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Additional Information

Modelling Biomass Gasifiers in Hybrid Renewable Energy Microgrids; a complete procedure for enabling gasifiers simulation in HOMER

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Abstract

Off grid electrification is key to achieving universal electricity access. Despite the potential of biomass gasifiers as a clean technology to ensure reliable systems, they are not as well looked upon as their advantages suggest. In particular, the software HOMER, which researchers and technicians use the most to simulate and design Microgrids, does not include biomass gasification among its simulation technologies. Although some authors did simulate biomass gasifiers in HOMER, the necessary parameters and procedures to calculate and include them in the tool remain unclear, non-replicable, and leave open research questions as regards modelling. Using the inbuilt Biogas power plant modules in HOMER, this paper presents a set of steps to include the technical and economic parameters to simulate fuelling an electric generator through the syngas produced in a downdraft biomass gasification plant. Two case studies of isolated rural communities in Honduras and Zambia show the viability of the procedure. These case studies also confirm the technical and economic viability of islanded biomass-photovoltaic hybrid renewable energy microgrids. In both cases, the energy demand supplied and distributed by the microgrid had a Levelized Cost of Energy lower than the alternative of extending the electric grid to the communities.

Keywords— Hybrid Microgrids, Renewable Energy, Biomass Gasifier, HOMER

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1. Introduction

Access to modern electricity is one of the targets of the Sustainable Development Goal 7 (SDG7) and one of the United Nations' key priorities for humankind during the next decade [1]. Despite decades of effort, around 0.77 billion people still live without access to electricity [2]. Among them, 80% of the people without access to electricity live in rural areas that will achieve the SDG throughout the expansion of the grid, individual systems or microgrids [3]. According to the IEA, in their 100% electrification scenario, microgrids will provide almost 50% of the new access worldwide [4]. Moreover, if these microgrids need to be carbon neutral, they will rely on renewable energy sources (RES) combined in what is known as Hybrid Microgrid of Renewable Energy Sources (HRES) [5]. In this sense, the study of rural electrification with HRES is gaining increasing attention among scholars due to its potential to meet people's needs with sustainable solutions [6] and their potential to be designed with a holistic system perspective [7].

RES depends on natural resources that are by definition stochastic and variable. However, electricity systems require stability and equilibrium between generation and demand to ensure the security of supply. While Solar photovoltaic (PV) or Wind generation can provide generation at a competitive cost, they cannot always be dispatched when they are needed [8]. To overcome this, HRES planners install storage systems such as Battery Energy Storage Systems (BESS), include dispatchable technologies such as electric generators, or combine both to optimise the systems [9]–[12]. Communities, where electrification is required, tend to be isolated locations and sometimes without enough water resources. These contexts make it difficult to secure the supply with other dispatchable energy resources such as diesel, biomass anaerobic digestion, or mini-hydro schemes; the former due to high logistic costs, the latter two due to lack of water resources [5].

In contrast, dry biomass resources are common in most rural communities due to nearby forests and agricultural waste [13]. This availability leads to a growth of interest in small scale biomass gasification systems in developing countries [14], with India as one of the places with the most applications and significance [15]. Biomass gasifiers convert dry biomass into syngas that fuels an electric generator to dispatch electricity when needed. However, the amount of biomass to use in gasification or combustion needs to be properly managed to ensure correct forest management and avoid deforestation. This requires specific capacities, which are difficult to sustain in rural areas [16]. HRES with biomass gasification are promising since they allow renewable dispatchable generation and reduced consumption of biomass compared with systems that only rely on biomass [17], [18], [19]. Thus, carefully managed, biomass gasification stands as an alternative worth considering for the design and optimisation of HRES [5].

Nowadays, several options exist in the literature for evaluating, designing, sizing, and modelling HRES. Among mathematical software tools, HOMER is extensively used by researchers, academics, planners, and

1 policy makers [20]. Furthermore, Kobayakaba and Kampal [21] justify that HOMER performs better compared
2 with other modelling approaches and tools, which end up simplifying the HRES model for the simulation more.
3 Indeed, Lal *et al.* consider it as one of the most useful tools for simulation and optimisation of both off-grid and
4 grid-tied micro-grids [22]. In this regard, authors use HOMER for sizing and optimising HRES for rural
5 electrification in several locations such as India [23], Iraq [24], Algeria [25], and Nigeria [26].

6 While there is a lot of work on modelling HRES in HOMER, there is little work on including biomass gasification
7 as a potential technology in HRES. Table 1 summarizes the most recent work done by authors about the
8 topic. The table classifies authors by type of technologies used in the simulation, biomass type, biomass
9 characterization, syngas characterization, ratio syngas output to biomass input, type of gasifier, usage
10 patterns, and economic parameters. This review shows how authors do not characterize nor explain how
11 biomass gasification is simulated in HOMER. In this regard, most works do not consider or at least provide
12 neither biomass type, syngas characteristics, parameters of the gasifier, usage patterns of the gasifier,
13 economic parameters of both biomass and gasifier, nor the ratio syngas output to biomass input.

1 **Table 1** Previous work modelling biomass gasifiers in HOMER

Energy Technologies	Biomass Type	Biomass characterization	Biogas characterization	Ratio syngas output to Biomass input	Type of gasifier	Usage patterns	Economic parameters	Ref.
Gasification + PV + Wind +Grid	Pine needles	Yes	No	No	Yes	No	Yes	[27]
Gasification + PV + Wind + Biogas + BESS + Fuel cell	Forest foliage	No	No	No	No	No	Incomplete, not justified	[28]
Gasification + PV + BESS + Grid	No	No	No	No	No	No	Yes	[29]
Gasification	Urban waste	No	Incomplete, not justified	No	No	Incomplete, not justified	Incomplete, not justified	[30]
Gasification + PV + Diesel + Grid	Rice straw, Rice husk, Agricultural waste, Forest feeds	No	No	No	Yes	No	Yes	[31]
Gasification +PV + Wind	Pine needles	No	No	No	No	No	Yes	[32]
Gasification + PV + BESS + Diesel	Rice husk	No	No	No	No	No	Yes	[33]
Gasification + BESS + CHP	Forestry feedstock and sawdust wood pellets	No	No	No	Yes	Incomplete, not justified	Incomplete, not justified	[34]
Gasification + PV + BESS + Fuel cell	No	No	No	No	No	No	No	[35]
Gasification+PV	No	No	No	No	Yes	Incomplete, not justified	Yes	[36]
Gasification + PV + Hydro	No	Incomplete, not justified	No	No	No	No	Incomplete, not justified	[37]
Gasification	Wood pellets	Incomplete, not justified	No	No	Yes	No	Incomplete, not justified	[38]
Gasification	Agro-industrial waste	Yes	No	No	Yes	No	No	[39]
Gasification + PV + Wind + BESS	Dung, Wood and Rice straw	No	No	No	No	Incomplete, not justified	Incomplete, not justified	[21]
Gasifier + PV + BESS	Dung, Wood and Rice straw	No	No	No	No	No	No	[40]
Gasification + PV + BESS + Fuel Cell	No	No	No	No	Incomplete	No	Incomplete	[41]
Gasification+ PV + Diesel	No	No	No	No	No	No	Incomplete, not justified	[42]
Gasification + PV + BESS + Grid	Wood pellets	Yes	Yes	No	Incomplete	Incomplete, not justified	Yes	[43]
Gasification + Grid	Rice straw and husks	No	No	No	No	No	No	[44]
Gasification + PV + Wind + Grid	Pine needles	Yes	No	No	Yes	No	Yes	[45]
Gasification + PV + BESS	No	No	No	No	No	No	Incomplete, not justified	[46]
Gasification + PV + Fuel cell	No	No	No	No	No	No	Incomplete, not justified	[47]
Gasification	Pine needles	No	No	No	No	No	No	[48]
Gasification +PV + Diesel + Grid	No	No	Incomplete	Yes, not justified	Yes	No	Yes	[49]

