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Valencia-Sullca, CE.; Atarés Huerta, LM.; Vargas, M.; Chiralt, A. (2018). Physical and Antimicrobial Properties of Compression-Molded Cassava Starch-Chitosan Films for Meat Preservation. Food and Bioprocess Technology. 11(7):1339-1349. doi:10.1007/s11947-018-2094-5



The final publication is available at http://doi.org/10.1007/s11947-018-2094-5

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Additional Information

- 1 Physical and antimicrobial properties of compression-moulded cassava starch-
- 2 chitosan films for meat preservation.
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Abstract

9 Cassava starch-chitosan films were obtained by melt bending and compression 10 moulding, using glycerol and polyethylene glycol as plasticizers. Both the 11 starch:chitosan and the polymer:plasticizer ratios were varied in order to analyse their 12 effect on the physical properties of the films. Additionally, the antimicrobial activity of 13 70:30 polymer:plasticizer films was tested in cold-stored pork meat slices as affected 14 by chitosan content. All film components were thermally stable up to 200 °C, which 15 guaranteed their thermostability during film processing. Starch and chitosan had limited miscibility by melt blending, which resulted in heterogeneous film microstructure. 16 Polyethylene glycol partially crystallized in the films, to a greater extent as the chitosan 17 ratio increased, which limited its plasticizing effect. The films with the highest plasticizer 18 19 ratio were more permeable to water vapour, less rigid and less resistant to break. The 20 variation in the chitosan content did not have a significant effect on water vapour 21 permeability. As the chitosan proportion increased, the films became less stretchable, 22 more rigid and more resistant to break, with a more saturated yellowish colour. The 23 incorporation of the highest amount of chitosan in the films led to the reduction in 24 coliforms and total aerobic counts of cold-stored pork meat slices, thus extending their shelf-life. 25

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Keywords: thermoplastic starch, microstructure, thermal analysis, mechanical properties, antimicrobial.

1. Introduction

31 In recent years, increasing interest in biodegradable materials has developed mainly 32 due to concerns over the disposal of conventional synthetic plastic materials derived from petroleum, which take a long time to be degraded (Fang et al., 2005). 33 Starch has been widely used for the preparation of biodegradable films because of its 34 35 abundance, low cost, renewable nature, biocompatibility and non-toxicity (Carvalho, 36 2008). Native starch can be converted into thermoplastic starch by the disruption of the 37 polymeric chains interactions, under specific conditions of temperature and /or mechanical energy, in the presence of a plasticizer (Tomé et al., 2012). In order to 38 39 obtain thermoplastic starch, scaling-up processing methods using equipment designed 40 for synthetic polymers is indispensable (Thunwall et al., 2006). For example, extrusion, 41 blowing, injection and thermocompression are viable alternatives due to their energy-42 efficiency and high productivity (Pelissari et al., 2012). As opposed to casting, these 43 techniques are suitable for film production at industrial scale (Tomé et al., 2012). 44 Starch-based films exhibit low oxygen permeability (Jiménez et al., 2012a). However, they show several disadvantages, which reduce their applicability as packaging 45 material, such as their highly hydrophilic character, limited mechanical properties and 46 47 the retrogradation phenomena that occur during aging (Ortega-Toro et al., 2015). The 48 use of plasticizers reduces the interchain forces associated to hydrogen bonds, 49 enhancing molecular mobility, which helps to overcome film brittleness, making the film 50 more extensible. 51 Aiming to improving its film-forming performance, starch has been combined with both 52 synthetic and natural polymers. Amongst them, chitosan has led to positive results in films obtained by casting (Chillo et al., 2008; Bonilla et al., 2013) and by thermal 53 processing (López et al., 2014; Mendes et al., 2016). Incorporating chitosan into 54 55 starch-based films has been reported to reduce their water affinity and improve their 56 mechanical properties, due to the formation of intermolecular hydrogen bonds between

57 the amino and hydroxyl groups of chitosan and the hydroxyl groups of starch (Xu et al., 2005). Moreover, chitosan provided the starch-chitosan blend films obtained by casting 58 59 with antibacterial properties (Bonilla et al., 2013). However, to the best of our 60 knowledge, the studies on the antimicrobial performance of thermoplastic starchchitosan films for food preservation are still scarce. 61 The aim of this work was to characterize the microstructural, tensile, barrier and optical 62 properties, as well as the thermal behaviour of starch-chitosan films obtained by 63 64 compression-moulding as affected by the polymer:plasticizer and the starch:chitosan 65 ratios. The effect of chitosan content on the antimicrobial activity of the films was also 66 evaluated in cold-stored pork-meat slices.

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2. Materials and methods

69 2.1. Materials

70 Cassava starch (CS) with 9.28 % amylose and an amylose: amylopectin ratio of 1:9.8, 71 was produced by Asia CO, LDT (Kalasin, Thailand) and purchased by Quimidroga SA 72 (Barcelona, Spain). Chitosan (CH) of high molecular weight (practical grade, >75% 73 deacetylation degree, Batch MKBP1333V) and polyethylene glycol 4000 (PEG) were purchased from Sigma-Aldrich (Madrid, Spain). Glycerol (Gly) and Mg(NO₃)₂ were 74 75 provided by Panreac Química, S.A. (Castellar del Vallés, Barcelona, Spain). Pork meat 76 was purchased in a local supermarket and processed at the laboratory. Buffered 77 peptone water, Violet Red Bile Agar and Plate Count Agar were provided by Scharlau 78 (Barcelona, Spain).

