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Discrete swarm intelligence optimization algorithms applied to steel–concrete composite bridges

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ABSTRACT

Composite bridge optimization might be challenging because of the significant number of variables involved in the problem. The optimization of a box-girder steel–concrete composite bridge was done in this study with cost and CO_2 emissions as objective functions. Given this challenge, this study proposes a hybrid algorithm that integrates the unsupervised learning technique of k-means with continuous swarm intelligence metaheuristics to strengthen the latter's performance. In particular, the metaheuristics sine-cosine and cuckoo search are discretized. The contribution of the k-means operator regarding the quality of the solutions obtained is studied. First, random operators are designed to use transfer functions later to evaluate and compare the performances. Additionally, to have another point of comparison, a version of simulated annealing was adapted, which has solved related optimization problems efficiently. The results show that our hybrid proposal outperforms the different algorithms designed.

1. Introduction

Bridge optimization is an interesting problem to address both because of the technical challenges that the problem presents and because of the potential applications in reducing costs, CO_2 emissions, and energy consumption. The technical difficulties are related to the large number of discrete variables required in its design and the complex objective functions and restrictions that these must satisfy [1]. Due to the more significant number of variables necessary for their design, Steel–Concrete Composite Bridges (SCCB) present a considerable challenge. According to the SCCB literature, they can be classified into three groups according to their cross-section: Plate-beam, Twin-Girders, and Box-Girder [2], and their behavior are different between these types.

Due to the type of objective function and the constraints used in structural design problems, metaheuristics (MH) have had good results in optimizing structures. These techniques have been applied in steel structures [3], arch bridges [4,5] or reinforced concrete columns [6] among others. In some studies, metaheuristic has been applied as first optimization step for topological optimization [7] due to the computational cost of this last method [8]. In particular, metaheuristic techniques have performed well in addressing complex SCCBs optimization [9]. For example, in [10] a discrete harmony search algorithm was proposed and applied to the design of multi-span composite box girder bridges. In the article, the authors obtained a 15% reduction of

materials when compared to a traditional design. In [11], a two-stage based optimization methodology is developed for the design of simply supported steel-concrete composite I-girder bridges. In the first stage, a simplified structural model based on expert criteria is developed and used with the aim of providing a starting point for the local search. In the second stage, a search group algorithm is chosen based on statistical analysis. The proposed method was shown to reduce the structural cost by up to 9.17%. Three metaheuristic algorithms were studied in [12] and used for reaching the optimal design of steel-concrete composite I-girder bridges. The algorithms used were Collision Bodies (CBO), Collision Body Enhanced Optimization (ECBO), and Vibration Particle System (VPS). Among the results, it was obtained that the final optimized design does not need longitudinal stiffeners.

Despite the excellent performance of metaheuristics and the large size of many combinatorial problems, the strengthening of metaheuristics is also necessary. Among the different strategies to strengthen the metaheuristics, the hybrid methods have stood out. Several of the most frequently utilized hybridization techniques, include *hybrid heuristic*, [13], where different metaheuristic algorithms are combined to enhance their capabilities. *Mateheuristics*, [14], where mathematical programming methods are integrated with metaheuristics techniques. *Simheuristics*, [15], which encompass a combination of simulations with metaheuristic modeling.

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Metaheuristics generate important ancillary data in the solution search process, which can be exploited by machine learning methods. This opens a line of research in which machine learning techniques can be integrated into metaheuristic algorithms to strengthen the performance of the latter.

When searching for integration types in which machine learning techniques improve the performance of metaheuristic algorithms, three main categories are found. Low-level integrations, high-level integrations, and optimization problems [16,17]. In the case of the hybrid algorithm proposed in this article, the type of integration designed is a low-level integration. The low-level integrations involve local search operators, population initiation, binarization, parameter control, in which ML approaches improve particular operators of the MH algorithm. For example in parameter tuning, in [18], an iterated racing method was employed; a reset mechanism was combined with an elitist procedure (to assure the optimal configuration), and the use of a truncated sampling distribution to allow for automated parameter setting. Decision trees were utilized in [19] to modify particular parameters in the traveling salesman problem. Compared to fixed parameter values, the decision tree technique improved the quality of the solutions and the computing time. Another case of low-level integration is used to initialize solutions. For the shop scheduling problem [20], decision trees were utilized to produce early solutions for new instances, in conjunction with Opposition Based Learning (OBL), to begin complementary solutions. Reinforcement Learning (RL) and other approaches can also be utilized to create solutions. In these situations, the solution building may be thought of as a series of additions of decisions, for which an RL algorithm can be trained. For example, a Deep Q-network was constructed and utilized for the optimization of the Job-Shop Scheduling Problem [21]. Similarly, in [22], transfer learning approaches were utilized to generate initial solutions using three evolutionary multiobjective algorithms and applied to 12 benchmark functions. Finally, another successful application of low-level integration has been used to generate binary versions of algorithms that work on continuous spaces.