1 For instance, Kaur *et al.* model in HOMER an HRES for a rural community in India integrating biogas, PV, and
2 batteries, but no specificities on how to include the biogas generator nor the biomass characteristics are
3 included in their study [29]. Similarly, Suresh *et al.* [28] model in HOMER an HRES in India that includes PV,
4 fuel cells, wind power, battery systems, biogas, and biomass, but without specifying the main economic or
5 technical parameters, nor the sensitivity data used to include the biomass gasification in HOMER. Islam *et al.*
6 analyse the potential of hybrid PV biomass gasification systems for electrifying the northern region of
7 Bangladesh [33]. Chambon *et al.* provide an analysis of HRES that combine biomass gasification and PV
8 panels by using HOMER [49]. However, how they include the biomass gasification properties in the software
9 is generic, it does not show where the information comes from nor consider the operational hours of the
10 biomass gasifier. Besides, the specific information about the biomass is not presented, making it impossible
11 to replicate the complete characterisation of the biomass gasifier used in the research. Finally, Alfonso-Solar
12 *et al.* model a hybrid PV-biomass system for higher education buildings in HOMER [43]. They include the
13 main parameters but again no method is used to include the gasification in HOMER, especially regarding the
14 usage patterns of the gasifier and the ratio syngas output to biomass input. To sum up, some authors pioneer
15 the consideration of biomass gasifiers in HOMER, but no clear method on how to include them or where to
16 find the specific information exists in the literature.

17 Therefore, gasification modelling in HOMER is still a self-made practice by specialists as the software does
18 not include a direct way to model biomass gasifiers among their default generation options. This results in the
19 incapability to easily model a viable and promising technology, or the common practice of leaving all the by
20 default values, which compromises the results accuracy. In consequence, the gasifiers' potential is scarcely
21 assessed with HOMER, and even less so for HRES in dry rural areas.

22 To overcome this gap, this paper provides a procedure to model biomass gasifiers in HOMER considering
23 and naming the main parameters needed to include them in the software, and where to obtain the required
24 data. The paper also points out the critical elements for modelling gasifiers for rural areas. The proposed steps
25 pay special attention to the main variables of this technology, fuel type, resource and technology costs, and
26 operational availability under rural conditions. The method details the possible paths to obtain this information
27 and how to process it for the correct coupling with the software. To prove the viability of the process, we apply
28 it to two real projects on isolated rural communities in Honduras and Zambia, with populations of around a
29 thousand people. Then, the paper discusses the critical information needed to model this technology and
30 provides valuable findings and tips to model gasifiers based on the authors' real experience.

31 The rest of the paper's structure is as follows. Section 2 presents the method and material used, including a
32 description of HOMER and the way of modelling biomass gasifiers. Section 3 provides the information on the

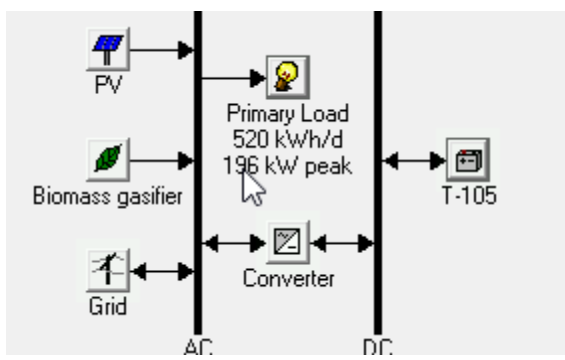
1 case studies, the biomass used, and how it was modelled. Section 4 discusses the results and section 5
2 presents the conclusions.

3 **2. Material and methods**

4 This section describes the general procedure to perform feasibility analysis of HRES using HOMER simulation
5 software [50], which, as previously stated, is widely used for economic and environmental feasibility analysis
6 of case studies and policies [38], [43], [51], [52]. A detailed description of how to introduce performance
7 characteristics of a biomass gasifier for electricity generation including the typical ranges of the key
8 performance parameters has been included.

9 **2.1 General procedure to define simulation inputs**

10 Before running the simulation, it is necessary to predefine the system, i.e. energy sources must be selected,
11 together with the storage systems and the energy demand. Figure 1 shows a scheme of the chosen sources
12 and devices. Either an AC or a DC bus could be chosen to integrate the sources, the utility grid (if available),
13 the primary load (electricity load curve of the site), and, additionally, a converter (inverter-charger) that
14 connects both buses.



15
16 Figure 1 **Scheme of the components once the inputs have been introduced in HOMER.**

17 Figure 2 shows the required inputs for the setup and the outputs given after the simulation process in the
18 HOMER software that should be considered in any HRES simulation.

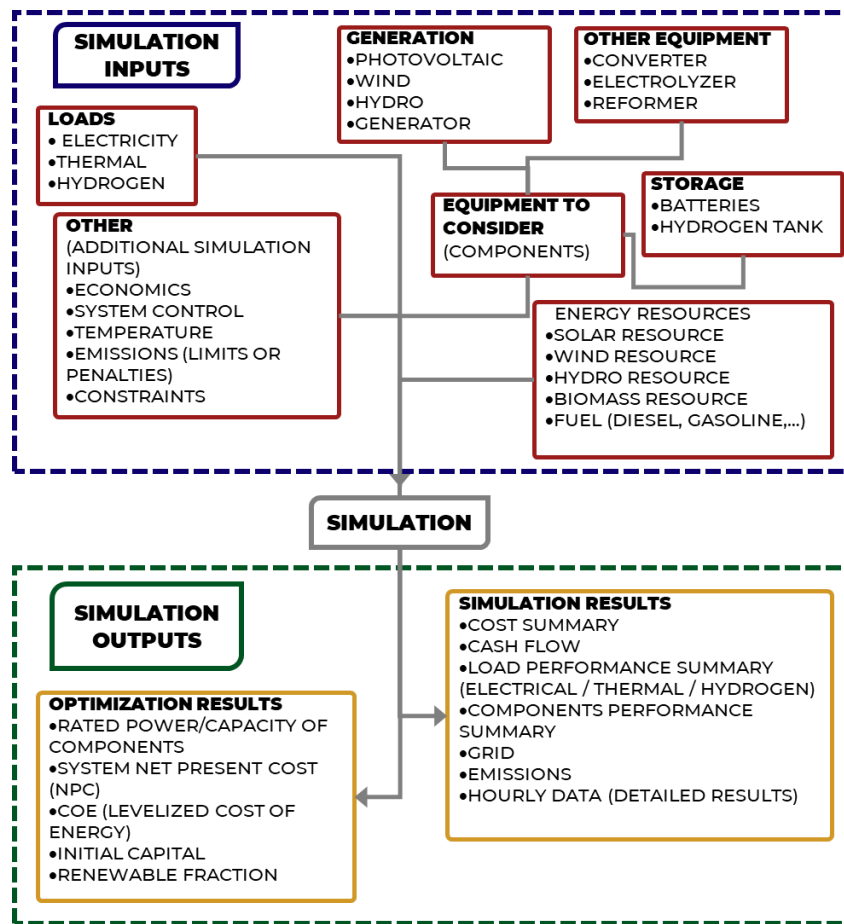


Figure 2 Schematic overview of inputs and outputs of HOMER Software

The system uses these inputs to make hourly energy balances for a year. For each hour, generation and storage components cover the electricity demand, the software calculates the flows of energy from/to each component (generation, storage, or other energy conversion system). Feasible configurations are only those combinations that cover the demand for the whole year with a set parameter of the non-covered load.