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80 2.2. Film preparation

Eight formulations based on CS, CH, with Gly and PEG as plasticizer (P), were prepared. In all cases, plasticizers were mixed in a constant Gly: PEG mass ratio 75:25. Two series of formulations were prepared with polymer: plasticizer mass ratios 70:30 and 60:40. In each series, CS:CH mass ratios were 100:0, 90:10, 80:20 and 85 70:30. After weighing, CS, CH and plasticizers were dispersed in distilled water. The formulations were melt-blended on a two roll mill (Model LRM-M-100, Labtech 86 87 Engineering, Thailand) at 160 °C and 10 rpm for 30 minutes until a homogeneous paste 88 was obtained. Before compression moulding, the paste was conditioned at 25 °C and 53% relative humidity (RH) using Mg(NO₃)₂ oversaturated solutions for 72 h. The films 89 were obtained by compression moulding (Model LP20, Labtech Engineering, Thailand). 90 91 Four grams of the paste were put onto steel sheets and preheated on the heating unit 92 for 5 min. The films were performed at 160 °C for 2 min at 5 MPa (50 bar), followed by 93 6 min at 12 MPa (120 bar); thereafter, a cooling cycle (40 °C/min) was applied for 3 min. The films obtained were conditioned at 25 °C and 53% RH for 1 or 5 weeks before 94 95 characterization.

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- 2.3. Characterization of the films
- 98 2.3.1. Microstructural analysis
- The microstructural analysis of the cross-sections of the films was carried out by
 means of scanning electron microscope (JEOL JSM-5410, Japan, model JSM-5410).

 The film samples were maintained in desiccators with P₂O₅ in order to eliminate film
- The film samples were maintained in desiccators with P_2O_5 in order to eliminate film moisture. Film pieces (5x5 mm approximately) were cryofractured and mounted on cupper stubs. After gold coating, the samples were observed using an accelerating
- 105 2.3.2. Thermogravimetric analysis

voltage of 10 kV.

The thermal stability of the films and their components was analysed using a thermogravimetric analyser (TGA/SDTA 851e, Mettler Toledo, Schwerzenbach, Switzerland), equipped with an ultra-micro weighing scale (±0.1 μg), under nitrogen flow (50 mL/min). The analysis was carried out during heating from 25 to 600 °C at 10 °C /min. Approximately 3 mg of sample were used in each test, considering at least two replicates per formulation. Initial degradation temperature (T₀), i.e. the temperature at

- which 10% mass loss is registered, and maximum degradation rate temperature
 (Tmax) were registered.
- 2.3.3. Differential scanning calorimetry
- The thermal properties were analysed using a differential scanning calorimeter (DSC 1
- Star System, Mettler- Toledo, Inc., Switzerland) with a 20 mL/min nitrogen flow. Film
- samples were desiccated with P₂O₅ and crushed with a mortar. Two samples
- (approximately 10 mg) per formulation were placed into aluminium pans and sealed.
- An empty sample pan was taken as a reference. A first heating step was done from 0
- °C to 160 °C at 50 °C/min to remove any residual water, followed by a cooling step to 0
- °C at the same speed, and a second heating to 200 °C at 10 °C /min.
- 2.3.4. Moisture content and water vapour permeability
- The moisture content of film samples previously conditioned at 53% RH was
- determined by the gravimetric method. Five samples per formulation were considered.
- 125 Water was eliminated from them using a two-step method: desiccation in a vacuum
- oven (60 °C 24 h), and storage in desiccators with P₂O₅ until constant weight was
- reached. The results were expressed as g of water per 100 g of dry film.
- The water vapour permeability (WVP) of the film samples was determined by means of
- the ASTM E96-95 gravimetric method (ASTM, 1995), as described by Ortega-Toro et
- 130 al. (2014).
- 131 2.3.5. Mechanical properties
- A universal test machine (TA-XT plus, Stable Micro Systems, Surrey, United Kingdom)
- was used to determine the elastic modulus (EM), tensile strength at break (TS) and
- percentage of elongation at break (%E) of the film samples. These parameters were
- obtained from stress-Hencky strain curves, following ASTM standard method D882
- 136 (ASTM, 2001). Ten film stripes (25 mm wide and 100 mm long) per formulation were
- tested. Film thickness was measured in four positions along the stripe to the nearest
- 138 0.0025 mm with a hand-held digital micrometer (Electronic Digital Micrometer,
- 139 Comecta S.A., Barcelona, Spain). Equilibrated samples were mounted in the film-

140 extension grips of the testing machine and stretched at 50 mm min⁻¹ until breaking. The relative humidity of the environment was held constant, at approximately 53% 141 142 during the tests, which were performed at 25 °C. 143 2.3.6. Optical properties 144 The surface reflectance spectra of the films were obtained from 400 to 700 nm with both a white and a black background by using a spectrocolorimeter (CM-3600d, 145 146 Minolta CO., Tokyo, Japan). The Kubelka-Munk theory for multiple scattering was 147 applied to the reflection spectra to determine internal transmittance (T_i) (Hutchings, 148 1999). Lightness (L*), chroma (C^*_{ab}) and hue (h^*_{ab}) values of the films were obtained from the surface reflectance spectra, taking into account illuminant D65 and observer 149 150 10°. Whiteness index (WI) was calculated according to Atarés et al. (2010). The gloss 151 was determined at a 60° incidence angle by means of a flat surface gloss meter (Multi 152 Gloss 268, Minolta, Germany), following the ASTM standard D523 method (ASTM, 153 1999). The measurements of each sample were taken in triplicate and four films were 154 measured per formulation. The results were expressed as gloss units (GU), relative to 155 a highly polished surface of black glass standard with a value near to 100 GU. 156 2.3.7. Antimicrobial properties 157 Films were tested for their antibacterial properties using sliced pork meat and following 158 a methodology adapted from Bonilla et al. (2014). Each test sample was obtained by 159 placing 10 g of meat in a petri dish (5 cm diameter), and coating with the films. Non-160 coated samples (control) and samples coated were stored in duplicate at 10 °C for 7 days. To perform the microbiological analyses, each sample was homogenized in a 161 162 Stomacher (Bag Mixer 400, Interscience) with 90 mL of sterile buffered peptone water 163 for 2 min. Then, serial dilutions were made and plated out. Total viable and coliform microorganism counts were determined at 0, 1, 4 and 7 days. Total aerobic counts 164 were determined in Plate Count Agar incubated at 37 °C for 48 h, while coliforms were 165 determined in Violet Red Bile Agar incubated at 37 °C for 48 h. All tests were made in 166 167 triplicate.

