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Additional Information

1	Integration of simultaneous tactile sensing and reflectance visible and near-
2	infrared spectroscopy in a robot gripper for mango quality assessment
3	
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17	
18	ABSTRACT
19	Development of non-destructive tools for determining mango ripeness would improve the
20	quality of industrial production of the postharvest processes. This study addresses the
21	creation of a new sensor that combines the capability of obtaining simultaneously both
22	mechanical and optical properties of the fruit. It has been integrated in a robot gripper that
23	can handle the fruit obtaining non-destructive measurements of firmness, incorporating
24	two spectrometer probes to simultaneously obtain reflectance properties of the visible and
25	near-infrared, and two accelerometers attached to the rear side of two fingers. Partial least
26	square regression was applied to different combinations of the spectra data obtained from

the different sensors to determine the combination that provides the best results. Best prediction of ripening index was achieved using both spectral measurements and two finger accelerometers signals, with  $R_p^2 = 0.832$  and RMSEP of 0.520. These results demonstrate that simultaneous measurement and analysis of the data fusion set improve the robot gripper features, allowing to assess the quality of the mangoes during pick and place processes.

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*Keywords*: spectrometry; chemometrics; non-destructive sensor; tactile sensor;
accelerometer

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### 37 **1. INTRODUCTION**

Mango (Mangifera indica L.) is a tropical fruit marketed throughout the world with a very 38 39 high economic importance (Luke, 2013; Calatrava, 2014) that is generally harvested a little earlier than the fully mature stage to avoid the onset of climacteric respiration during 40 41 transportation to distant markets (Jha et al., 2007). Therefore, mango requires a ripening period before it achieves the taste and texture desired at the time of consumption (Cortés 42 et al., 2016). The ripening process, and hence the organoleptic quality, is regulated by 43 44 genetic and biochemical events that result in biochemical changes such as the biosynthesis of carotenoids (Mercadante & Rodriguez-Amaya, 1998), loss of ascorbic 45 acid (Hernández et al., 2006), increase in total soluble solids (Padda et al., 2011); physical 46 changes such as weight, size, shape, firmness and colour (Ornelas-Paz et al., 2008; 47 Kienzle et al., 2011); and changes in aroma, nutritional content and flavour of the fruit 48 (Giovannoni, 2004). The evaluation of these changes plays an important role for 49 50 determining the ripening level of harvesting, which will decide the market (i.e. domestic, exportation) and/or price of the product. Traditional determination of these changes has 51

required a destructive methodology using specialised equipment, procedures and trained 52 53 personnel, which results in high analysis costs (Torres et al., 2013). In addition, destructive methods allow to analyse only a few set of samples trying to represent the 54 55 variability of the whole production, but this desirable situation can be only achieved if all fruits are inspected in automated lines (Kondo, 2010). Traditionally, electronic sorters 56 based on computer vision, used in postharvest to inspect the quality of the fruit, work at 57 a very high speed, analysing the surface of the fruits not being possible any internal 58 inspection. The most advanced and innovative sorters can incorporate NIR technology 59 for testing the internal properties of the produces but light is projected to the fruit at a 60 61 fixed distance and later, the reflected or transmitted light, is also measured at a certain fixed distance. However, as the fruits have different sizes and shapes, the measurements 62 63 can be strongly influenced by these features. For instance Velez-Rivera et al. (2014a) and 64 (2014b) developed computer vision techniques to determine damages and ripeness of mango 'Manila' trough colour measurements. 65

Robots have enormous potential to automate production in the food sector (Blasco et al., 66 2003; Wilson, 2010). Their main current function is to transport and manipulate objects 67 but they have clear difficulties for handling soft and variable products (Bogue, 2009). 68 69 Advances in new robot grippers are allowing their introduction in industrial and 70 manufacturing systems for monitoring and controlling production (Tai et al., 2016). Automation with robots, in primary packaging operations, makes possible to incorporate 71 different sensors that can be used to assess fruits quality. Tactile sensors added to gripper 72 73 fingers provide the capability to evaluate a product through physical contact (Lee, 1999) and have been used for classifying eggplants (Blanes et al., 2015a) and to assess cv. 74 75 'Osteen' mangoes firmness (Blanes et al., 2015b) with a good prediction performance of the PLS model ( $R_P^2 = 0.760$  and RMSEP = 17.989). 76

