

process was done to remove the VO_x deposited on the undesired regions. Finally, an ex-situ annealing process is carried out to form a polycrystalline VO_2 layer [39]. The electrodes have been fabricated by two e-beam positive resist exposure prior to metal evaporation and lift-off processes [38]. First, a 90 nm-thick Ti was processed and then 400 nm-thick AlCu pads were deposited.

Figure 2(a) shows a SEM image of the fabricated hybrid VO_2/Si waveguide with the lateral microheater. Identical structures albeit with different grating couplers were fabricated to test the optical switching performance for both TE and TM polarizations. By changing the processing conditions, the morphology of the VO_2 film could be modified such that a granular VO_2 layer, instead of a homogeneous one, was obtained. The granular morphology was the result of an additional solvent bath step during the exposure/lift-off processes. Furthermore, the thickness and roughness of the VO_2 layer was also measured by Atomic Force Microscopy (AFM) after the electrodes fabrication. A thickness of around 15 nm with a roughness of 10 nm was obtained in the sample with granulated VO_2 compared to a thickness of 30 nm with a roughness of 6 nm obtained in the sample with homogeneous VO_2 . Figure 2(b) shows a zoom-in on the hybrid VO_2/Si waveguide with a homogenous VO_2 layer while Fig. 2(c) depicts the hybrid waveguide with a granular VO_2 layer.

3. Experimental results

3.1 Insulator-metal transition of the VO_2 active material

The electrical resistivity was first characterized as a function of temperature in VO_2 test patches deposited on the same wafers having the hybrid VO_2/Si waveguides after ex-situ annealing. The results obtained for the homogenous and granular VO_2 are shown in Fig. 3. The insulator to metal phase transition is clearly observed for both cases. The transition occurs at around 75°C for the heating up process while the reversed transition (metal to insulator) occurs at 65°C along the cooling down process, which implies a hysteresis width of 10°C and a transition temperature of 70°C. The single-phase character of the VO_2 layer is confirmed by the transition temperature being close to the reported value for bulk samples. However, a higher overall resistivity and a slightly lower resistivity change across the phase transition is achieved in the granular VO_2 .

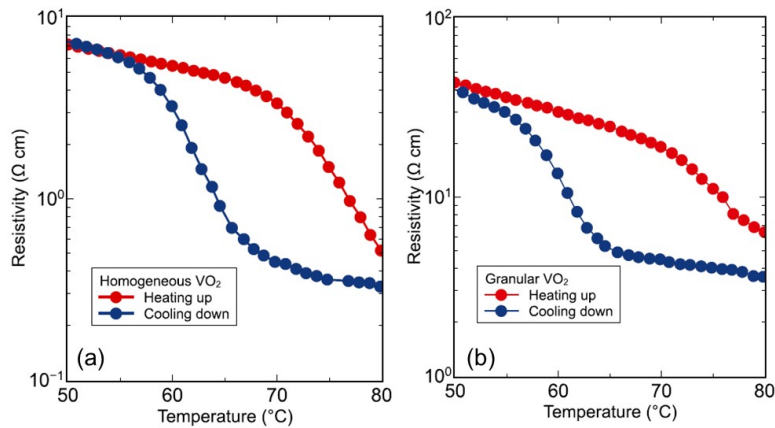


Fig. 3. Electrical resistivity of the (a) homogenous and (b) granular VO_2 layers as a function of temperature after ex-situ annealing. The one order of magnitude change in resistivity as the temperature increases, indicating an IMT at 70°C, confirms the transformation to VO_2 in both samples.