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2.4 Statistical analysis

Results were statistically analysed through the analysis of variance (ANOVA) with a 95% significance level. The analyses were performed by using Statgraphics

Centurion® version XVI. II. Multiple comparisons were performed by means of 95%

Fisher's least significant difference (LSD) intervals.

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3. Results and discussion

3.1. Microstructural analysis

Figure 1 shows the micrographs of the cross-section of the films after a 1-week storage period at 25 °C and 53% RH. Films showed a quite homogenous structure where no starch granules were observed, which indicates that starch was gelatinized during the roller mill step. Nevertheless, all samples exhibited micro-cracks, which reflects the sample fragility after desiccation with P₂O₅. The increase in the plasticizer content did not change this behaviour. Incorporation of chitosan into the film matrix was not homogenous due to the lack of miscibility of polymers by melt blending. Although a homogeneous matrix was obtained when starch-chitosan blend films were obtained by casting the aqueous solutions of both macromolecules at different ratios (Bonilla et al., 2013), no total compatibility of polymers was obtained in dry conditions. This may be due to difficulties in the melt blending, where the much higher viscosity of the medium and the difficulties for chain extension inhibit the establishment of adequate interactions between the polymer segments. Therefore, some flakes with different sizes of chitosan in the starch matrix can be observed in samples regardless the ratio of chitosan. These were observed in different zones of the films with a random distribution. Even at the lowest chitosan ratio, immiscibility of melt polymers was evident.

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3.2 Thermogravimetric analysis

The mass loss curves of the films showed three separate steps (Figure 2). The first step corresponded to the initial weight loss attributed to the loss of water, being the mass reduction (about 10-15%) coherent with the water content of the films. The second step at around 200 °C was attributed to the degradation of glycerol (Dou, Dupont, Williams, Chen and Ding, 2009). The third highest mass loss step appeared at about 320 °C and corresponded to the degradation of the polymers. Table 1 shows the values of the initial degradation temperature (T₀) and maximum degradation rate temperature (T_{max}) of the films components and films, as well as the percentage mass loss of all samples at the end of the TGA test (600°C). The T_{max} values of the pure compounds (native CS, CH, Gly and PEG) were 321°C, 302°C, 251°C and 407°C, respectively. Similar results have been reported previously (Dou et al., 2009; Pelissari et al., 2009). Therefore, the T₀ values of all film components were higher than 200 °C, which guarantees their stability in the elaboration of the films by compression moulding. The addition of chitosan up to the mass ratio 70:30 (CS:CH) did not affect the thermal stability of the films. Both pure polymers showed similar degradation pattern and their blend degradation were mainly affected by the presence of plasticizers. Degradation process in the blend films was more extended, starting at lower temperature due to the early glycerol degradation. Pelissari et al. (2009) also reported similar T_{max} values for cassava starch-chitosan films produced by extrusion. The reported values of T₀ and T_{max} of the starch films, regardless the plasticizer proportion, were similar to those reported for corn starch and cassava starch films obtained by compression moulding and extrusion (Ortega-Toro et al., 2014; Dang, & Yoksan, 2015). Additionally, it was observed that, as chitosan proportion was increased in the film formulation, the percentage mass loss at 600 °C was reduced, in agreement with the greater mass residue of CH. This is coherent with previous studies on cassava starch-chitosan films

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(Dang & Yoksan, 2015).

3.3. Differential scanning calorimetry

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Table 2 shows the thermal properties (T_m, ΔH_m and% crystallinity of PEG) of the studied films conditioned for 1 week at 25 °C and 53% RH, along with those of pure PEG. No glass transition or melting of polymers were observed in the temperature range analysed, but both in the first and the second heating steps, a melting endotherm attributable to PEG was observed at the temperatures (T_m) reported in Table 2, with the corresponding ΔH_m values. Pure PEG sample shows an endothermic peak at 62.5 °C, with a melting enthalpy of 194 J/g. Similar results were obtained by Song, Xue, He, Liu, & Xiao (2008). Over the first heating step of the film samples, this endotherm was observed at slightly lower temperatures, the T_m values ranging between 56 °C and 61 ^oC. T_m reduction was also observed over the second heating step when the thermal history of the sample had been deleted. This reduction in the melting temperature, with respect to that of pure PEG, suggests that some film components are partially miscible with PEG, depressing its melting point, coherently with previous reports (Song et al., 2008). In a compatible blend, the melting temperature of one component is often reduced owing to the increasing of lattice defects resulted from the partial miscibility of the noncrystalline phase. The crystallization degree of PEG in the films was estimated from the enthalpy values of pure compound assuming complete crystallization in this case. In general, crystallization degree increased when the CH ratio rose in the film, which could be related with the interactions between these components. Nevertheless, sample with the highest CH ratio and 40% plasticizers exhibited the lowest crystallization degree. Higher plasticization promoted molecular mobility and so the polymer crystallization. The PEG crystallization in the films limited its plasticizing effect since the crystallized fraction was in a separated phase without interactions with the polymer chains. Then, the reduction of PEG ratio in the films should be considered.