Visible and near-infrared spectroscopy combined with multivariate analysis has been 77 78 widely used for quantitative determination of several internal properties or compounds, to determine ripeness, and to measure quality indices in fruits in general and in mango in 79 particular (Schmilovitch et al., 2000; Theanjumpol et al., 2013; Jha et al., 2013; Cortés 80 et al., 2016). Cortés et al. (2016) predicted, in a laboratory, the internal quality index for 81 cv. 'Osteen' mangoes using visible and near-infrared spectrometry (VIS-NIR) obtaining 82 good results with the full spectral range and some selected wavelengths ( $R_p^2 = 0.833$  and 83  $R_{p}^{2} = 0.815$ , respectively). Thus, incorporating the capability of performing spectral 84 measurements to gripper fingers in combination with other sensors would multiply the 85 86 possibilities of measuring internal fruit quality when the fruit is handled. However, this would require to develop sensor fusion techniques to obtain the maximum of the 87 combined information of all the sensors avoiding redundancy (Cimander et al., 2002). 88

89 Furthermore, sensor fusion enables rapid and economical in-line implementation for fruit quality assessment (Ignat et al., 2015). Multiple sensors have been widely used in a 90 91 variety of fields. Steintmetz et al., (1999) developed a robotic quality inspection system 92 for apples that included a colour camera and NIR spectroscopy to predict sugar content using sensor fusion techniques. Since then, significant food advances in the field of sensor 93 94 fusion have been developed among computer vision and near-infrared spectroscopy to 95 assess fish freshness (Huang et al., 2016), fusion of impedance e-tongue and optical spectroscopy to determine the botanical origin of honey (Ulloa et al., 2013), sensor fusion 96 of electronic nose and acoustic sensor to improve the mango ripeness classification 97 (Zakaria et al., 2012) or fusion of electronic nose, near-infrared spectrometer and standard 98 bioreactor probes to monitor yoghurt fermentation (Cimander et al., 2002). Hitherto, 99 100 examples of combination of signals from visible and near-infrared spectroscopy spectral data and tactile sensors in a robot gripper are inexistent. Therefore, getting a sensor fusion 101

system integrating tactile and spectral properties of the fruit would be a key advance forthe post-harvest industry.

Thus, the aim of this study is to develop a novel robotic gripper that incorporates accelerometers and fibre-optic probes coupled to a spectrometer to analyse the mango ripening state by simultaneously measuring firmness and visible and near-infrared reflectance when the fruit is handled in the packing house during postharvest operations.

108

109 2. MATERIALS AND METHODS

# 110 **2.1. Experimental procedure**

A batch of 275 unripe mangoes (Mangifera indica L., cv 'Tommy Atkins') were selected 111 with similar size and colour and free of external damage. During the experiments, fruits 112 were ripened in a storage chamber at  $20.0 \pm 2.1$  °C and  $67.6 \pm 3.3$  % RH and fruits were 113 114 divided in sets of 45 fruits each (sets marked as M1, M2, M3, M4, M5 and M6). Every 2-115 3 days one set was analysed starting with set M1 until the last set M6 reached senescence 116 (18 days). All the mangoes in each set were handled by the robotic gripper to obtain non-117 destructive measurements and later their physicochemical properties (total soluble solids, titratable acidity and destructive firmness) were evaluated. Prior the measurements, the 118 temperature of the mangoes was stabilised at  $24 \pm 1$  °C. 119

## 120 **2.2. Reference analysis**

Routine methods were used to determine the quality attributes of the mangoes. Mango firmness was measured using a Universal Testing Machine (TextureAnalyser-XT2, Stable MicroSystems (SMS) Haslemere, England) through a puncture tests using a 6 mm diameter cylindrical probe (P/15ANAMEsignature) until a relative deformation of 30 %, at a speed of 1 mm s<sup>-1</sup>. Two measurements were performed per fruit, on opposite sides

126 along the equator. The fracture strength ( $F_{max}$ ) expressed in Newtons was also obtained 127 for all samples.

128 The total soluble solids (*TSS*) content was determined by refractometry (%) with a digital 129 refractometer (set RFM330+, VWR International Eurolab S.L Barcelona, Spain) at 20 °C 130 with a sensitivity of  $\pm 0.1$  °Brix. Samples were analysed by triplicate.

The analysis of the titratable acidity (*TA*) was performed with an automatic titrator (CRISON, pH-burette 24, Barcelona, Spain) with 0.5 N NaOH until a pH of 8.1 (UNE34211:1981), using 15 g of crushed mango which was diluted in 60 mL of distilled water. The *TA* was determined based on the percentage of citric acid that was calculated using Eq. (1).

136 
$$TA \left[g \ citric \ acid/100 \ g \ of sample\right] = \left( \left( (A \times B \times C) \cdot D^{-1} \right) \times 100 \right) \cdot E^{-1} \quad (1)$$

where *A* is the volume of NaOH consumed in the titration (in L), *B* is the normality of NaOH (0.5 N), *C* is the molecular weight of citric acid (192.1 g·mol<sup>-1</sup>), *D* is the weight of the sample (15 g) and *E* is the valence of citric acid (E = 3).