3.2 Optical switching performance of the hybrid VO₂/Si waveguides

The optical switching performance of the hybrid VO₂/Si waveguides has been characterized by applying a voltage to the electrodes and measuring the variation of the optical power at the output. In addition, the applied electrical power was obtained by simultaneously measuring the electrical current flowing through the electrodes. The light from a continuous-wave (CW) laser was injected into the chip and extracted at the output through the grating couplers. The polarization of the injected light was adjusted with an external polarization controller. The output light was photodetected and measured with a power meter. The electro-optical responses for the different types of VO₂ morphologies are shown in Fig. 4 for TE polarization and in Fig. 5 for TM polarization. For both polarizations, it can be clearly seen that the variation of the optical power has a hysteretic response in agreement with the change of the electrical resistivity with temperature observed in Fig. 3, which confirms the existence of the phase transition regardless the morphology of the VO₂ film. The transition from the insulating to the metallic state is achieved by heating the VO₂ (heating up process) while the VO₂ is switched back from the metallic to the insulating state by decreasing the electrical power and therefore decreasing the heat applied to the hybrid waveguide (cooling down process).

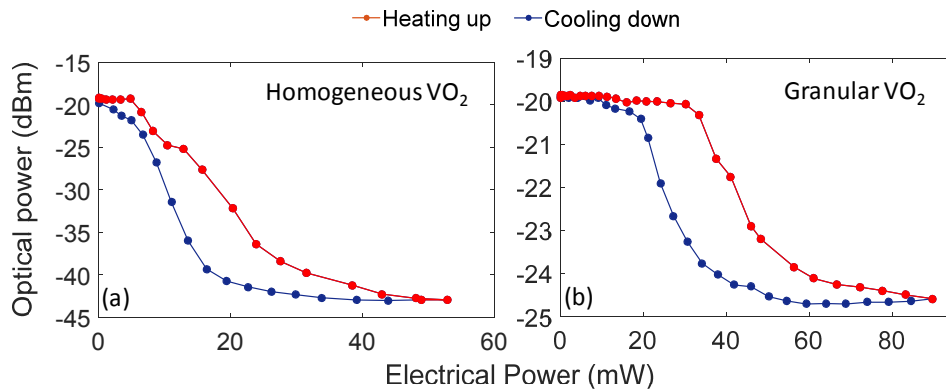


Fig. 4. Variation of optical power as a function of the applied electrical power for TE polarization in the hybrid VO₂/Si waveguide with (a) homogeneous and (b) granular VO₂.

Nevertheless, marked switching differences can be appreciated depending on the VO₂ morphology and the polarization of the light. For TE polarization, the optical losses at steady conditions, i.e. without applying any electrical power, are similar for both hybrid VO₂/Si waveguides with homogenous [Fig. 4(a)] and granular [Fig. 4(b)] VO₂ layers. However, a much larger variation of the optical power when switching towards the metallic state (>20 dB) and a smaller power consumption is achieved for the case of the structure with the homogenous VO₂ layer, which makes this waveguide configuration preferable for TE polarization. The smaller power consumption is attributed to a more efficient heat transfer through the homogenous VO₂ film from the heater to the top of the optical waveguide and therefore independent of the light polarization.

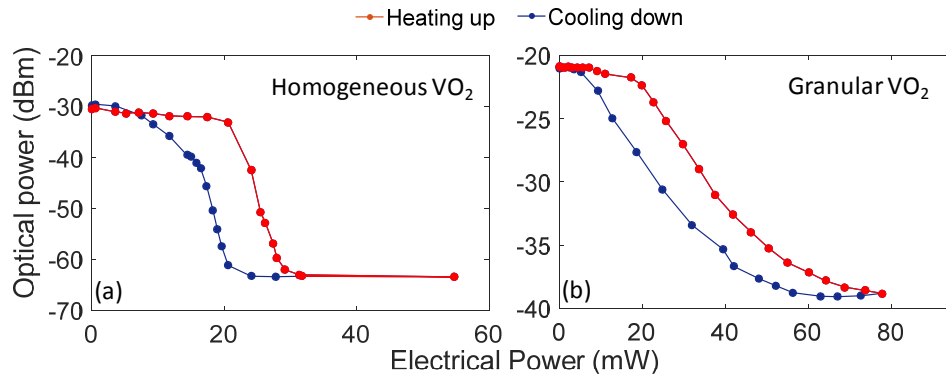


Fig. 5. Variation of optical power as a function of the applied electrical power for TM polarization in the hybrid VO_2/Si waveguide with (a) homogeneous and (b) granular VO_2 .