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3.4. Thickness, moisture content and water vapour permeability

251 Table 3 shows the values of thickness along with water vapour permeability (WVP) and moisture content data for 1 and 5-week storage period at 53% RH-25 °C. 252 253 As can be observed, the film thickness increased when CH was incorporated into the 254 film (from 170 µm to 260 µm). Similar results were reported by Pelissari et al. (2009) 255 and López et al. (2014) studying starch and chitosan films obtained by extrusion. As 256 observed in Figure 1, the partial incompatibility of both polymers led to more 257 heterogeneous structures while blend films were also thicker. The increase in the film 258 thickness, associated with the rose in CH ratio, may be attributed to the lower 259 flowability of the chitosan melt (with higher viscosity) as compared to the starch melt, 260 which limits the blend extension during compression moulding. 261 The moisture content values ranged between 10 and 15 g water / 100 g dry film. It was 262 significantly increased after 5 storage weeks (p <0.05), indicating that films equilibrate 263 slowly with the ambient relative humidity, even though storage time did not affect WVP significantly. Similar results have been reported previously by Ortega-Toro et al. (2014) 264 265 for CS-HPMC films obtained by compression moulding, and by Jiménez et al. (2012b) 266 in CS- fatty acids films obtained by casting. In these studies, storing the films for 5 weeks resulted in a significant increase (p <0.05) in the film moisture content with no 267 268 effect on the WVP values, regardless of the film composition. Very small differences in 269 the moisture content of the films were observed for the different CS:CH ratios, although 270 the increase in the plasticizer content promoted moisture uptake. 271 The polymer: plasticizer ratio had a significant effect (P* <0.05) on both the moisture 272 content and WVP values. Regardless the storage time, as the plasticizer proportion 273 was increased, both properties rose. Previous works have reported this effect of 274 plasticizer on the moisture content on the films (Mali et al., 2006) and WVP (Alves et 275 al., 2007; Chillo et al., 2008). The addition of plasticizer modifies the molecular organization making the structure less compact and therefore more permeable. An 276 277 increase in inter-chain spacing due to inclusion of plasticizer molecules may promote water vapour diffusivity through the film, hence enabling water vapour transmission 278

(Yang & Paulson, 2000). Contrarily, the CS:CH mass ratio did not have a significant effect on WVP.

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3.5. Mechanical properties

Table 4 shows these parameters for each film formulation after 1 and 5 weeks of storage at 25 °C and 53% RH, the corresponding stress-strain curves of the films are shown in Figure 3. The polymer: plasticizer ratio had a significant effect on both EM and TS (*P <0.05), whereas no effect on %E was found. After one week or five weeks of storage, the films with higher plasticizer ratio (60:40) were significantly less stiff and less resistant to break (lower EM and TS) than those with a lower ratio (70:30). This is in accordance with previous reports. Da Róz et al. (2006) observed that the quantity and type of plasticizer influenced the mechanical properties of thermoplastic starch obtained by melt processing, and a softening effect caused by the plasticizing of the amorphous phase was observed. Mali et al. (2006) observed a significant reduction of EM and TS as the glycerol ratio increased in compression moulded cassava starch films. The molecular size, configuration and total number of functional hydroxide groups of the plasticizer as well as its compatibility with the polymer could affect the interactions between the plasticizer and the polymer (Yang & Paulson, 2000). Being a small molecule, glycerol can get into the polymer chains and weaken the interactions between them (Su et al., 2010). The CS:CH ratio also affected the mechanical properties significantly, and as the CH ratio was increased, the films became stiffer, more resistant and less stretchable (*P <0.05), regardless of the storage time (Table 4). In fact, no plastic deformation was observed for CH containing films (Figure 3). The improvement of the tensile parameters in starch films caused by chitosan addition had previously been observed both in films obtained by casting (Chillo et al., 2008;

Bonilla et al., 2013) and by extrusion (Bourtoom & Chinnan, 2008; Pelissari et al.,

2012; López et al., 2014). This effect could be attributed to the intermolecular hydrogen bonding between starch -OH groups with chitosan – NH₂ groups (López et al., 2014). As the chitosan proportion increased in the film formulation, more -NH₂ groups are available to form hydrogen bonds with starch, hence improving the film resistance (Pelissari et al., 2012). The stretchability reduction in starch blend films caused by chitosan addition has been previously reported by several authors (Xu et al., 2005; Bourtoom & Chinnan, 2008; Pelissari et al., 2012; López et al., 2014). Pelissari et al. (2012) justified this reduction by pointing out the potential increase of the starch crystallinity caused by chitosan, although no starch melting was observed in the studied formulations at the usual temperature (150-200 °C) according to López et al (2014). The mixture effect increasing the structural heterogeneity could also result in some film shortening and an additional effect of the reduced plasticizing efficiency of the PEG, due to its greater crystallization in CH containing films, could also be pointed out. Storage time did not modify the tensile parameters following a clear pattern. In fact, the effect of plasticizer content and CH was more coherent at 5 storage weeks probably by the complete film equilibration, which avoided variability associated to differences in the moisture content. The small changes observed in tensile behaviour must be attributed to the moisture content equilibration more than to relevant changes in the polymer matrix during storage.