Another essential field of study is the creation of binary versions of algorithms that function in continuous areas naturally. There are some examples of ML and metaheuristics working together in this field. The K-means approach was utilized to build binary versions of the cuckoo search algorithm (CS) and used to the matrix covering problem in [23]. For the multidimensional knapsack problem, in [24] a hybrid algorithm using k-means as the binarization method and KNN as the local search operator is proposed. The hybridization between metaheuristic techniques with the aim of improving the convergence or quality of the solutions is another interesting line of low-level integration. In [25], the hybridization of hybrid metaheuristic algorithms was proposed with the aim of addressing the optimal dimensioning of steel beam structures with numerous discrete variables. The numerical results indicate that the hybrid algorithm of adaptive dimensional search and exponential big bang-big crunch is the most promising of the techniques investigated. In [26], it is integrated the convergence curve of each subsequent execution of the algorithm in relation to the information gained from prior executions. It is monitored at specified times during each subsequent execution, referred to as the solution monitoring period. The solution monitoring period is chosen in such a way that each run allows the algorithm to explore the search space in order to increase the quality of the solution, while also periodically forcing the algorithm to return to the most promising prior visit. If it is unable to improve the solution after a specified number of iterations, it will terminate. Numerical investigations with tough test examples containing up to 354 design variables reveal that, in general, the proposed approach improves the solution quality and the robustness or stability of the outcomes in metaheuristic structure optimization.

Following this last line of generating binary versions to efficiently solve binary optimization problems. In this article, the integration method has been adapted to address discrete problems. In particular, a discrete hybrid algorithm is proposed. This algorithm incorporates the k-means technique into the discretization solution phase of continuous swarm intelligence metaheuristics. The contribution of this work includes:

- In this study, a cost, and CO₂ emissions optimization of a 60-100-60 three-span single box-girder steel–concrete composite bridge has been performed.
- It should be noted that it considers 35 design variables on average 55 possible choices for each variable, which implies a computationally demanding structure.
- A discrete hybrid k-means swarm intelligence algorithm is proposed, and the contribution of the k-means technique to the robustness of the algorithm is studied. In particular, it should be noted that in previous works [24,27], k-means has been used to solve binary optimization problems, that is, whether the variable is present or not. In the optimization developed in this article, the technique was adapted to allow more than two states for each of the variables.
- The results of the hybrid algorithm are compared with discrete simulated annealing that has been efficient in solving related problems [28], in addition to considering the comparison with algorithms that perform discretization through transfer functions that are frequently used to binarize or discretize solutions [29].

A brief content structure of the following sections: In Section 2, the box-girder steel-concrete composite bridge problem is detailed. Later, in Section 3, the discrete k-means swarm intelligence algorithm is developed. Our numerical experiments and comparisons are detailed in Section 4. Finally, in Section 5, the conclusions and future lines of research are discussed.

2. The optimization problem and computational model

This section aims to define and detail the optimization problem. In the case of bridges, there are different objective functions to be minimized, among which there is a particular interest in the costs of the bridge and the CO₂ emissions released in the manufacture of its materials. In this work, two mono-objective functions are defined. The first shows the bridge's overall cost, which is formalized in Eq. (1) and is calculated by multiplying the unit cost of each material c_i , multiplied by the units used, m_i . In the case of CO₂ emissions, the calculation is similar to the previous one, with the difference that instead of considering cost, the emissions e_i considers cradle-to-gate analysis for each unit of material *i* multiplied by the amount of material *i* used. The emissions calculation is formalized in Eq. (2). For the cost function, the values from Table 1 are used, which were obtained from the Construction Technology Institute from Catalonia by the BEDEC database [30]. Finally, the bridge design process is subject to constraints imposed by expert recommendations and regulations related to the standard. Generically, these are shown in Eq. (3).

$$C(\vec{x}) = \sum_{i=1}^{n} c_i \cdot m_i(\vec{x}) \tag{1}$$

$$E(\vec{x}) = \sum_{i=1}^{n} e_i \cdot m_i(\vec{x})$$
⁽²⁾

$$G(\vec{x}) \le 0 \tag{3}$$

For the description of the problem, the variables, parameters, and constraints of the problem will be considered. In the case of variables, they correspond to the values modified in the optimization procedure to achieve the optimum. In the case of parameters, they are values that are considered fixed in the optimization, and that usually represent boundary conditions. Finally, the constraints are imposed by regulations [31–33] and recommendations of specialists [2,34].