The optimum switching structure for TM polarization is the opposite compared to TE polarization. In this case, optical losses at steady conditions are almost 10 dB higher for the hybrid waveguide with the homogenous VO_2 layer, Fig. 5(a). Therefore, the waveguide with the granular VO_2 layer is more attractive despite the larger power consumption. Furthermore, as there is a stronger interaction of light with the VO_2 layer compared to TE polarization, a variation of optical losses above 20 dB is still achieved as it can be seen in Fig. 5(b).

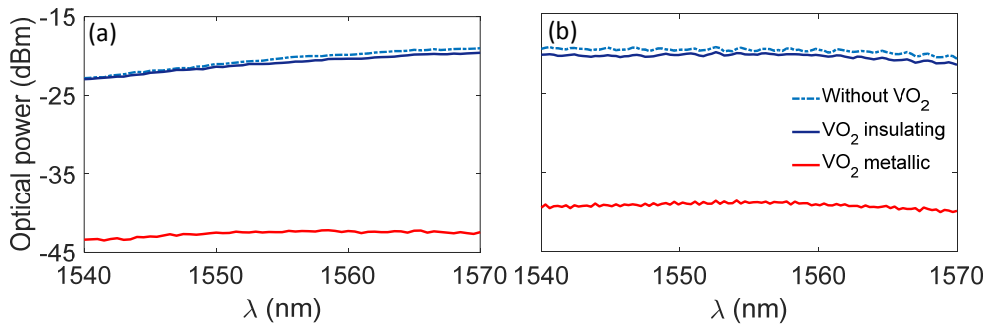


Fig. 6. Transmission spectra of a Si waveguide and the hybrid VO_2/Si waveguide (a) with homogeneous VO_2 layer and TE polarization and (b) with the granular VO_2 and TM polarization. The VO_2 metallic state is achieved by applying an electrical power of around (a) 45 mW for TE and (b) 70 mW for TM.

The transmission spectrum of the hybrid VO_2/Si waveguide is shown for TE polarization and homogeneous VO_2 in Fig. 6(a) and for TM polarization and the granular VO_2 in Fig. 6(b). A similar response is obtained for both polarizations showing that changing the VO_2 morphology could be an easy and cost-effective approach to achieve hybrid VO_2/Si structures with optimized performance for the target polarization. Insertion losses are almost negligible as it can be observed in Fig. 6 when comparing the response of the hybrid waveguide with VO_2 in the insulating state with the response of a silicon waveguide without VO_2 fabricated on the same sample. It should be noticed that the effective thickness of the VO_2 layer is smaller in the hybrid waveguide with granulated VO_2 , which also contributes to reduce insertion losses. An extinction ratio higher than 20 dB is achieved for both polarizations when the VO_2 is switched to the metallic state with a power consumption of ~ 45 mW for TE and of ~ 70 mW for TM. Furthermore, the optical switching bandwidth is maintained very broad (>30 nm) regardless of the morphology of the VO_2 . The wavelength range shown in Fig. 6 was determined by the bandwidth of the CW laser used in the measurements.

3.3 Temporal switching performance and bistability

The optical switching performance of the hybrid VO₂/Si waveguide can be stabilized at any point of the hysteresis cycle just by changing the applied electrical power and, hence, film temperature. The performance of the hybrid waveguide with granular VO₂ has been used to analyze if the morphology of the VO₂ could have an influence on the temporal response. Measurements have been carried out by supplying electrical voltage pulses with a duration of several seconds on the electrodes. Figure 7(a) shows the switching operation for TM polarization between minimum and maximum optical levels of the hysteresis cycle exploiting the full VO₂ phase transition. In this case, the smallest insertion losses and maximum extinction ratio are achieved. Figure 7(b) shows the temporal response of the electrical power (EP) applied to the electrodes and the corresponding normalized optical power (NOP). The switching between states is clearly stable and reversible.

