ±0.2 ^b	61.4 ± 0.4 cd	$41.0\pm\!0.8^{~cd}$	63.9 ±0.6 °	$23 \pm 1^{\ b}$
PLA_10PEG1000	36.0 ± 5.0 ab	86.0 ±3.0 ^a	$24.0~\pm 8.0$ b	n.d.	169.1 ± 0.8 b	64.4 ±0.9 °	$25.0 \pm \! 8.0^{\ b}$	67.1 ±0.9 ^d	42 +9 ^d
PLA_5PEG4000	42.0 ± 0.9 abc	90.7 ±0.4 abc	$34.0 \pm 3.0^{\ bc}$	0.09 ±0.02 ^a	170.2 ± 0.1 b	60.1 ± 0.7 bc	$36.0 \pm 5.0^{\ bc}$	$62.6\pm\!0.7^{\ bc}$	27 ± 4 bc
PLA_10PEG4000	$34.0\pm\!5.0^{~a}$	$86.0\pm\!6.0^{~ab}$	7.0 ±3.0 ^a	n.d.	167.5 ±0.5 ^a	$63.0\pm\!2.0^{~cde}$	7.0 ± 4.0^{a}	65.4 ± 3.0 cd	$58\pm7^{\ e}$
PLA_5Palamoll [®] 638	48.3 ± 1.1^{cd}	98.7 ± 0.9 cd	41.4 ± 0.5 cd	$0.18\pm0.01^{\ b}$	173.7 \pm 0.4 $^{\rm c}$	$57.9 \pm 0.2^{\ b}$	43.1 ± 0.7 cd	60.3 ± 0.3^{b}	17 ± 1 ab
PLA_10Palamoll [®] 638	$40.0~{\pm}4.0~^{abc}$	87.0 ±5.0 ^{ab}	$26.6 \pm 0.7^{\ b}$	n.d.	173.0 ±0.2 °	63.2 ± 0.5 de	27.7 ± 0.7 b	65.8 ±0.7 ^{cd}	$38 \pm 1^{\ cd}$

n.d.: non detected

 X_{cl} : degree of crystallization estimated from crystallization exotherm = $\Delta H_c / \Delta H_m^0$

 X_{c2} : degree of crystallization estimated from the melting endotherm = $\Delta H_m / \Delta H_m^0$

 X_c cool: occurred during the cooling step and deduced from the difference between X_{c2} and X_{c1}

Different superscript letters within the same column indicate significant differences among formulations (p<0.05).

T_{max} (°C)
4.0 ±0.5 ^e 339.6 ±0.6 ^c
$.4 \pm 0.2$ cd 338.9 ± 0.4 bc
$.7 \pm 0.5$ bc 337.3 ± 0.2 ab
$.8 \pm 0.3$ ab 337.3 ± 0.2 ab
7.9 ± 0.6^{a} 337.0 $\pm 0.3^{a}$
.5 ±0.1 ^d 338.8 ±0.3 ^{bc}
.3 ±0.6 ^d 338.8 ±1.0 ^{bc}

Different superscript letters within the same column indicate significant differences among formulations (p<0.05).

Table 4. Thickness, tensile parameters (TS, EM, % ϵ), water vapour permeability (WVP: m.g.h⁻¹.Pa⁻¹.m⁻²), oxygen permeability (OP: cm³.m⁻¹.s⁻¹.Pa⁻¹) and internal transmittance (T_i at 600 nm) of films. Mean values \pm standard deviation.

	Thickness (mm)	TS (MPa)	EM (MPa)	ε (%)	WVP	OP x10 ¹²	T_i (%)
PLA	0.136 ±0.008 d	62 ±2 ^f	1583 ±17 ^{cde}	4.4 ±0.2 ^d	0.093 ±0.003 ^a	2.44 ±0.14 ^a	88.96 ±0.02 ^e
PLA_5PEG1000	0.126 ±0.011 b	25 ±4 °	1530 ±50 bc	$1.9\pm0.4^{\ \mathrm{b}}$	0.113 ±0.007 ^{ab}	$1.90 \pm 0.01^{\ b}$	88.79 ± 0.03^{d}
PLA_10PEG1000	$0.129 \pm 0.008 \ bc$	27 ±3 °	1500 ±40 ab	$1.9\pm0.1^{\ \mathrm{b}}$	0.127 ± 0.011 b	> D.L.	88.54 ±0.06 ^b
PLA_5PEG4000	0.119 ±0.009 a	$18\pm7^{\ b}$	1620 ±30 ^e	1.2 ±0.5 ^a	0.115 ±0.010 ab	> D.L.	88.67 ±0.02 °
PLA_10PEG4000	0.117 ±0.010 a	10 ±3 ^a	1400 ± 100^{a}	$1.0~\pm 0.7~^{\rm a}$	0.147 ± 0.002^{c}	> D.L.	88.46 ±0.02 ^a
PLA_5Palamoll®638	0.132 ±0.007 cd	56 ±2 ^e	$1600\pm70^{\text{ de}}$	$3.9\pm0.1^{\text{ c}}$	0.103 ±0.009 ^a	2.90 ±0.60 ^a	88.85 ± 0.04^{d}
PLA_10Palamoll®638	0.129 ±0.009 bc	51 ±3 ^d	1550 ±60 bcd	3.7 ±0.3 °	0.108 ±0.008 ^a	> D.L.	88.80 ±0.05 ^d

D.L.: 200 cm³/m².day

Different superscript letters within the same column indicate significant differences among formulations (p<0.05).