Fig. 1. Transverse section variables for SCC bridge.

Table	1		

Cost and CO_2 emission values.		
Unit	Cost (€)	Emissions (kg of CO_2)
m ³ of concrete C25/30	88.86	256.66
m ³ of concrete C30/37	97.80	277.72
m ³ of concrete C35/45	101.03	278.04
m ³ of concrete C40/50	104.08	278.04
m ² of precast pre-slab	27.10	54.98
kg of steel B400S	1.40	0.70
kg of steel B500S	1.42	0.70
kg of rolled steel S275	1.72	4.33
kg of rolled steel S355	1.85	4.33
kg of rolled steel S460	2.01	4.33
kg of shear-connector steel	1.70	2.8

2.1. Variables of the problem

Our optimization problem is a Steel-Concrete Composite Bridge (SCCB) with a box-girder cross section divided in three spans of 60-100-60 m. The problem variables can be grouped into two groups. The first group correspond to the geometric variables of the bridge and the second group with grades of steel and concrete. In order to design bridges that are feasible to build, these variables cannot take any value, but only allowed values, with which our search space corresponds to a discrete space. Variables are shown in Table 2. These variables, depending on their characteristics, are grouped into five categories. The first category correspond to geometric variables of the transverse section. Upper distance between wings (b), wings and cells angle (α_w) , top slab thickness (h_s) , beam high (h_b) , floor beam minimum high (h_{fb}) , top flange thickness (t_{f_1}) , top flange width (b_{f_1}) , top cells high (h_{c_1}) and thickness (t_{c_1}) , wing thickness (t_w) , bottom cells high (h_{c_2}) , thickness (t_{c_2}) , and width (b_{c_2}) and bottom slab thickness (h_{s_2}) . For clarity, these variables are outlined in Fig. 1.

The second category of variables corresponds to the diameters of the base reinforcement, first reinforcement and second reinforcement bar diameters (ϕ_{base} , ϕ_{r_1} , ϕ_{r_2}), and the corresponding bar number of the reinforcement areas (n_{r_1} , n_{r_2}). These variables are intended to improve the bridge transverse section. To optimize the top slab reinforcement, it has been divided into a base reinforcement that is the minimum required by regulations [31–33] and two more areas, in negative bending sections, where the reinforcement is increased. The lower slab and the lengths of the increasing area of reinforcement will be described in Section 2.2.

Design variables and boundaries.									
Variables	Unit	Lower bound	Increment	Upper bound	Values number				
Ь	m	7	0.01	10	301				
α_w	deg	45	1	90	46				
h_s	mm	200	10	400	21				
h_b	cm	250	1	400	151				
h_{fb}	mm	400	100	700	31				
t_{f_1}	mm	25	1	80	56				
b_{f_1}	mm	300	10	1000	71				
h_{c_1}	mm	0	1	1000	101				
<i>t</i> _{c1}	mm	16	1	25	10				
t_w	mm	16	1	25	10				
h_{c_2}	mm	0	10	1000	101				
t _{c2}	mm	16	1	25	10				
b_{c_2}	mm	300	10	1000	71				
t_{f_2}	mm	25	1	80	56				
h_{s_2}	mm	150	10	400	26				
nsi	u	0	1	10	11				
d _{st}	m	1	0.1	5	41				
d_{sd}	m	4	0.1	10	61				
b _{fb}	mm	200	100	1000	9				
$t_{f_{fb}}$	mm	25	1	35	11				
$t_{w_{ch}}$	mm	25	1	35	11				
n _r	u	200	1	500	301				
n _{ro}	u	200	1	500	301				
ϕ_{base}	mm	6, 8, 10, 12, 1	6, 20, 25, 32		8				
ϕ_{r_1}	mm	6, 8, 10, 12, 1	6, 20, 25, 32		8				
ϕ_{r_2}	mm	6, 8, 10, 12, 1	6, 20, 25, 32		8				
s fa	mm	From IPE 200	to IPE 600 ^a		12				
s _w	mm	From IPE 200	to IPE 600ª		12				
s _t	mm	From IPE 200	to IPE 600ª		12				
h _{sc}	mm	100, 150, 175,	200		4				
ϕ_{sc}	mm	16, 19, 22			3				
f_{ck}	MPa	25, 30, 35, 40			4				
f_{yk}	MPa	275, 355, 460			3				
f_{sk}	MPa	400, 500			2				

^aFollowing the standard series of IPE profiles.