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3.6. Optical properties: transparency, colour and gloss

Figure 4 shows typical internal transmittance (T_i) spectra of films, from 400 to 700 nm, as a transparency indicator. Higher values of T_i are related with higher structural homogeneity and more transparent films (Villalobos et al., 2005). Of the films tested, those with no CH were the most transparent, regardless the plasticizer ratio and the storage time (Figure 4). Cassava starch has previously shown high transparency in a comparative study reported by Cano et al. (2014). On the other hand, the incorporation of CH brought about a decrease in T_i, closely related to the CH proportion

incorporated. This is in accordance to the increased heterogeneity of the films caused by CH incorporation, as previously described. The heterogeneous structure implies the occurrence of changes in the refractive index and higher light dispersion resulting in transparency loss, which is especially remarkable at low wavelength. This transparency reduction of starch films caused by chitosan addition was previously observed (Pelissari et al., 2012; López et al., 2014; Dang & Yoksan, 2015). The selective reduction of T_i at low wavelengths was coherent with the above-mentioned yellowness development in the films during thermoprocessing. Lightness, chroma, hue, whiteness index and gloss values of the films after 1 and 5 weeks storage at 25 °C and 53% RH are shown in Table 5. Regardless of the plasticizer proportion and the storage time, the increase in the chitosan content resulted in a decrease in lightness and hue values and a significant increase in terms of chroma values (*P <0.05). In fact, the films with higher CH proportion showed a more saturated yellowish colour (lower whiteness index). Similar results were obtained when CH was incorporated in extruded cassava starch films (Dang & Yoksan, 2015; Khanh & Rangrong, 2015) or in corn starch films prepared by thermo-compression (López et al., 2014). This colour change was attributed to the occurrence of Maillard reactions between amino groups of chitosan and the carbonyl groups of the starch fraction (López et al., 2014). This reaction is promoted by the thermoprocessing temperature and, in the early stage, involves the formation of conjugates between the carbonyl and amine groups of chitosan, producing Schiff bases, Amadori compounds and insoluble polymeric compounds (melanoidins). In this sense, it is noteworthy that films prepared with 40% plasticizer exhibited less browning just after processing, but the Maillard reaction progressed during film storage. In this study, all films showed low gloss values at both 1 and 5 storage weeks. This is in accordance with previous results on starch-HPMC thermo-compressed films (Ortega-Toro et al., 2014). The limited compatibility of both polymers, as observed in

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section 3.1., may be responsible for the films surface roughness and the consequent reduced gloss.

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3.7. Antimicrobial properties

Table 6 shows the progress over storage time (up to 7 days) of the total aerobic and coliform counts of control sample (sliced pork meat without film) and samples coated with the four films with the proportion of polymer: plasticizer (70:30), since they show better tensile and barrier properties. In all cases, chitosan proportion in the films had an effect on the progression of the counts and the final values. Cassava starch films with no chitosan had no antimicrobial effect, and the bacterial growth in this case was even slightly higher than that found for control samples (*P <0.05). After 7 days of storage, the lowest populations corresponded to the films with the highest chitosan proportion (*P <0.05), although only a 1 Log reduction was achieved. The compression moulding method that was used for film preparation could lead to strong interactions between the hydroxyl groups in starch and amino groups in chitosan, thus affecting the diffusion phenomenon of chitosan from the film matrix into the food system (López et al., 2014). Likewise, Pelissari et al. (2009) reported that chitosan incorporation into cassava starch films produced by extrusion did not result in antimicrobial action. The significant antimicrobial activity of chitosan observed by Bonilla et al. (2013) in previous studies carried out with starch-chitosan films produced by casting method can be explained by the previous solution of chitosan in acetic acid, which protonates the amino groups of chitosan and enhances its solubility. Whenever chitosan dissolution is unnecessary (i.e. extrusion and compression moulding method) the amino groups are not protonated, which could explain the observed reduced antimicrobial activity of the obtained films. Likewise the loss of free amine groups during thermal processing could also contribute to reduce the antibacterial action of chitosan. Nevertheless, despite this reduction, films containing 70:30 starch:chitosan ratio extended the shelf-life of meat by 3 days, as compared to the control samples, and considering the commission limits on aerobic colony counts for meat (Commision Regulation 2073/2005).

4. Conclusions

The physical properties of thermoplastic cassava starch films were significantly affected by the incorporation of chitosan and the polymer:plasticizer proportion. Starch and chitosan exhibited lack of miscibility by melt blending. Chitosan incorporation induced Maillard reaction that occurred during the films thermoprocessing, causing films yellowing. As the chitosan ratio increased, the films became stiffer and more resistant to break but less stretchable. Polyethylene glycol was crystallized in the films, which limited its plasticizing effect, being the films with the highest plasticizer ratio the ones that showed the less convenient barrier and mechanical properties for food packaging purposes. The addition of the highest amount of chitosan yielded antimicrobial films that extended the shelf-life of cold-stored pork meat slices. Taking into account the barrier and tensile properties of the films and their antibacterial activity, films with 70:30 starch chitosan ratio and 30 % total plasticiser could be recommended to extend the shelf-life of pork meat.

Acknowledgements

- The authors acknowledge the financial support provided by the Spanish Ministerio de Economía y Competividad (Projects AGL2013-42989-R and AGL2016-76699-R).
- 410 Author Cristina Valencia-Sullca thanks the Peruvian Grant National Program
- 411 (PRONABEC Grant).

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Table 1. Thermal properties of the films analysed by TGA (T_0 , T_{max} , % Mass loss over degradation). Mean values and standard deviation in brackets.