Then HOMER orders the feasible configurations according to the lowest Net Present Cost (NPC) [50]. For the studied project's lifespan, NPC takes into account initial investment, component replacement cost within the project lifetime, Operation and Maintenance (O&M) cost, fuel cost and cost of energy purchased from the grid, if available [53], [54]. As a result, a sensitivity analysis is obtained, giving information about the size of each component, the energy transacted with the grid, the renewable energy fraction, and the costs and the emissions produced for each scenario (Figure 3).

Calculate Simulations: 0 of 1260 Progress: Status: Completed in 6:54.
Sensitivities: 12 of 12

Sensitivity Results | Optimization Results

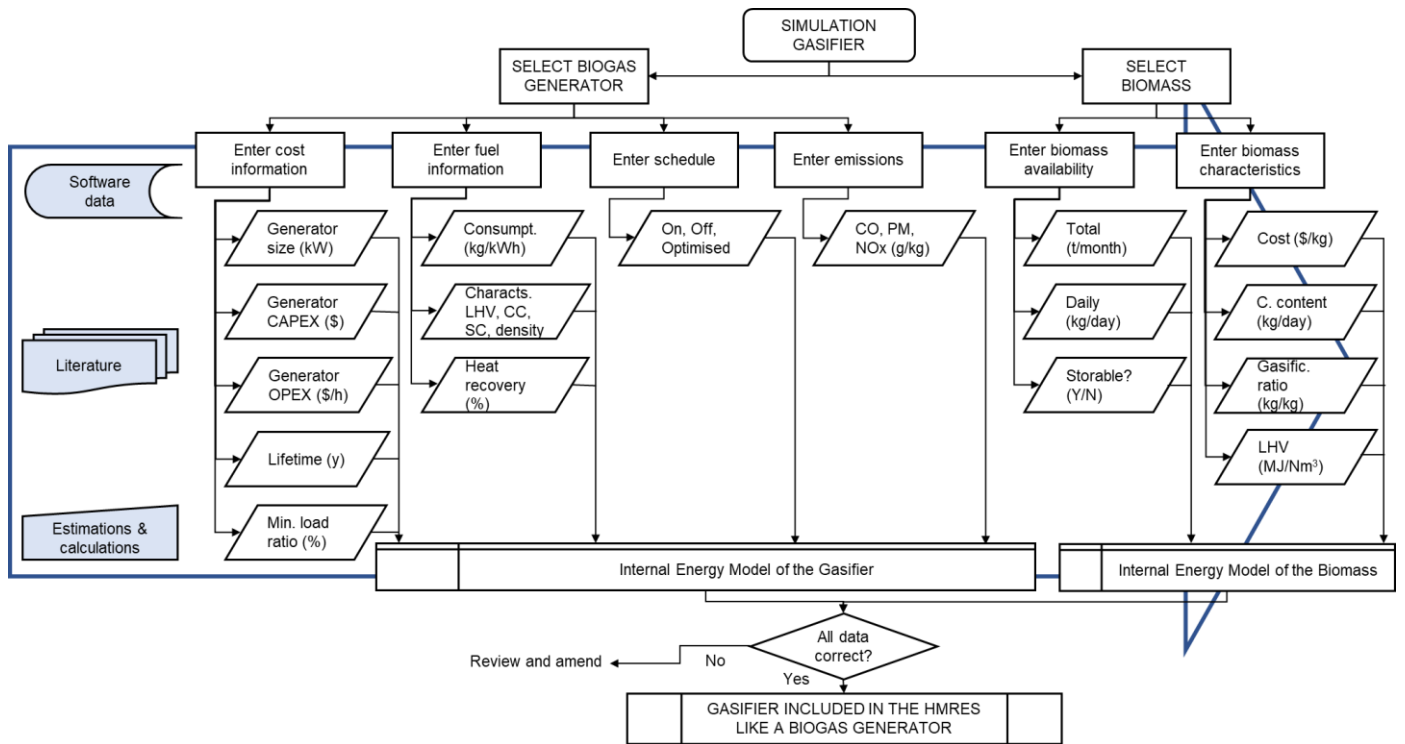
Double click on a system below for optimization results.

Biomass Price (\$/t)	Min. RF (%)					PV (kW)	BGPP (kW)	T-105	Conv. (kW)	Grid (kW)	Initial Capital	Operating Cost (\$/yr)	Total NPC	COE (\$/kWh)	Ren. Frac.	Biomass (t)	BGPP (hrs)
225.000	0					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
225.000	40					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
225.000	60					80	20			250	\$ 158,501	36,088	\$ 953,280	0.222	0.63	63	3,654
225.000	80					80	80			250	\$ 260,077	83,321	\$ 2,095,071	0.488	0.81	252	3,654
150.000	0					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
150.000	40					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
150.000	60					80	20			250	\$ 158,501	30,966	\$ 840,461	0.196	0.65	68	3,654
150.000	80					80	60			250	\$ 217,058	51,510	\$ 1,351,475	0.315	0.81	200	3,654
100.000	0					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
100.000	40					80				250	\$ 88,000	17,679	\$ 477,354	0.111	0.53		
100.000	60					80	20			250	\$ 158,501	27,219	\$ 757,960	0.177	0.68	74	3,654
100.000	80					80	60			250	\$ 217,058	40,836	\$ 1,116,395	0.260	0.83	206	3,654

Figure 3 Example of sensitive results given by HOMER.

2.3 Simulation in HOMER of gasification technology

The issue when designing an HRES integrating a Biomass Gasification Plant (BGP) emerges when the simulation program, such as the case of HOMER, does not have a predefined energy technology associated with it, usually resulting in the need to accommodate it with the existing elements. To integrate a BGP in HOMER, the first step needed is to understand the necessary parameters to include both the desired generator and the fuel (biomass in this case). Secondly, the method requires the performing of a literature review and the problem formulation. The aim is to identify the key features that describe how to define a BGP and the fuel by the software, according to the requested parameters [19], [53]. Finally, the software runs the simulations with the gasifier correctly modelled if all data are correctly entered. Figure 4 illustrates the process.



1
2 **Figure 4 Methodology to add a BGP in HOMER**

3 The information required to set up the biomass gasification generator in the subsection “Equipment to
 4 consider” is “Cost”, “Fuel”, “Schedule”, and “Emissions”. First, the software requires adding a generator in
 5 the section ‘components’ and introducing economic information about the gasifier such as the size and cost
 6 of at least one gasifier (the one intended to be installed). The cost of the gasification plant for small scale
 7 applications is in the range of 2.0-3.5 USD/W [53], [55]. To this value, shipping cost and taxes must be added.
 8 Both of them depend on the final location of the plant. Replacement and Operation and Maintenance (O&M)
 9 costs are also needed, and both strongly depend on the gasifier’s location. According to [55], [56], the fixed
 10 cost of O&M (without considering fuel cost) for a gasification plant ranges from 2 to 6 % of CAPEX/year [53].
 11 HOMER requires the O&M cost in USD per hour of operation (if all the values are in another currency,
 12 HOMER will give all the results in that currency) so users must consider an estimated annual operation time
 13 of the gasification plant to calculate this cost. If the O&M cost information is available in terms of USD per
 14 produced kWh of electricity, typically 0.05 to 0.2 USD/kWh [55]), users must consider an average operational
 15 power of the gasification plant, usually 50- 100% of rated installed power, to define the value in USD per
 16 hour.