140

A multi-parameter ripening index (*RPI*) was calculated by Eq. (2) which was described
previously by Vásquez-Caicedo *et al.* (2005) and Vélez-Rivera *et al.* (2014b). This index
was then used as reference to test the measurements obtained by the robot gripper:

$$RPI = ln(100 \cdot F_{max} \cdot TA \cdot TSS^{-1})$$
<sup>(2)</sup>

where  $F_{max}$  is the fracture strength (Newton), *TSS* is the total soluble solids (g soluble solids per 100 g of sample) and *TA* is the titratable acidity (g citric acid equivalent per 100 g of sample).

148

### 149 **2.3. Robot gripper**

A robot gripper has been specifically developed to handle quasi spherical fruit and 150 programmed in these experiments to work with mango fruits. The gripper has four 151 fingers: FA1, FA2, FB1 and FB2 (Fig. 1). The design of the gripper fingers and its 152 153 mechanical configuration adapt to a wide range of varied shapes while are handled, and provide a good performance of the accelerometers as intrinsic tactile sensors (Blanes et 154 155 al., 2016). The FA2 has hemispherical concave shape, is attached to the chassis of the gripper and is linked by a ball joint. The FA1 is linked to a pneumatic cylinder (DSN 10-156 157 80P, Festo, Germany) with a float joint and has straight motion that is aligned with the FA2. The FB1 and FB2 are linked to their respective pneumatic cylinders (CD85N10-158 159 50B, SMC, Japan) with two float joints and move following parallel paths. FA1, FB1 and FB2 have pads of a latex membrane filled with sesame seeds. Each pad is soft when its 160 161 internal pressure is atmospheric or slightly higher and tough when its internal pressure is 162 lower than atmospheric. The design of these fingers allows the gripper adapting to every 163 mango shape while it is grasped. The gripper was attached to a delta robot (IRB 340, Flexpicker, ABB, Switzerland). 164

165

In addition, the gripper was equipped with two types of sensors, two accelerometers (*ACC1* and *ACC2*) and two reflectance probes (*P1* and *P2*). The signals captured by the sensors were recorded in a laptop by means of a data acquisition module (USB 6210, National Instruments, USA) in the case of accelerometers, and a multichannel VIS-NIR spectrometer platform (AVS-DESKTOP-USB2, Avantes BV, The Netherlands) for the reflectance probes (Fig. 2)..

Accelerometers *ACC1* and *ACC2* were joined to the rear side of the *FA1* and *FA2* respectively. They are intrinsic tactile sensors because they are not in direct contact to every manipulated mango. *P2* was attached to the *FA2* through a hole performed in this finger. It was able to collect data as soon as both *FA1* and *FA2* were closed. Once *FA1* and *FA2* grasp a mango, *P1* approximates by means of the pneumatic cylinder action (C85E10-40, SMC, Japan). This probe was linked to the pneumatic cylinder rod by means of a ball joint. Ball joints allowed the probes adapting to the shape of every different mango since they can rotate freely around three rotation axes.

180 Due to the mechanical configuration of the gripper, the sensors took measurements at181 different points over the surface of every mango (Fig. 3).

182

## 183 **2.3.1. VIS-NIR reflectance signals**

Each reflectance probe consisting of seven fibres with a diameter of 200  $\mu$ m, delivered the light to the sample through a bundle of six fibres, collecting the reflected light trough the seventh one. The probe tip was designed to provide reflectance measurements at an angle of 45° so as to avoid specular reflectance from the surface of the fruit.

The spectra of mango samples were collected in reflectance mode using the multichannel 188 189 spectrometer platform equipped with two detectors and a quartz beam splitter (BSC-DA, 190 Avantes BV, The Netherlands). The first detector (AvaSpec-ULS2048 StarLine, Avantes BV, The Netherlands) included a 2048-pixel charge-coupled device (CCD) sensor 191 (SONY ILX554, SONY Corp., Japan), 50 µm entrance slit and a 600 lines mm<sup>-1</sup> 192 193 diffraction grating covering the working visible and near-infrared (VNIR) range from 600 194 nm to 1100 nm with a spectral FWHM (full width at half maximum) resolution of 1.15 nm. The spectral sampling interval was 0.255 nm. The second detector (AvaSpec-195 196 NIR256-1.7 NIRLine, Avantes BV, The Netherlands) was equipped with a 256 pixel noncooled InGaAs (Indium Gallium Arsenide) sensor (Hamamatsu 92xx, Hamamatsu 197 Photonics K.K., Japan), a 100 µm entrance slit and a 200 lines mm<sup>-1</sup> diffraction grating 198 covering the working NIR range from 900 nm to 1750 nm and a spectral FWHM 199