Samples	T ₀ (°C)	T _{max} (°C)	% Mass loss
Native CS	294.5 (0.4)	321.3 (0.4)	90.5 (0.3)
CH	278.9 (0.1)	302.5 (0.5)	76.1 (0.1)
Gly	220.7 (0.3)	250.8 (0.4)	96.9 (0.1)
PEG	372.8 (0.3)	406.9 (0.1)	98.3 (0.1)
$(CS_{100}-CH_0)_{70}-P_{30}$	299.5 (0.3)e	319.3 (0.5) ^{ab}	92.4 (0.1) ^f
$(CS_{90}-CH_{10})_{70}-P_{30}$	291.1 (1.4) ^{cd}	318.8 (0.1) ^{ab}	84.2 (0.1) ^{cd}
$(CS_{80}\text{-}CH_{20})_{70}$ - P_{30}	281.0 (4.0) ^b	319.8 (0.6)bc	82.2 (0.2) ^a
$(CS_{70}-CH_{30})_{70}-P_{30}$	268.7 (1.4) ^a	319.9 (0.1) ^{bc}	81.7 (0.6) ^a
$(CS_{100}-CH_0)_{60}-P_{40}$	296.2 (1.4) ^{de}	318.1 (1.5) ^a	86.6 (0.3) ^e
(CS ₉₀ -CH ₁₀) ₆₀ -P ₄₀	273.0 (6.0) ^a	319.1 (0.7) ^{ab}	83.3 (0.5) ^b
(CS ₈₀ -CH ₂₀) ₆₀ -P ₄₀	286.3 (0.5)bc	322.9 (0.1) ^d	84.8 (0.1) ^d
(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	293.1 (1.2) ^{de}	321.1 (0.7)°	83.6 (0.2) ^{bc}

Different superscripts (a-f) within the same column indicate significant differences among films (*P < 0.05).

Table 2. Thermal properties of films analysed by DSC. Mean values and standard deviation in brackets.

Samples	T _m (°C)		ΔH _m (J/g PEG)		% Crystallinity* (PEG)	
	1 st heating	2 nd heating	1st heating	2 nd heating	1st heating	2 nd heating
(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	56.4 (0.6) ax	50.4 (1.1) ^{bcy}	68.6 (0.4) ^{fx}	28.9 (0.9) ^{ey}	35.4 (0.7)bx	8.8 (0.2) ^{by}
(CS ₉₀ -CH ₁₀) ₇₀ -P ₃₀	58.1 (0.6)bcx	52.4 (0.3) ^{dy}	73.4 (0.9) ^{ex}	47.3 (0.5) ^{cy}	37.9 (0.6)cx	24.9 (0.0)gy
(CS ₈₀ -CH ₂₀) ₇₀ -P ₃₀	56.8 (0.0) abx	50.8 (0.2)bcy	81.2 (1.4) ^{dx}	38.9 (1.4) ^{dy}	42.0 (0.7)dx	20.1 (0.4) ^{ey}
(CS ₇₀ -CH ₃₀) ₇₀ -P ₃₀	58.6 (1.2) cx	51.0 (0.7)cdy	104.0 (4.0) ^{bx}	57.0 (2.0) ^{by}	53.4 (0.5) ^{fx}	29.7 (0.5) ^{hy}
(CS ₁₀₀ -CH ₀) ₆₀ -P ₄₀	58.5 (0.0) cx	48.8 (0.4) ^{ay}	73.8 (1.4) ^{ex}	14.6 (0.1) ^{gy}	38.2 (0.7)cx	6.4 (0.1) ^{ay}
(CS ₉₀ -CH ₁₀) ₆₀ -P ₄₀	60.6 (1.7) dx	50.5 (0.4) ^{bcy}	91.0 (2.0) ^{cx}	41.0 (0.6) ^{dy}	47.2 (0.9)ex	21.8 (0.2) ^{fy}
(CS ₈₀ -CH ₂₀) ₆₀ -P ₄₀	60.2 (1.2) ^{dx}	50.8 (0.1)bcy	95.0 (2.0) cx	30.1 (0.9) ^{ey}	48.9 (1.1)ex	17.6 (0.1) ^{dy}
(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	57.3 (0.6) ^{abcx}	49.4 (0.5) ^{aby}	62.0 (4.0)gx	21.3 (1.4) ^{fy}	32.2 (0.5)ax	11.3 (0.2) ^{cy}
PEG	62.5 (0.3) ^{ex}	56.4 (0.5) ^{ey}	194.0 (3.0) ^{ax}	174.0 (3.0) ^{ay}		

Different superscripts indicate significant differences among films (a-h) or between the first and the second heating step (x,y) (P < 0.05). *Estimated from the crystallization enthalpy values of pure completely crystallized PEG (194 J/g).

Table 3. Thickness, moisture content and water vapour permeability (WVP) of films equilibrated at 53% RH. Mean values and standard deviation in brackets.

Film	Thickness (µm)	WVP (g mm	kPa ⁻¹ h ⁻¹ m ⁻²)	Moisture content (g water/ 100g dry film)		
		Week 1	Week 5	Week 1	Week 5	
(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	199 (12)b	16.0 (3.0) ^{abc1}	15.1 (0.9)bc1	10.4 (0.4) ^{a1}	11.8 (0.4)b2	
(CS ₉₀ -CH ₁₀) ₇₀ -P ₃₀	216 (5)°	15.3 (0.8) ^{ab1}	15.5 (0.4)bc1	9.8 (0.5) ^{a1}	11.8 (0.8) ^{b2}	
(CS ₈₀ -CH ₂₀) ₇₀ -P ₃₀	237 (6) ^d	14.1 (0.1) ^{a1}	13.2 (0.6) ^{a1}	9.7 (1.1) ^{a1}	10.2 (0.5) ^{a1}	
(CS ₇₀ -CH ₃₀) ₇₀ -P ₃₀	260 (12) ^f	14.7 (1.5) ^{a1}	14.5 (0.9) ^{ab1}	9.9 (0.8) ^{a1}	10.7 (0.2) ^{a2}	
(CS ₁₀₀ -CH ₀) ₆₀ -P ₄₀	170 (6) ^a	21.0 (3.0) ^{e1}	16.9 (1.2) ^{de2}	12.4 (0.5)b1	13.7 (1.2) ^{c2}	
(CS ₉₀ -CH ₁₀) ₆₀ -P ₄₀	193 (8) ^b	19.0 (2.0) ^{cd1}	17.1 (1.1) ^{de1}	12.8 (0.4) ^{b1)}	15.0 (1.1) ^{d2}	
(CS ₈₀ -CH ₂₀) ₆₀ -P ₄₀	229 (4) ^d	20.0 (2.0) ^{de1}	16.3 (1.1)cd1	12.2 (0.4)b1	14.6 (0.2)cd2	
(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	247 (10)e	18.0 (2.0)bcd1	18.0 (2.0) ^{e1}	12.4 (0.5)b1	14.4 (0.7)cd2	

Different superscript (a-e) within the same column indicate significant differences among films ($^{*}P < 0.05$). Different superscript (1,2) within the same row indicate significant differences due to storage time ($^{*}P < 0.05$).