17 In subsection “Schedule” it is possible to set up the gasification plant’s operation schedule (hour by hour).
 18 For every month, what time the gasifier will be ON, OFF, or OPTIMIZED, can be set up. If the OPTIMIZED
 19 option is selected the generator will be ON or OFF according to each possibilities' higher economic feasibility.

1 By default, the program decides for each time step whether or not to operate the generator based on the
2 electrical demand and the generator's economics compared to other power sources. However, it is possible
3 to force using or not using the generator during the planning time [57]. The operational schedule is especially
4 useful when the manufacturer advises using the gasifier no more than a certain number of hours per day to
5 avoid damage or the reduction of the gasifier's lifespan. In this case, it is necessary to analyse and set the
6 most convenient schedule for the gasifier's operation when simulating. HOMER will decide, within the
7 selected range, how long the BGP must operate. Moreover, to improve social acceptability of a BGP in HRES
8 of "Prosumers", usage hours should be optimised in an hour range that is compatible with living patterns.

9 In subsection "Fuel", information about fuel consumption as a function of the output power must be provided
10 to HOMER. The aim is to calculate the efficiency at different loads. Fuel can be a fossil or renewable fuel
11 (gasoline, natural gas, biogas...), or stored hydrogen. For the simulation, the fuel properties needed are:
12 Lower Heating Value (LHV), Carbon content (CC), Sulphur content (SC), and density. For this method,
13 biogas is selected as fuel, therefore, to introduce information about biomass resources will be necessary.
14 For this, HOMER requires the setting up of biomass availability and properties.

15 Biomass availability represents the average biomass feedstock availability. Available biomass is the
16 sustainably available biomass per month (tonnes/month) or, if necessary, kilograms for each hour of the
17 year. Then, for simulation purposes, the available biomass feedstock (tonnes/day) is required. If all the
18 biomass is not used in a given time step, the user must set if the biomass can be used in future time steps
19 [50].

20 Biomass properties include four parameters. The biomass cost depends on the plant's location. The carbon
21 content depends on the biomass used, typically in the range 45-55% on the dry mass basis [58]. The Lower
22 Heating Value (LHV) of the obtained biogas, which in the method refers to the syngas obtained from the
23 biomass gasification process. And finally, the gasification ratio, which is the mass ratio of produced syngas
24 (biogas for HOMER) to biomass consumed by the reactor. This ratio allows us to calculate the amount of
25 biomass resource used or purchased if the price of the biomass is assigned. One of the limitations is that the
26 program assumes the gasification ratio value is constant in time, but in reality, it depends on the biomass
27 characteristics, the efficiency of the gasification process, and the power ratio of the plant. If one or more of
28 these values are modified, the gasification will change. Even during the operation of a BGP, the efficiency
29 could change as a load function. In this case, an average or a weighted value must be used as an input. A
30 typical gasification ratio usually ranges from 2 to 3 Nm³ of syngas per kg of biomass [59]–[62]. However,
31 HOMER requires this parameter in kg gas/kg biomass. The syngas density is around 0.9 – 1.1 kg/Nm³. For
32 instance, at 20°C and 1 atmosphere, and assuming a composition of 21% CO, 17% H₂, 48% N₂, 13% CO₂,

1 1% CH₄, the syngas density would be equal to 0.95 kg/m³ [63]. Thus, the value to use as input would range
2 from 1.8 to 3.3 kg of syngas per kg of biomass.

3 The LHV values range from 4.5 to 6 MJ/Nm³. The gasifier uses biomass as primary fuel and air as a gasifying
4 agent. These values of LHV are within the range of that obtained by [18], [19], [53], [58]–[60], [64], [65]. Users
5 must check that the efficiency of the gasification process (ratio syngas flow to biomass flow, both expressed
6 in terms of energy) is consistent with literature values, i.e. it ranges from 60 to 88% [18], [59], [65] or make
7 the required experiments in the laboratory to measure biomass' properties.

8 Finally, in subsection "Emissions" the definition of the expected generator emission factors is provided. The
9 program estimates the generator's absolute total emissions per year, of Carbon Dioxide (CO₂), Carbon
10 Monoxide (CO), Unburned Hydrocarbons (UHC), Particulate Matter (PM), Sulphur Dioxide (SO₂) and
11 Nitrogen Oxides (NO_x). HOMER requires four of the six mentioned pollutants (in grams per kg of fuel) to
12 carry out the estimation. The emission factor is required for CO, UHC, PM, and NO_x. Additionally, the user
13 must indicate which proportion of fuel sulphur the fuel emits as PM (so the rest will be emitted as SO₂). The
14 quantity of the pollutant produced by the generator depends on the fuel, engine design, and operating
15 conditions, including the load of the generator. For simplicity's sake, the program assumes the emission
16 factors are constant values [57].

17 **3. Case Studies**

18 The proposed process has been implemented in two case studies: the rural community of El Santuario, in
19 the Honduran Dry Corridor; and Mumbeji, located in the North-Western province of Zambia. The communities
20 have been selected given their similarity in terms of socio-economic, environmental, and energy context.
21 This allows us to assess the feasibility of implementation and replication potential of the model for the
22 gasification introduction in HOMER. Also, the benefits of incorporating gasifiers to HRES when there is
23 enough available dry biomass.

24 Both communities are characterized by being isolated and non-electrified. Currently, population densities are
25 respectively around 500 in 76 households in the Honduran community and around 1,000 inhabitants in the
26 Zambian located in 100 households. Solar and dry biomass are the main available renewable resources,
27 due to climate and geographic conditions. The predominance of agroforestry and farming activities provides
28 biomass resources in the form of crop and timber waste. Wind power and micro-hydraulics were discarded
29 due to their unreliable supply.

1 Energy demand was estimated according to the detected needs in the fieldwork, surveys [66], and the
2 literature regarding similar rural electrification projects [16], [67], [68]. Similar results were obtained for both
3 communities. The annual energy demand is estimated at 2-3 kWh per day and household, aligned with the
4 global data on basic energy needs for ensuring human well-being [69]. The load profile has two typical peak
5 loads: one during the early morning and one more prominent in the evening, at dusk after the working hours,
6 reaching a maximum value of 18 kW (6:00 pm) in the case of Honduras and 30.5 kW (9:00 pm) in the case
7 of Zambia.

8 The gasification plant is integrated into an HRES that combines a PV system, gasification, and a battery
9 bank. Gasifier integration was simulated following the following proposed procedure. Syngas generation
10 technologies have been techno-economically assessed to model a potentially replicable system.
11 Nevertheless, biomass availability and characteristics will differ in different locations and must be
12 independently evaluated.