200 resolution of 12 nm. The spectral sampling interval was 3.535 nm. Two Y-shaped fibre-201 optic reflectance probes (P1 and P2) (FCR-7IR200-2-45-ME, Avantes BV, The 202 Netherlands) were configured each with an illumination leg which connects the fibreoptic probe coupled to stabilised 10 W tungsten halogen light sources (AvaLight-HAL-203 S, Avantes BV, The Netherlands). The light sources ensure a permanent light intensity 204 over the whole measurement range. The other leg of the Y-fibre-optic probe was 205 connected to a beam combiner (BSC-DA, Avantes BV, The Netherlands) which 206 207 converted the two light beams into one light beam. This only light beam was transmitted through another Y-shaped fibre-optic probe to both detectors for simultaneous 208 measurement. 209

The calibration was performed using a 99 % reflective white reference tile (WS-2, 210 Avantes BV, The Netherlands) so that the maximum reflectance value over the range of 211 212 wavelengths was around 90 % of saturation. The integration time was set to 240 ms for 213 the VNIR detector and to 4200 ms for the NIR detector due the different features of both 214 detectors. For both detectors, each spectrum was obtained as the average of five scans to 215 reduce the thermal noise of the detector (Nicolaï et al., 2007). The average reflectance measurements of each sample (S) were then converted into relative reflectance values (R)216 with respect to the white reference using dark reflectance values (D) and the reflectance 217 218 values of the white reference (W), as shown in Eq. (3):

$$R = \frac{S-D}{W-D} \tag{3}$$

The dark spectrum was obtained by turning off the light source and completely coveringthe tip of the reflectance probe.

222 **2.3.2.** Accelerometers signals

The accelerometers used (ADXL278, Analog Devices, USA) have a measurement range
of +/- 50 g. They are capable of sensing collisions and, motoring and control vibration.

225 Only the deceleration signals of the normal axes to the fingers were collected. They were 226 sampled during approximately 0.27 s at 30 kHz and low-pass filtered (Fig. 4a), but only less than 0.1 s were used for analysing the tactile sensor responses. These signals were 227 228 only processed between  $t_0$  (0.0366 s) and  $t_1$  (0.08 s) (Fig. 4b) to capture the first contacts of the gripper fingers with every mango. Signals were rearranged using the maximum 229 values as reference, for hence always maximum values will be at 0.0125 s. Signals also 230 were cut to collect 0.0315 s (Fig. 4c) and were transformed by Fast Fourier Transform 231 232 using LabVIEW 11.0 (National Instruments, USA), with the option measurement magnitude root main square with Hanning window, in order to get energy spreading into 233 234 frequencies (Fig. 4d).

235

## 236 2.4. Robot gripper process and signals acquisition

237 A robot program controls every grasping and sensing operation of the gripper. Three 238 electrovalves (SY3120, SMC, Japan) were used, one for the motion of FA1, one the 239 motion of FB1 and FB2 and other for moving the P2. Two adjustable flowmeter control 240 valves (AS2201F-01-04S, SMC, Japan) were used to adjust the speed of FA1 and P2. A vacuum generator with blow function (VN-07-H-T3-PQ2-VQ2-RO1-B, Festo, Germany) 241 provides the possibility of controlling the hardness of FA1 by means of its internal valves 242 243 2 and 4. The data acquisition device used to collect the accelerometer signals starts to 244 collect data when the robot sends the signal to close FA1.

When the gripper is at the approach position to grasp a mango, valve 1 is activated for closing *FA1*. After 0.3 s, the valve 2 is activated during 0.05 s for changing the pad of *FA1* to a softer state. During this time, valve 1 is deactivated for opening *FA1*. Then, the signals of the valves 1 and 3 are activated for closing the *FA1*, *FB1* and *FB2* during 0.3 s and the pad of *FA1* changes to a tougher state (valve 4 activated) and waits for 0.5 s. This process adapts the pad of the *FA1* to every mango shape. The *P2* starts to collect data.
The robot moves the gripper up. The pad of the *FA1* is at tough state and starts an open/close loop (open during 0.05 s, close for 1 s). During this loop, the signals of *ACC1* and *ACC2* are collected. Then, valve 5 is activated, *P1* is approached to the mango surface and starts to collect data. The whole process is shown in figure 5.