Table 4. Tensile properties (elastic modulus: EM, tensile strength: TS and deformation:
 E %, at break) of all films equilibrated at 53% RH after 1 and 5 weeks of storage. Mean
 values and standard deviation in brackets.

Films	EM (MPa)		TS (MPa)		E (%)	
FIIIIS	Week 1	Week 5	Week 1	Week 5	Week 1	Week 5
(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	321 (19) ^{b1)}	542 (28) ^{e2}	7.4 (0.5) ^{a1}	13.3 (0.8)b2	7.9 (0.6) ^{h1}	5.2 (0.3)e2
(CS ₉₀ -CH ₁₀) ₇₀ -P ₃₀	422 (12)d1	761 (49) ^{f2}	13.7 (0.7) ^{e1}	14.5 (0.4) ^{c2}	4.7 (0.3) ^{f1}	2.0 (0.2) ^{a2}
(CS ₈₀ -CH ₂₀) ₇₀ -P ₃₀	596 (22)g1	930 (20) ^{g2}	16.8 (0.3) ^{f1}	18.1 (0.5) ^{d2}	3.3 (0.2) ^{e1}	1.9 (0.1) ^{a2}
(CS ₇₀ -CH ₃₀) ₇₀ -P ₃₀	732 (16) ^{h1}	1118 (36) ^{h2}	20.0 (0.9)g1	22.2 (0.8) ^{e2}	2.8 (0.2)d1	1.9 (0.1) ^{a2}
(CS ₁₀₀ -CH ₀) ₆₀ -P ₄₀	245 (6) ^{a1}	145 (11) ^{a2}	9.3 (0.3)b1	8.6 (0.2) ^{a2}	6.4 (0.5)g1	8.5 (0.3) ^{g2}
(CS ₉₀ -CH ₁₀) ₆₀ -P ₄₀	344 (15)c1	281 (16)b2	9.8 (0.4) ^{bc1}	8.3 (0.5) ^{a2}	2.3 (0.1)bc1	5.6 (0.4) ^{f2}
(CS ₈₀ -CH ₂₀) ₆₀ -P ₄₀	463 (14)e1	350 (20)c2	10.1 (0.6)c1	8.1 (0.7) ^{a2}	2.1 (0.2) ^{ab1}	4.4 (0.3) ^{d2}
(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	546 (32) ^{f1}	459 (35) ^{d2}	10.8 (0.8) ^{d1}	8.5 (0.3) ^{a2}	1.93 (0.13) ^{a1}	2.6 (0.2)bc2

Different superscripts (a-h) within the same column indicate significant differences among formulations (*P < 0.05). Different superscripts numbers (1, 2) within the same row indicate significant differences for the same formulation with different storage time (*P < 0.05).

Table 5. Lightness (L*), chroma (C^*_{ab}), hue (h^*_{ab}), whiteness index (WI = 100 – (100-L*2 + a*2 + b*2)0.5) and gloss at 60° after 1 and 5 week storage. Mean values and standard deviation in brackets.