13 **3.1 Biomass generator selection**

14 Downdraft technology is recommended as proven on small scale projects with good performance results
15 [70]. It is less costly and easier to operate than other syngas generation technologies, which makes it suitable
16 for small rural communities [71]. Besides, the tar content ratio is below 1 g/Nm³, almost 100 times lower if
17 compared to updraft gasification technologies [72].

18 Among more than 20 models and manufacturers, the *PP30* gasifier from *All Power Labs* [73] was assessed
19 as the most proven, efficient, and cost-effective technology. The installed power is 30 kW, with a maximum
20 electrical power output of 27 kW at 60 Hz frequency. The investment cost of the gasification plant is 2 USD/W
21 of equipment [73]. The total cost is 60,000 USD, including shipping and installing. Replacement costs of the
22 whole system were set to 10% less of the investment costs (1.8 USD/W). Maintenance costs are considered
23 2% of the investment costs (0.04 USD/W), equivalent to 0.072 USD/hour considering that the gasifier lifetime
24 is calculated as 15,000 operating hours.

25 The minimum syngas flow rate for the gasification system is 2.2 Nm³/h, equivalent to approximately 3 kW of
26 electrical power output. The gasifier load ratio is recommended to be above 10% to avoid operational failures.
27 Two different scenarios have been assessed regarding the minimal load ratio in the syngas gasifier output.
28 In the case study of Honduras, the minimum load ratio is set to 50%, whereas in Zambia's case there is no
29 load restriction, provided that output does not go below the minimum set by the manufacturer, 3 kW.

30 Gasifier biomass electrical generation efficiency is 23% based on the manufacturer's data. Manufacturer
31 tests show a typical composition from syngas obtained of 21% CO, 19% H₂, 3% CH₄, 11% CO₂, 44% N₂, and

1 Sulphur content almost negligible. Biogas fuel properties (LHV, CC, SC, and density) will be defined
2 according to the biomass characteristics. The gasification plant allows us to recover heat from the engine, in
3 a proportion of 1.5-2 kWth/kWe. Heat recovery efficiency reaches close to 42%. This thermal energy will be
4 available to serve future thermal needs in the community, although it is not considered as part of the
5 simulation outputs.

6 In the proposed model, the gasifier is expected to operate mainly as a back-up system to the HRES to avoid
7 biomass over-consumption. Therefore, the gasifier is expected to generate enough energy to cover the
8 demand when the solar resource is not enough, or the batteries reach a State of Charge (SoC) of 30%. To
9 implement that in the simulation, the usage schedule is set to follow "Optimized" operation. In addition, the
10 operation of the gasifier is further improved by forcing it to stop during the central hours of the day and resting
11 hours at night. In the simulations no emission limits and penalties have been considered, syngas being a
12 renewable gas within a closed biomass carbon cycle [49].

13 **3.2 Biomass selection and characterization.**

14 Biomass availability and characteristics will vary according to the location. When possible, biomass
15 properties should be determined in specific physicochemical laboratory tests. As an alternative, research
16 was performed in order to define wood biomass characteristics. The results showed similar characteristics
17 in both case studies.

18 In the Honduran Dry Corridor, forest biomass in the form of branches predominates due to forestry activities.
19 In contrast, the North-Western province of Zambia is an area of farmland, Cassava being the most
20 predominant and suitable crop in the region [74]. In the Honduras case study, the inhabitants noted a dry
21 biomass consumption ratio of 17 kg/day and household, mainly for cooking and lighting activities. But
22 biomass availability for the community is up to 2 tonnes/day [75].

23 Forestry biomass properties in Honduras were estimated based on literature [61], [76] ICF's data (Honduran
24 Forestry Conservation Institute), and a similar stand-alone HRES consuming wood biomass [19]. According
25 to the references, the syngas generation per kg biomass was set to 2.1 Nm³/kg. The density of syngas is
26 about 0.72 kg/m³, then the gasification ratio is calculated at 1.85 kg gas/kg biomass. The LHV input was 5.5
27 MJ/Nm³ (1.53 kWh/Nm³). Knowing that conversion gas-electricity using the syngas generator is 23%, the
28 electrical generation per kg of biomass is calculated at 0.9 kWh/kg.

29 The rural community of Mumbeji in Zambia currently cultivates 23 ha of Cassava with a crop yield of 5.8
30 tonnes/ha/year. Cassava production is calculated in 0.365 tonnes per day. The final dry biomass potential is
31 estimated at 0.13 tonnes/day based on literature data regarding the ratio waste-useful crop (36 %) [74], [77].

1 Cassava waste properties had to be sought from existing literature [61], [74], [76], [78], [79] considering its
2 physicochemical properties comparable to wood biomass ones [77]. LHV of syngas is set at the minimum
3 suggested 4.5 MJ/Nm³ (1,25 kWh/Nm³) and the carbon content to 44%. Gasification ratio wood-syngas is
4 set at 2.08 Nm³/kg to be conservative, and following the proposal by [61], while the gasification ratio is
5 calculated at 1.24 kg gas/kg biomass. Applying 23% electrical generation efficiency, the gasifier produces
6 0.83 kWh/kg biomass.

7 Although available biomass is considered as a waste, a certain biomass acquisition price is recommended
8 to be included in the cost structure. This will allow us to cover the future expenditure of maintenance and
9 replacements, as well as to avoid deforestation by raising awareness of the cost of renewable electricity
10 generation.

11 According to an IRENA report [80], biomass for power generation costs ranges between 44 and 94 USD per
12 tonne. The commercialisation price of dry biomass in Latin-America is about 300 USD/tonne [75], whereas
13 the sale price of fresh cassava roots in 2013 was around 20 USD/tonne [81]. To avoid the risk of under or
14 overestimation of the price, it is fixed at 100 USD/tonne in the case of Honduras and 50 USD/tonne in the
15 case of Zambia.

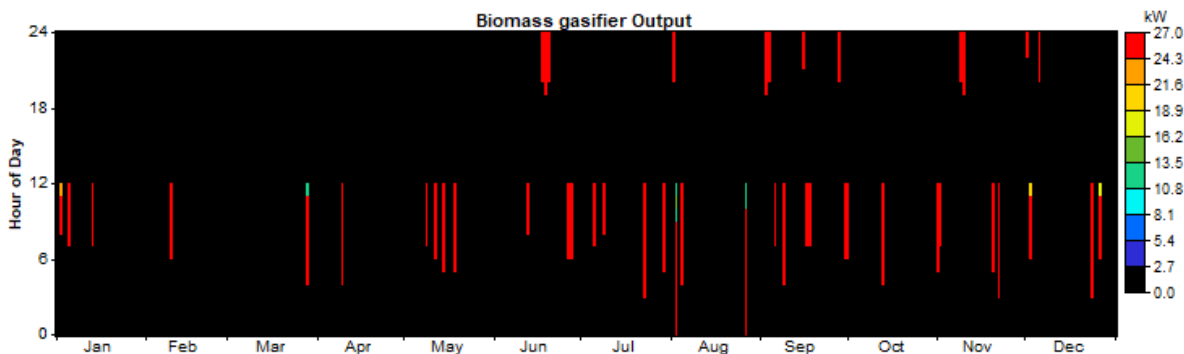
16 **3.3 Simulation results**

17 Once the BGP and the biomass have been modelled, data was introduced in HOMER and the gasification
18 plant was simulated. The results allow us to study the energy model and the integration of the gasifier in the
19 HRES.