255

## 256 2.5. Signal pre-processing and statistical analysis

The raw spectra from the spectrometer were transformed to apparent absorbance (log (1/R)) values using The Unscrambler Version 10.2 software package (CAMO Software AS, Oslo, Norway) to obtain linear correlations of the NIR values with the concentration of the estimated constituents (Shao *et al.*, 2007; Liu *et al.*, 2009) and centred by subtracting their averages in order to ensure that all results will be interpretable in terms of variation around the mean.

Figure 6 shows raw VNIR and NIR spectra and its correction after the application of the 263 264 pre-processing methods. Savitzky-Golay smoothing (the segment size is 15) was applied 265 to improve the signal-to-noise ratio in order to reduce the effects caused by the physiological variability of samples (Carr et al., 2005; Beghi et al., 2017). Due to the fruit 266 fresh light scattering (Santos et al., 2013), the light does not always travel the same 267 268 distance in the sample before it is detected. A longer light traveling path corresponds to a lower relative reflectance value, since more light is absorbed. This causes a parallel 269 translation of the spectra. This kind of variation is not useful for the calibration models 270 271 and need to be eliminated by the EMSC technique (He et al., 2007; Martens et al., 2003; Bruun et al., 2007). In addition to those three pre-processing, the second derivate with 272 273 Gap-Segment (2.3) were the best results for the NIR spectra because it allowed the 274 extraction of useful information (Rodriguez-Saona et al., 2001). The different pretreatments were applied in the sequence explained, specifying that the first two pretreatments (smoothing and EMSC) were only applied to the VNIR spectra and those two with the third (second derivate) applied to the NIR spectra (Cortés *et al.*, 2016). Finally, the adjustment to the spectral intensities from each sensor ACC1, ACC2, P1 and P2 was range-normalised so the data from all samples were directly comparable to each other (Andrés & Bona, 2005; Blanco *et al.*, 2006).

The different sensor signals were combined through a 'low-level' fusion procedure 281 282 (Roussel et al., 2003) by concatenating the pre-processed sensor signals - appending one to another- to create a single matrix with a total of 5516 variables, which was processed 283 284 using The Unscrambler. Data were organised in a matrix where the rows represent the number of samples (#N = 275 samples) and the columns represent the variables (X-285 variables and Y-variables). The X-variables, or predictors, were the signals obtained by 286 287 the data fusion between the two fibre-optic probes of the spectrometer and the 288 accelerometers. The Y-variable, or response, was the RPI of each sample. In order to 289 correct the relative influences of the different instrumental responses on model, 290 standardisation technique was used, where the weight of each X-variable was the standard deviation of the variable (Bouveresse et al., 1996). Then, fifteen regression models for 291 each combination of the spectra data from the different sensors were developed by partial 292 293 least squares (PLS) to predict RPI. Samples were randomly separated into two groups, 75 294 % of the samples were used to develop the model that was validated by cross validation, while the remaining samples (25 %) were used as the prediction set. The root mean square 295 error of calibration (RMSEC), root mean squared error of cross validation (RMSECV), 296 the root mean square error of prediction (RMSEP), the coefficient of determination for 297 calibration ( $R^{2}_{C}$ ), for prediction ( $R^{2}_{P}$ ) and for cross validation ( $R^{2}_{CV}$ ), and the required 298 number of latent variables (LV) were used to judge the accuracy of the PLS model. 299

300

#### **301 3. RESULTS AND DISCUSSION**

## 302 **3.1.** Changes in mango quality during ripening

303 The changes observed in the physicochemical characteristics ( $F_{max}$ , *TSS* and *TA*) of 304 mangoes during postharvest storage are shown in Table 1.

For all sets of mangoes there was a steady decrease in fruit firmness over time starting 305 306 around 137 N to fell to 28 N. These changes are due to significant changes in the 307 composition and structure of cell walls and middle lamella due to the solubilisation, de-308 esterification and de-polymerisation of the middle lamella (Singh et al., 2013), and the enzymatic activity (Prasanna et al., 2007; Yashoda et al., 2007). A similar behaviour has 309 310 been reported for other mango varieties such as 'Alphonso' (Yashoda et al., 2005), 311 'Ataulfo' (Palafox-Carlos et al., 2012), 'Keitt' (Ibarra-Garza et al., 2015) or 'Osteen' (Cortés et al., 2016). Similarly, the TA tends to decrease due to the cell metabolisation of 312 volatile organic acids and non-volatile constituents (Padda et al., 2011), and in addition 313 acids can be used as substrates for respiration when sugars have been consumed or 314 participated in the synthesis of phenolic compounds, lipids and volatile aromas (Abu-315 316 Goukh et al., 2010). In contrast, the TSS increased continuously during postharvest storage due to the conversion of starch to glucose and fructose, which are used as 317 substrates during fruit respiration (Eskin et al., 2013). Similar results were observed by 318 319 Quintana et al. (1984) who reported that TSS of mango increased gradually up to ripeness. RPI was calculated for every day of storage. Figure 7 shows the evolution of the RPI 320 through median plots with 95 % confidence intervals during the storage. It can be 321 322 observed that the values of the index clearly decreased during ripening. Initially, the RPI declines sharply when the fruits ripen to achieve their optimum organoleptic properties, 323 and then, fruit reaches the stage of over ripeness where the curve follows a constant trend 324

because the product reaches a maximum content of *TSS* and minimum firmness and *TA*.