	Films	L*	C _{ab} *	h _{ab} *	WI	Gloss (60°)
	(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	74.4 (0.3) ^{e1}	8.1 (0.3) ^{a1}	84.4 (0.1) ^{f1}	73.1 (0.4) ^{g1}	6.4 (1.1) ^{a1}
	$(CS_{90}-CH_{10})_{70}-P_{30}$	62.7 (0.5) d1	24.5 (0.6)b1	73.9 (0.4) ^{d1}	55.3 (0.7) ^{e1}	7.1 (0.6)b1
~	$(CS_{80}-CH_{20})_{70}-P_{30}$	58.8 (0.7) b1	29.8 (0.6)e1	69.9 (0.4) ^{b1}	49.2 (0.9)b1	9.0 (0.9) ^{d1}
꽃	$(CS_{70}-CH_{30})_{70}-P_{30}$	52.8 (0.2) a1	32.2 (0.7)f1	66.7 (0.4) ^{a1}	43.2 (0.0) ^{a1}	9.3 (1.2) ^{d1}
WEE	$(CS_{100}-CH_0)_{60}-P_{40}$	73.3 (0.3) ^{f1}	8.3 (0.2) ^{a1}	85.4 (0.4) ^{g1}	72.0 (0.3) ^{f1)}	5.9 (0.7) ^{a1}
>	$(CS_{90}-CH_{10})_{60}-P_{40}$	59.1 (0.4)b1	28.8 (0.6)d1	71.7 (0.5) ^{c1}	50.0 (0.7)b1	7.3 (0.8)b1
	$(CS_{80}\text{-}CH_{20})_{60}$ - P_{40}	63.0 (0.3) ^{d1}	27.5 (0.5)c1	74.4 (0.3)e1	54.0 (0.5) ^{d1}	7.4 (0.3)b1
	(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	62.1 (1.1) ^{c1}	29.5 (0.1)e1	71.5 (0.4)c1)	51.7 (0.9)c1	8.0 (0.8)c1
	(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	73.6 (0.4) ^{f1}	8.6 (0.6) ^{a1}	83.8 (1.2) ^{f1}	72.3 (0.3) ^{g2}	6.6 (0.6)bc1
	$(CS_{90}-CH_{10})_{70}-P_{30}$	65.5 (1.1) ^{e2}	26.4 (0.4)b2	76.6 (1.1) ^{e2}	56.8 (0.4) ^{e2}	6.9 (0.4) ^{d1}
2	$(CS_{80}-CH_{20})_{70}-P_{30}$	61.6 (0.3) ^{d2}	30.7 (0.5) ^{d2}	73.2 (0.3) ^{c2}	50.8 (0.5)c2	8.6 (0.5) ^{e1}
¥	(CS ₇₀ -CH ₃₀) ₇₀ -P ₃₀	54.5 (0.7)b2	35.3 (0.6) ⁹²	68.5 (0.6) ^{a2}	42.6 (0.9) ^{a1}	8.7 (0.5) ^{e2}
WEE	$(CS_{100}-CH_0)_{60}-P_{40}$	72.8 (0.2)g1	8.7 (0.7) ^{a1}	83.7 (0.9) ^{f2}	71.4 (0.2) ^{f1}	6.5 (0.6)b2
>	$(CS_{90}\text{-}CH_{10})_{60}$ - P_{40}	61.8 (0.4) ^{d2}	27.8 (0.7)c2	74.3 (0.5) ^{d2}	52.7 (0.7) ^{d2}	6.0 (0.4) ^{a2}
	$(CS_{80}\text{-}CH_{20})_{60}$ - P_{40}	53.4 (0.4) ^{a2}	33.4 (0.2) ^{f2}	68.3 (0.2) ^{a2}	42.8 (0.2) ^{a2}	6.2 (0.4) ^{a2}
	(CS ₇₀ -CH ₃₀) ₆₀ -P ₄₀	58.6 (1.3)c2	32.7 (0.5) ^{e2}	70.6 (0.7)b2	47.2 (1.2) ^{b2}	6.9 (0.5)cd2

⁵⁴⁶ Different superscript (a-f) within the same column indicate significant differences among films (*P < 0.05).
547 Different superscript (1,2) for the same film indicate significant differences due to storage time (*P < 0.05).

Table 6. Antimicrobial activity of the films on sliced pork meat during storage at 10 °C.

Mean values and standard deviation in brackets.

Microbial					
counts (log CFU/g)	Sample	0	1	4	7
	Control	0.27 (0.02) ^{a1}	1.07 (0.04) ^{(c)(2)}	3.50 (0.02) ^{d3}	5.36 (0.03)c4
υs	(CS ₁₀₀ -CH ₀) ₇₀ -P ₃₀	0.64 (0.03) ^{c1}	1.30 (0.04) ^{(e)(2)}	3.67 (0.02)e3	5.59 (0.03) ^{d4}
Coliforms	$(CS_{90}\text{-}CH_{10})_{70}$ - P_{30}	0.67 (0.03) ^{c1}	1.17 (0.05) ^{d2}	3.42 (0.04) ^{c3}	5.37 (0.04) ^{c4}
8	(CS ₈₀ -CH ₂₀) ₇₀ -P ₃₀	0.57 (0.03)b1	0.99 (0.04) ^{b2}	3.10 (0.03)b3	5.14 (0.03)b4
	(CS ₇₀ -CH ₃₀) ₇₀ -P ₃₀	0.28 (0.02) ^{a1}	0.69 (0.05) ^{a2}	2.96 (0.09) ^{a3}	4.53 (0.11) ^{a4}
	Control	1.28 (0.07)b1	2.68 (0.08) ^{c2}	4.74 (0.07) ^{c3}	6.43 (0.04) ^{d4}
obic	$(CS_{100}-CH_0)_{70}-P_{30}$	1.45 (0.04) ^{c1}	2.86 (0.13) ^{d2}	5.12 (0.03)e3	6.55 (0.04) ^{e4}
aer	(CS ₉₀ -CH ₁₀) ₇₀ -P ₃₀	1.88 (0.03) ^{e1}	3.21 (0.14) ^{e2}	4.53 (0.04)d3	5.47 (0.02)c4
Total aerobic	(CS ₈₀ -CH ₂₀) ₇₀ -P ₃₀	1.75 (0.03) ^{d1}	2.11 (0.04) ^{b2}	4.15 (0.04)b3	5.26 (0.09)b4
F	$(CS_{70}-CH_{30})_{70}-P_{30}$	1.13 (0.06) ^{a1}	1.71 (0.08) ^{a2}	3.79 (0.09) ^{a3}	5.01 (0.05) ^{a4}

Different superscripts (a-e) within the same column indicate significant differences among formulations for the same microbiological analysis ($^{*}P < 0.05$). Different superscripts (1-4) within the same row indicate significant differences due to storage time ($^{*}P < 0.05$).

556 557 Figure captions Figure 1. Scanning electron microscopy micrographs of the cross-sections of the films. 558 (a) Polymer: plasticizer proportion 70:30. (b) Polymer: plasticizer proportion 60:40. 559 Figure 2. Typical thermogravimetric curves (mass loss vs. temperature) and first 560 561 derivative (mg/s vs temperature) for a) Polymer: plasticizer proportion 70:30 and b) 562 Polymer: plasticizer proportion 60:40. Figure 3. Typical stress-strain curves of the films after 1 week (left) and 5 weeks (right) 563 of storage at 53% RH. 564 565 Figure 4. Spectral distribution of the internal transmittance (T_i) of the films. (a) Ratio 566 polymer: plasticizer 70:30. (b) Ratio polymer: plasticizer 60:40. After 1 week and 5 567 weeks of storage. 568