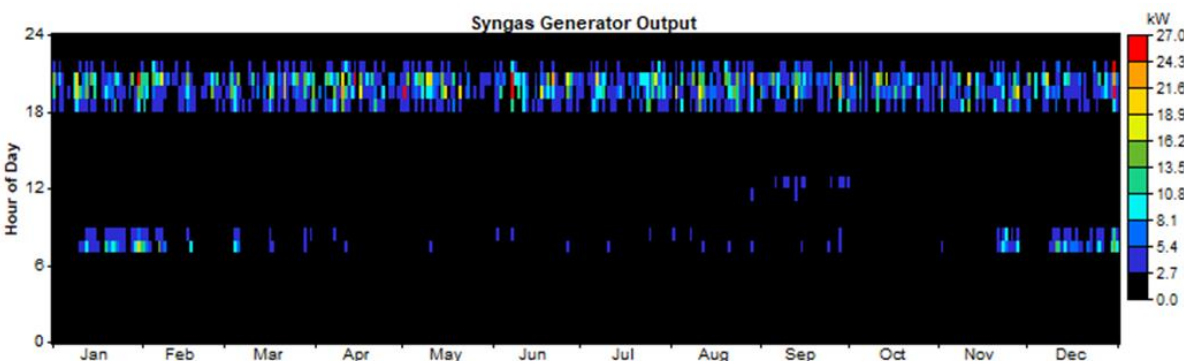
20 Figure 5 and Figure 6 show gasifier power output throughout the year for the 24 hours in a day in the case
21 studies of Honduras and Zambia, respectively. In both cases, the gasifier starting schedule is in intervals
22 from 6 am to 12 pm and from 6 pm to 12 am. Therefore, the gasifier's role as a backup system is confirmed
23 when solar power is low, demand high and storage SoC decreases to 30%.

24 However, the number of starts during the year differ according to the location, with 8.5 times more in the
25 case of Zambia. This is based mainly on the free minimum load ratio, the higher maximum load peak, and
26 the lower biomass cost. It does influence as well that the wet season in the Honduran Dry Corridor (May to
27 September) is drier than the one in the North-Western region of Zambia (November to February). Hence, it
28 turns out that, in the case of Zambia, the gasifier operates more as complementary power than as a back-up
29 system to the HRES.

1 Also, in the case of Zambia, the gasifier works at 30% of its rated capacity, which means that it still has the
2 potential to generate energy if the needs of the community increase in the future. The same applies to the
3 Honduras's case, in which the capacity factor is around 3%. This value is consistent with the role of the
4 gasifier as backup system. In addition, non-fixing of a minimum load ratio in the Zambian case, gave a
5 biomass consumption of 5.37 tonnes per day, 37% lower than in the 50% minimum load ratio case (8.5
6 tonnes/day). Hence it is more efficient in biomass but much less efficient in equipment usage, as will be
7 discussed in the next section. Anyhow, both outcomes are below the current biomass availability identified
8 in the community.

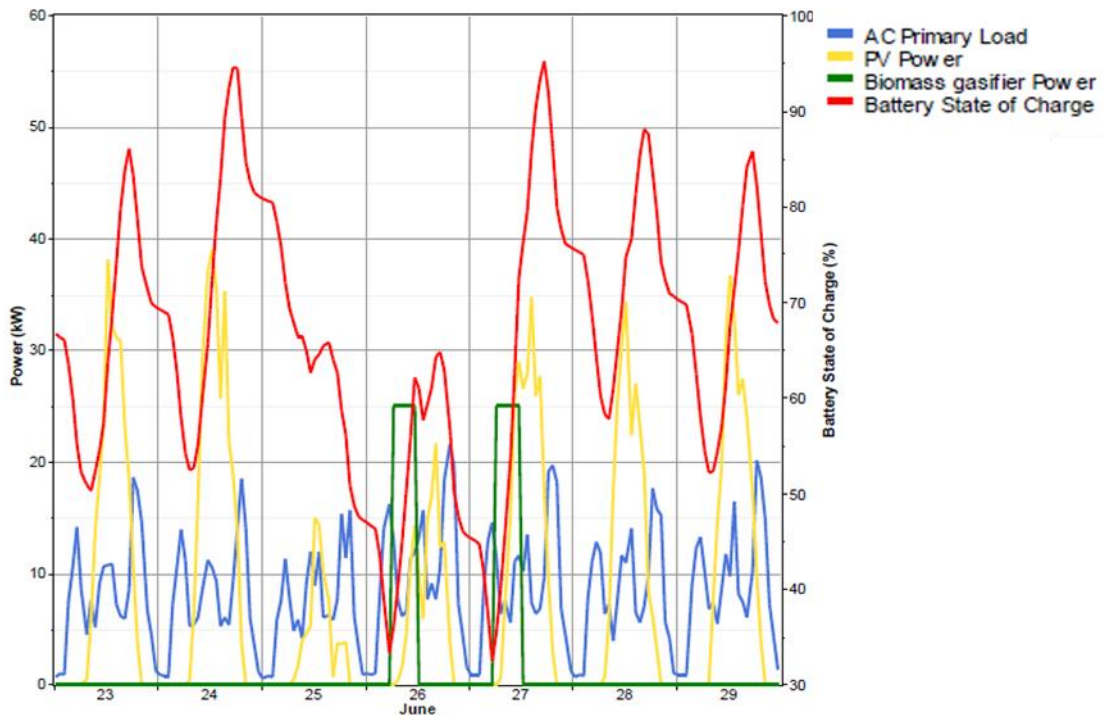


9
10 Figure 5 Output of the gasifier during a typical year for the case in Honduras.



11
12 Figure 6 Output of the gasifier during a typical year for the case in Zambia.

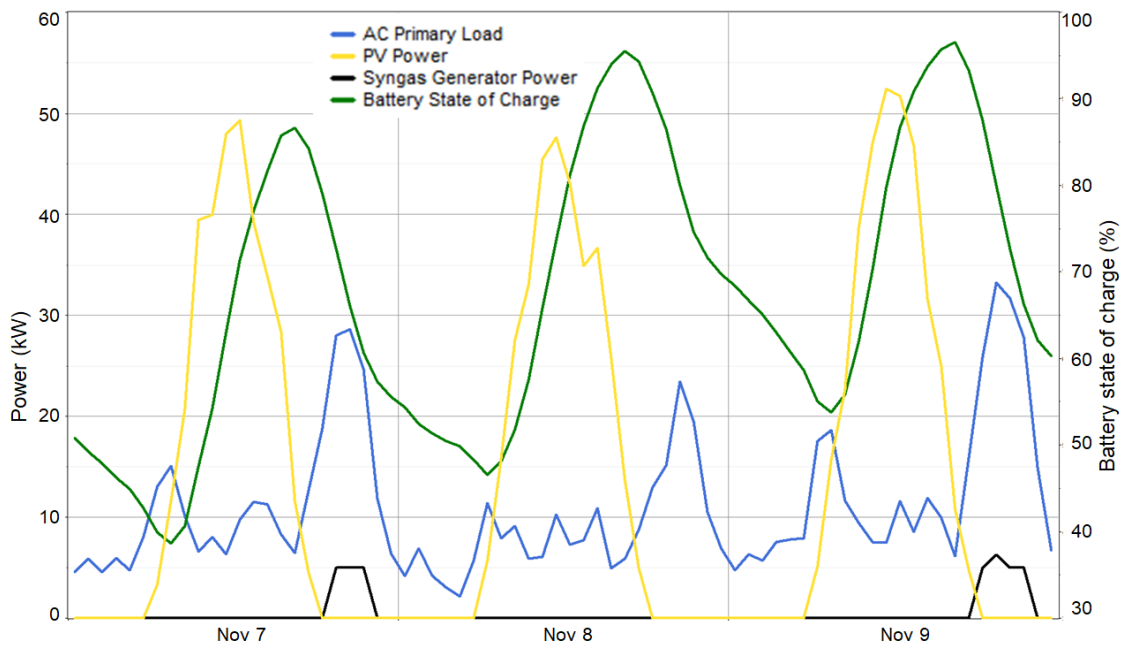
13 The simulations provide an overview of the operation of the gasifier as part of the HRES. Figure 7 shows the
14 example for a typical week of June when solar irradiation was limited due to the rainy season in Honduras.
15 Therefore, the PV power is limited, and the batteries must be used. When the batteries' SoC is close to the
16 minimum value of 30% the gasifier is activated, thus covering the demand of the community while charging
17 the batteries.