326

## 327 **3.2.** Non-destructive prediction of mango ripening

The data was concatenated (accelerometers and VIS-NIR spectra) (Decruyenaere *et al.*, 2009; Roussel *et al.*, 2003) to form a representative complex spectrum with a total of 5516 variables. Table 2 shows the results of the validation and prediction results of the PLS models built for the data obtained by every single sensor and for the data fusion (due to the concatenation of wavenumber) performed among all possible combinations of spectral data.

The best PLS model for prediction of *RPI* is presented in the Fig. 8. Figure 9 shows the regression coefficients of the best developed model and the PRESS plot for identifying the optimum number of LVs. The results for this model were obtained using VIS-NIR fibre-optic probes and the two accelerometer signals. The calibration model for predicting the RPI has an  $R^2_c = 0.945$  and RMSEC = 0.235, and the validation of the calibration model has an  $R^2_{cv} = 0.0.804$  and RMSECV = 0.447. The prediction model indicates a good prediction performance, and obtained values of  $R^2_p = 0.832$  and RMSEP = 0.520.

341

# 342 3.3 Integration of tactile sensing and reflectance data in the robot gripper

This novel gripper presents an important evolution from other previous grippers for sensing and handling the firmness of eggplants and mangoes by using accelerometers as tactile sensors (Blanes *et al.*, 2015a and 2015b). Unlike these previous grippers that caused damages in some over-ripe mangoes due to the action of a suction cup needed for holding the fruits, this new gripper incorporates four fingers and intrinsic sensors that avoid the need of such suction cup when holding the fruit for measurement and placing.

Besides, the combination of the two probes achieved better results than P2 or P1 349 standalone, having an  $R_{p}^{2}$  of 0.802 compared to those obtained of 0.732 and 0.632, 350 respectively. In the same way, ACC1 together with ACC2 had better result than ACC1 or 351 ACC2 alone with an  $R_p^2$  of 0.655 compared to 0.444 and 0.300, respectively. It is 352 important to remark that the composition of a fruit is not uniform and hence some parts 353 354 of the mango may have different ripeness than others. Therefore, it is necessary to take 355 simultaneous measurements at least in the three points studied to obtain reliable and 356 robust results. Blanes et al. (2015b) developed a gripper with three accelerometers to estimate the ripeness of mangoes cv. 'Osteen' achieving a  $R^2_P = 0.760$  which is lower 357 than the current robot gripper ( $R^{2}_{P} = 0.832$ ). This highlights the important contribution of 358 the integration of both tactile sensors and VNIR reflectance measurements in the robotic 359 360 gripper to assess the quality of the mangos during fruit handling.

361 A handicap of this system in the current version is the long time needed to process every mango. The incorporation of two spectrometer probes increases the processing time of 362 363 every mango up to 9 s. However, experiments have been done in a first prototype for 364 testing, where the algorithms, hardware and processes were not optimised for working at high speed. Integrating better the hardware, optimising algorithms and parallelising some 365 366 processes, the whole process could experience a dramatic reduction of the operation 367 speed. On the other hand, the combination of sensors of different nature provides the capability of obtaining simultaneously both mechanical and optical properties of the fruit. 368 This innovative approach is highly interesting in the emerging competitive food sector 369 370 where monitoring of product quality reproducibility and traceability is decisive in the 371 manufacture (Kondo, 2010).

372

## 373 4. CONCLUSIONS

A novel sensorised robot gripper with two accelerometers and two VIS-NIR reflectance 374 375 probes, has been developed and tested for fruit handling. The design uses sensors that do not need direct contact, are intrinsic tactile sensors, and can take the measurements 376 377 simultaneously during the mango handling which is an important advantage over the state of the art. The results show the prediction of the quality of the fruit using the *RPI* through 378 the information given by VIS-NIR spectra and non-destructive impact obtained during 379 handling, achieving an  $R_p^2$  of 0.832 and RMSEP of 0.520. This innovative prototype 380 381 integrates different types of sensors of different nature, whose data information is combined to obtain better prediction. The fusion of different types of sensors like 382 383 spectrometry (electromagnetic) and accelerometers (vibrational) achieved better results that using only the accelerometers, or similar results than using spectroscopy, but in this 384 385 case, the measurements were made while the fruit was handled. In this way, results show 386 the potential and advantages of performing simultaneous operations of sensors of different nature integrated on a robot gripper that can inspect and classify the mangoes 387 388 by their ripeness during a pick and place robot process.