On the other hand, different working points along the hysteresis curve can be chosen to take advantage of the VO₂ bistability feature. An example is shown in Fig. 7(c) with the selected points marked in grey. Two different states in terms of optical losses, state 1 and state 2, can be achieved by using the same electrical signal applied to the electrodes (~25 mW). A short voltage pulse is applied to change between both states. The temporal response in terms of EP and NOP is depicted in Fig. 7(d). For switching from state 1 to state 2, the electrical power must be increased to complete the insulator to metal transition. This is achieved by applying a positive electric pulse and therefore increasing the power applied to the electrodes. On the other hand, the switching from state 2 to state 1 is achieved by applying a negative electric pulse such that the electrical power applied to the electrode is zero during the time of the pulse. The fastest switching speed was measured in the microsecond range consistent with a thermal based operation. Furthermore, the same temporal switching performance was also measured for the hybrid waveguide with homogeneous VO₂.

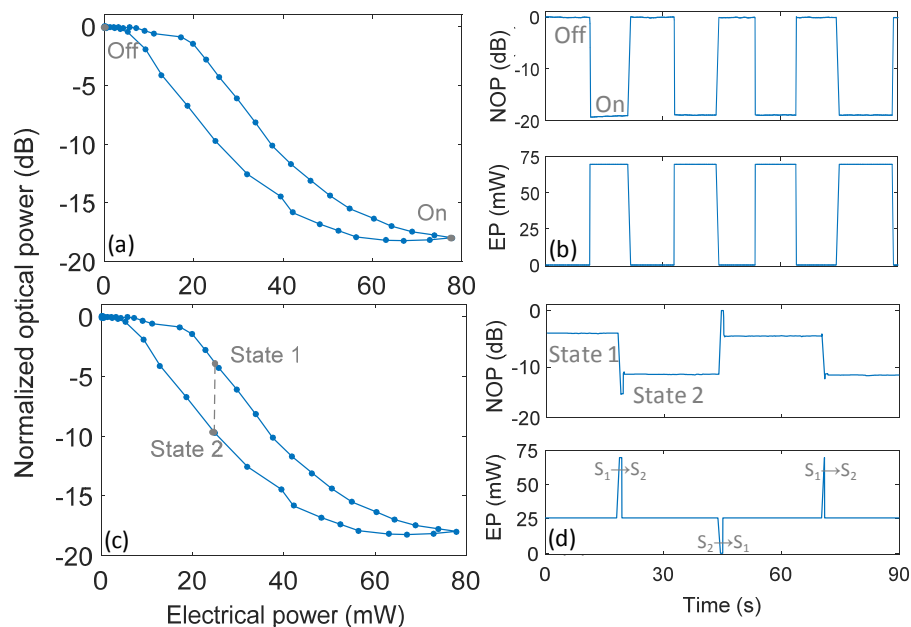


Fig. 7. (a) Scheme of the switching process between maximum (Off) and minimum (On) optical levels and (b) electrical power (EP) of applied voltage pulses as a function of time and the corresponding response of the normalized optical power (NOP). (c) Scheme of the bistable switching performance between State 1 and State 2 and (d) temporal responses of EP and the corresponding NOP for successive reversible switching between both states.

4. Conclusions

Thermally triggered optical switching in hybrid VO₂/Si waveguides has been proposed and demonstrated by using a lateral microheater based on a double metallization process. Furthermore, the impact of the VO₂ layer morphology on the switching performance has been analyzed and exploited to have the best features depending on the light polarization. Therefore, insertion losses below 1 dB and extinction ratios above 20 dB have been achieved with an active length of only 20 μm and an electrical power consumption of around 45 mW for TE polarization and 70 mW for TM polarization. The electro-optical switching response has a broadband performance above 30 nm and is temporally stable and reversible. Furthermore, a bistable switching performance has also been shown by exploiting the hysteretic response of the VO₂ phase transition. Such feature could be useful for implementing optical based memristors or microscale memories with optical readout functionality.

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