1

2 Figure 7. Hourly operation according to HOMER for a typical week of June. Case of Honduras.

3 A different scenario occurs in the case of Zambia (Figure 8) during November. On the 7th and 9th of
 4 November the gasifier starts to operate even though the PV power generation is high, but it is not enough to
 5 cover the demand. In this case, the batteries do not reach a SoC below 45%.



6

7 Figure 8. Hourly operation according to HOMER for a typical week of November. Case of Zambia.

1 Finally, Table 1 summarises the main economic and socio-technical features of the simulated HRES. The
 2 gasifier allows us to ensure the reliability and continuity of the energy supply, in El Santuario only 1.26 kWh/yr
 3 out of a demanded 73,000 kWh/yr will not be met (0.002%). In Mumbeji, the yearly electricity production is
 4 155,693 kWh, and the unmet load 1,537 kWh/yr (0.99%).

5 Table 1. **Main economic and socio-technical features of the simulated HRES.**

Case Study	Unmet Load (kWh/yr)	Initial Capital (USD)	Total NPC (USD)	LCoE (USD/kWh)
El Santuario (Honduras)	1.26	181,733	256,133	0.06
Mumbeji (Zambia)	1,537	429,400	564,697	0.48

6 The Levelized Cost of Energy (LCoE) could be assessed as the price the community would have had to pay
 7 back on the investment. However, in the case of a donation, the community would only have to cover the
 8 costs of dry biomass, other O&M costs, and future replacements.

9 The LCoE for the HRES in the rural community of El Santuario amounts to around 0.06 USD/kWh, clearly
 10 below the typical price of Honduran residential electricity: 0.12 to 1.14 USD/kWh [82]. The obtained value is
 11 higher for the case of Mumbeji (around 0.48 USD/kWh). The difference is mainly due to the higher usage of
 12 the gasifier increasing the O&M costs, the lower LHV of Cassava, and the higher investment costs considered
 13 for the installation (4.45 USD/kWh), which were based on African mini-grids literature [83].

14 Finally, the breakeven grid extension distance for Mumbeji was also evaluated, obtaining a value of 70.2 km.
 15 Calculation is based on [19], [74], [84], using a capital cost of 5,000 USD/km, an O&M cost of 160 USD/km/y
 16 and a grid power price of 0.02USD/kWh. As the nearest electricity transport line is more than 150 km away,
 17 the HRES results in a cost-effective solution for the electrification of the community.

18 **4. Discussion**

19 The simulation proposal resulting from this research has enabled the simulation of the performance of a
 20 gasifier in two HRES case studies combining PV, biomass gasifier, and batteries; one in Honduras and the
 21 other in Zambia. For this purpose, the already in-built model of a biogas electricity generator has been used.

22 The results obtained are fully consistent with the scarce literature found on the HOMER simulation of HRES
 23 combining the same RES. See Introduction. Of this literature, only the paper by Chambon *et al.* and Alfonso-
 24 Solar *et al.* can be considered detailed on the modelling of the gasifier in HOMER [43], [49]. However,
 25 Chambon *et al.* does not explain the LHV of the biogas, the *electric* generation ratio, nor the mode of

1 operation in the schedule (only downtime of 48 to 120 hours every 1,500 to 2,000 hours of operation). In that
2 paper, the minimum load ratio is set at 30%, as in the HRES of Islam *et al.* [33] while in the rest of the sources
3 there is no data. Regarding the paper from Alfonso-Solar *et al.*, while they include the biomass and syngas
4 characteristics, they do not provide the syngas output to biomass input nor the justification of the usage
5 patterns of the gasifier. No other paper has been found to explain how to set the schedule of the gasifier.

6 In the following proposed models, a CAPEX of 2 USD/kW has been set based on the manufacturer and in
7 the literature, which was found between 1.1 USD/kW [33] and 3.64 USD/kW [49]. Replacement costs vary
8 between 1,000 USD/kW and 20,000 hours of operation in [33] and 2,909 USD/kW in [49], who consider
9 150,000 hours of a gasifier's lifespan without distinguishing between operating and idle hours. Moreover, an
10 O&M cost of between 0.03 USD/h [49] and 0.10 USD/h [85] has been found, and in this paper is 0.072
11 USD/h. The LCoEs found ranges between 0.16 USD/kWh from Suresh *et al.* [28] and 0.21 from Chambon
12 *et al.*[49], which leaves the LCOE of the Zambian case very high. However, it should be noted that in the
13 case of Chambon *et al.* when they lower the blackout allowance from 4% to 0%, the LCoE rises rapidly to
14 0.8 USD/kWh, while in the Zambian case 2% is allowed.

15 Furthermore, although it is a critical parameter for the simulation, only Chambon *et al.* give the gasification
16 ratio: 2.5 kg gas/kg biomass [49], which is within the range from 1.8 to 3.3 estimated in this study. In the case
17 studies 1.9 kg/kg are considered for Honduras and Zambia, which is on the safe side. While the literature on
18 gasifiers proposes an LHV for the biomass of between 12.5 and 19.0 MJ/kg [76], only Suresh *et al.* [28] give
19 the figure: 18.81 MJ/kg for forest foliage. In the presented case studies, the LHV considered is 15.55 MJ/kg
20 for wood in Honduras and 9.36 MJ/kg for cassava in Zambia. On the contrary, biomass prices do occur and
21 vary between 0.3 USD/ton of Suresh *et al.* [28] and 58 USD/ton of Chambon *et al.* [49].

22 In contrast, it is worth arguing that there are social variables that must also be considered in the simulation.
23 As the difference in operation between the Honduran and Zambian cases shows, if no minimum load ratio is
24 set, the optimum performance is reached with the gasifier in continuous operation. But this is not desirable
25 because of the need for constant attention by a community member (mainly feeding it), and the higher O&M
26 costs for too much operation and too little generation. Thus, unless the gasification technology is used as a
27 base one and not as backup, setting a minimum load ratio improves the gasifier's operation. Indeed, in
28 Honduras's case (Figure 5) the gasifier operates mainly at its maximum capacity (mean power output 24.7
29 kW), whereas in the case of Zambia (Figure 6) there is a mean electrical power output of 7.22 kW. In that
30 regard, the biomass storing and the periodicity in the feeding of the gasifier should be controlled to avoid
31 operational failures. Therefore, the minimum load ratio and the schedule must be set in a coordinated way
32 for a socially acceptable operation of the equipment.