389

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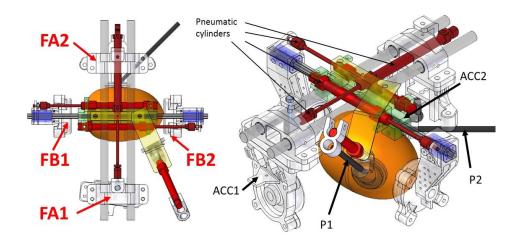
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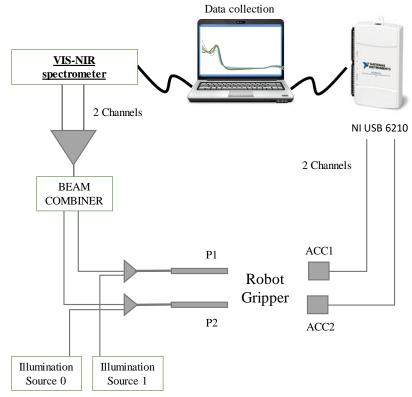
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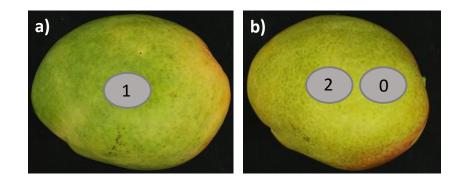
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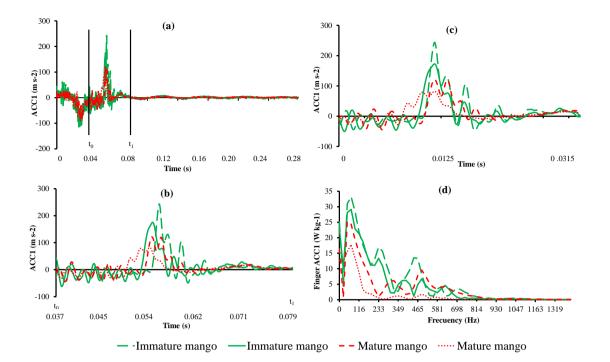
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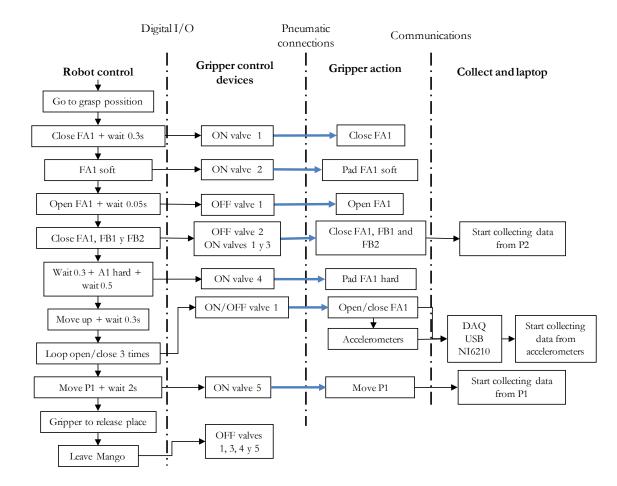