1 The authors find that the social acceptability of a project is key to ensure the success of a rural electrification
2 project [5], [86]. Usage hours of the gasifier should be compatible with living patterns in the community. In
3 this regard, modelling the operation hours of the gasifier remains crucial to ensure that the optimised hours
4 are not only ideal from a technological perspective but also from a social acceptance one. Another concern
5 arises regarding the payments needed to sustain the resource flow to the gasifier and its operation. Specific
6 payments regarding obtaining the resource and the hours of management may generate problems among
7 the community. This results in the need to understand that variable costs of the gasifier may vary or not be
8 used as designed if the opinion of the community is not considered in a first design. Nevertheless, producers
9 and consumers' communities of energy, energy "Prosumers" communities, are in a better position to move
10 from energy poverty to the understanding of the technicalities and externalities of the supply, to manage, and
11 maintain the power system and to include all participants of the energy community in its benefits [87].

12 Finally, the simulation results prove biomass gasifiers are a dispatchable energy source that enables
13 valorising biomass resources or biomass waste to generate electricity in key moments. The inclusion of this
14 technology allows HOMER to optimise the HRES performance and achieve lower LCoE of the system without
15 compromising its reliability.

16 Hence, gasification serves three main purposes and benefits in an HRES: first, it delivers capacity during
17 peak demand hours and ensures a flexible resource for future demand increases as can be seen in Figures
18 5 and 6. Second, it ensures the security of supply of the HRES during adverse weather events such as
19 consecutive days of low solar irradiation, avoiding in this way designing a system with over-generation and
20 storage capacity as seen in Figures 7 and 8. Besides, the operation of batteries is improved by not allowing
21 them to go below certain SoC levels by being switched on to supply electricity to the community and charge
22 the battery bank as shown in Figures 7 and 8. Third, gasifiers contribute to optimising the initial capital costs
23 to solve the energy poverty of isolated and rural areas without access to electricity without compromising the
24 SDG7. Their dispatchability helps HRES to compete in reliability and cost with the alternative to electrifying
25 rural areas, the grid extension.

26 **5. Conclusion**

27 This study proposes a complete procedure to model a biomass gasifier in HOMER. For this, the biogas pre-
28 set energy source in HOMER is taken due to the absence of gasifiers as a generation technology. To prove
29 the feasibility of the simulation proposal two case studies were carried out. On the one hand, the models of
30 the gasifiers were included in HOMER. On the other hand, the viability of gasifiers as dispatchable renewable
31 energy is confirmed if the biomass resource is available, as well as its benefits for the beneficiaries of the

1 HRMES. This paper advances ongoing research and, particularly, one of the hybrid power plants of the case
2 studies is currently being executed.

3 To model a gasifier in HOMER numerous parameters must be set up, such as fuel consumption, operation
4 hours, and output power, among others. This fact presents the disadvantage of needing to determine not
5 only the biomass properties but also the syngas, assimilable to biogas produced in HOMER, and the
6 performance of the generator when converting biomass into syngas. However, those are data that gasifier
7 technology suppliers and the literature provide for a reliable model of gasifier performance. The availability
8 of biomass resources, in turn, is normally more readily available than other data on renewable resources, as
9 biomass plays a key role in energy for poor, isolated rural communities.

10 The proposal enables us to completely model biomass gasifiers in HOMER with realistic results. All the
11 HOMER parameters that too often are left "by default", or where left unexplained (and thus not-replicable)
12 could be estimated following this process: the biomass characteristics, the ratio of biomass input to syngas
13 output, the characteristics of the syngas, the performance of the gasifier, etc. This will help designers and
14 researchers to reliably include this technology in their analysis of biomass gasifiers' potential for all types of
15 applications in HOMER. Of particular interest is the participation of gasifiers as power systems (backup or
16 not) in off-grid HRES for energy-poor isolated communities, provided there is a sufficient supply of dry
17 biomass. These HRES help to mitigate climate change and help the energy-poor communities to better adapt
18 to it, to align their development with national, and international sustainable development strategies,
19 particularly SDG7.

20 Moreover, should the grid reach the community over time, the power plant will still help to reduce the energy
21 costs, keep the greenhouse gas emissions low, and preserve the reliance of the community against
22 blackouts, prices increase, or even fuel poverty, understood as the incapability to pay the price of the energy
23 they have access to.

24 Furthermore, based on the results of the case studies in El Santuario and Mumbeji, an HMRES including a
25 gasifier as a backup system achieves competitive LCoE of electricity: in El Santuario around 0.06 USD/kWh,
26 below the typical Honduran residential electricity price of 0.12 to 1.14 USD/kWh. The obtained value is higher
27 for the case of Mumbeji: 0.48 USD/kWh. However, it is still lower than extending the electric grid to the
28 community. Besides, the simulation shows the importance of correctly setting the free minimum load ratio,
29 the higher maximum load peak, and the lower biomass cost. The continuous operation in Mumbeji's case is
30 less convenient than the in El Santuario's. The simulation forced the gasifier to act as a backup system, but
31 in both cases the gasifiers have a wide margin to increase their energy generation (if there is enough
32 biomass) as they are delivering less than 30% of their peak power. The gasifier is activated when the

1 batteries' SoC is close to 30%, thus covering the demand of the community while charging the batteries. This
2 arrangement will prolong the life of batteries, around 40% of the CAPEX in both HMRES. This way, the
3 gasifier ensures the reliability and continuity of the energy supply in El Santuario, with only 1.26 kWh/yr that
4 will not be met (0.002%). In Mumbeki, the unmet load is 1,537 kWh/yr (0.99%).

5 Nevertheless, in contrast with its potential, modelling biomass gasifiers in HOMER may not be considered
6 as essential elements of their daily operation, maintenance, costs, and necessities, which are relevant, and
7 which designers ought to consider. Gasification has a potential environmental impact such as overharvesting,
8 deforestation, and waste mismanagement. Social implications arise from the community usage times of the
9 gasifier and the cost structure and payment of its management. Finally, physical-chemical characteristics
10 and the energy transformation process of the biomass must be carefully considered so as not overestimate
11 the potential of the technology and resource.

12 Other issues to be concerned with are that dry biomass and agricultural waste are the main energy sources
13 of most rural areas without access to electricity. Biomass is used for cooking lighting and heating in these
14 areas with a common rules-based management that prevents deforestation. The usage of dry biomass to
15 generate electricity is a sensitive issue and may lead to deforestation patterns following the Jevons paradox.
16 Consequently, when modelling gasifiers these concerns must be considered in the total biomass resource
17 of the model and transferred to the community to ensure the proper management of the common resources.
18 Moreover, if agricultural waste is used to power gasifiers, the community requires seasonal storage systems
19 that need to be counted in the cost structure of the system. The storage needs to be managed properly in
20 order to minimise property loss due to anaerobic degradation, ensure proper humidity conditions, and avoid
21 spontaneous ignition. Thus, since the cost structure, biomass resource use and usage patterns vary
22 according to the project country, local data must be considered in order to project the economic balance of
23 the system and introduce the above-mentioned design components of HOMER.

24 Finally, and also as discussed, the social acceptability of a project is key to ensuring the success of a rural
25 electrification project. Using hours of the gasifier, payments of the fuel, etc. should be compatible with living
26 patterns in the community. Nevertheless, communities of energy prosumers are more competent and resilient
27 to all these challenges.

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