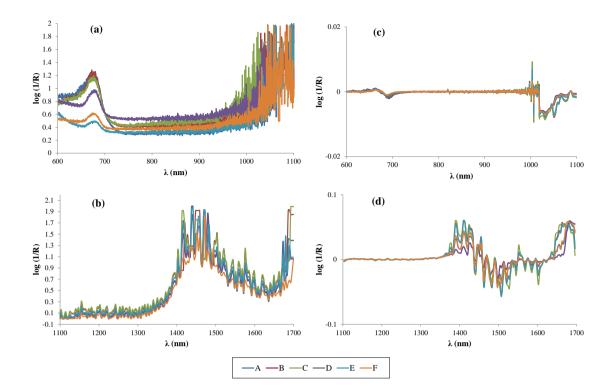


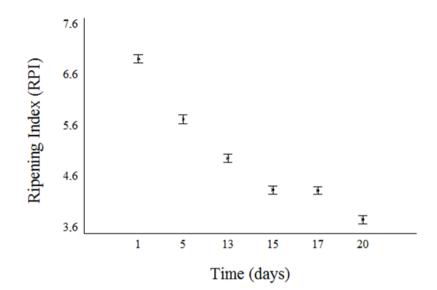
Tungsten halogen light sources

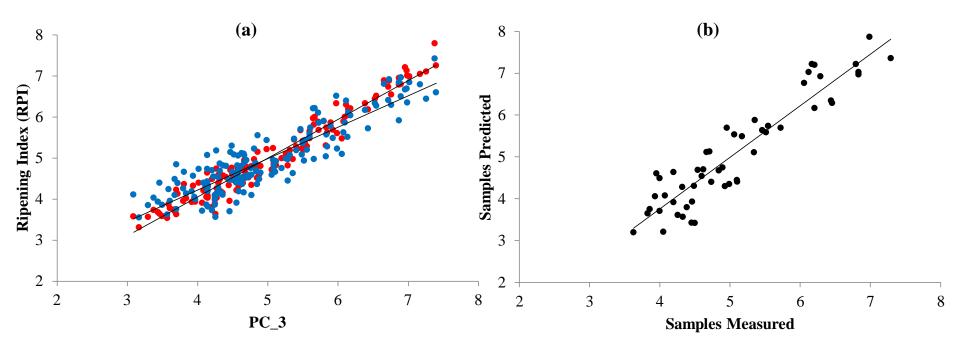


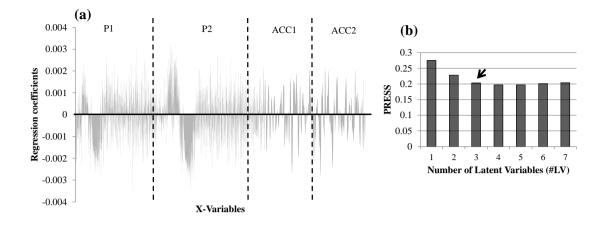












		Set A	A Set B	Set C	C Set I	D Set I	E Set F
Mechanical properties	F <sub>max</sub> (N)	137±18ª	62±16 <sup>b</sup>	45±16°	34±11 <sup>d</sup>	$35 \pm 8^{d}$	28±8e
nal sition	TSS (%)	10.4±0.9ª	12±1 <sup>b,c</sup>	12±1 <sup>c,d</sup>	12±1 <sup>d</sup>	12±1 <sup>b</sup>	12±2 <sup>b,c</sup>
Internal composition	TA (%)	$0.8{\pm}0.2^{a}$	$0.62{\pm}0.15^{b}$	0.41±0.08 <sup>c</sup>	$0.30{\pm}0.06^{d}$	$0.29{\pm}0.06^{d}$	0.19±0.05 <sup>e</sup>

Table 1. Descriptive statistics for the quality parameters analysed in mango samples during the storage period.

Values are mean  $\pm$  SD. a–e Different superscripts in the same row indicate significant difference among sets (p < 0.05).

**Table 2.** Comparison of the prediction of mango ripening provided by different possible

 combination of sensor fusion to the two fibre-optic probes of VIS-NIR spectrometer and

		Calibration set				Prediction set	
Sensors	#LV	R <sup>2</sup> <sub>C</sub>	RMSEC	R <sup>2</sup> <sub>CV</sub>	RMECV	R <sup>2</sup> <sub>P</sub>	RMSEP
P2	1	0.769	0.506	0.742	0.537	0.732	0.663
P1	3	0.895	0.323	0.739	0.512	0.632	0.727
<i>P2+ P1</i>	3	0.933	0.268	0.782	0.487	0.802	0.554
ACC1	6	0.677	0.574	0.575	0.663	0.444	0.871
ACC2	4	0.611	0.626	0.48	0.727	0.300	1.020
ACC1 + ACC2	4	0.758	0.758	0.595	0.595	0.655	0.737
P2+ ACC1	2	0.854	0.373	0.77	0.471	0.778	0.613
<i>P2+ACC2</i>	1	0.695	0.586	0.649	0.632	0.733	0.665
P1 + ACC1	4	0.940	0.251	0.753	0.513	0.662	0.698
P1 + ACC2	5	0.971	0.175	0.776	0.493	0.662	0.742
P2 + P1 + ACC1	4	0.973	0.166	0.786	0.467	0.797	0.550
P2 + P1 + ACC2	2	0.867	0.379	0.777	0.494	0.784	0.595
P2 + ACC1 + ACC2	2	0.813	0.460	0.705	0.580	0.813	0.567
P1 + ACC1 + ACC2	5	0.971	0.176	0.779	0.490	0.733	0.642
P2 + P1 + ACC1 + ACC2	3	0.945	0.235	0.804	0.447	0.832	0.520

two accelerometers located at the fingers of the robot gripper.