The stiffeners correspond to the third category of variables. In this design, half IPE profiles for wings (s_w) , bottom flange (s_{f_2}) and the transverse ones (s_t) are considered variable stiffeners. For bottom flange stiffeners, the number of stiffeners $(n_{s_{f_2}})$ has also been considered as a variable. As can be seen in Fig. 1, there are two more variables that define the distance between diaphragms (d_{sd}) and transverse stiffeners (d_{st}) .

16	m		
3			
100	m		
60	m		
15	mm		
25	mm		
45	mm		
20	mm		
$22 \cdot ((f_{ck} + 8)/10)^3$	MPa		
$E_{cm}/(2 \cdot (1+0.2))$	MPa		
210 000	MPa		
80769	MPa		
Eurocodes [31-33,3	35], IAP-11[36]		
XD2			
S5			
100	years		
25	kN/m ³		
78.5	kN/m ³		
24	kN/m ³		
100	mm		
5.6	kN/m		
According to the codes			
According to the codes			
According to the co	odes		
	16 3 100 60 15 25 45 20 22 $\cdot ((f_{ck} + 8)/10)^3$ $E_{cm}/(2 \cdot (1 + 0.2))$ 210 000 80 769 Eurocodes [31–33,5] XD2 S5 100 25 78.5 24 100 5.6 According to the co According to the co		

The last two categories correspond to the geometry of the shear connector's characteristics, and the floor beam variables. The floor beam variables are defined by the width of the floor beam (b_{fb}) and the thicknesses of the flanges (t_{ffb}) and webs (t_{wfb}) . Shear connectors have been defined by their height (h_{sc}) and diameter (ϕ_{sc}) . Finally, the elastic limit of rolled steel (f_{yk}) , the strength of concrete (f_{ck}) and the elastic limit of reinforcing steel bars (f_{sk}) complete the definition of the variables.

2.2. Parameters of the problem

In each optimization problem, it is necessary to set some variables, typical of the conditions to which the structure will be subjected, defined by some regulation, environmental conditions, or some geometric definition that has no need or the possibility of changing. These fixed attributes are called parameters and remain unchanged throughout the optimization process. The parameters and values defined in the bridge design are summarized in Table 3.

Considering the Eurocode regulations [31,32], that our bridge is a 60-100-60 m three-span box-girder steel–concrete composite bridge with a deck width (*B*) of 16 m without height variation, for cells have been defined in the transverse section for improving the resistant behavior. These cells are shown in Fig. 1. Two cells are at the upper side of the wings, and the other two are at the bottom. The minimum height of these cells, (h_{c_1}, h_{c_2}) , has been set to zero in order to identify if they contribute to the reduction of costs or emissions of CO₂ additionally for set the upper limit of these, the bridge design rules defined in [34] has been considered.

The base reinforcement for the upper and lower concrete slab is set according to the minimum need for reinforcement defined in Eurocode 2 [33]. The connection between the concrete slab and the steel beam is dimensioned to resist the shear lag stresses produced in the top flanges. For bending resistance the effective width given by Eurocode 4 [31] have been considered. Also, because the only width considered resistant is effective, the defined steel bar reinforcements are placed only in that width. Finally, steel bar reinforcement increase and lower slab areas are defined. The lower slab is placed in negative bending sections to mobilize the composite dual-action. To define lengths where negative bending can be produced, we have considered the distance defined by Eurocode 4 [31] for shear lag stresses that correspond with one-third of the span length. As stated earlier, it is necessary to increase the upper slab reinforcement to resist the tension stresses produced. In this case study, we have considered two reinforcement areas. The first is placed in zones where the section can be subjected to negative bending, and base reinforcement cannot resist the stresses. The second is placed on top of supports, corresponding to one-third of the distance between the support and the point of change of sign of the bending of the theoretical law.

2.3. Constraints of the problem

In designing a structure, the constraints imposed by regulations and specific conditions to the structure, such as safety factors, must be considered. Mainly, in the optimization of this bridge, the necessary constraints to consider are defined in the regulations, [31– 33] and additionally, recommendations defined in, [2,34] have been incorporated.

When analyzing the regulations, it is found that the constraints imposed make up two groups: The first one corresponds to the Ultimate Limit States (ULS) and the second group, to the Service Limit States (SLS). In the case of ULS, the restrictions are related to the structural resistance of the bridge elements subjected to the stresses caused by the acting loads. In the case of SLS, the restrictions are intended to ensure the serviceability of the structure during its useful life. All applied loads and their combination are defined in the [35] regulation. The Table 3 summarizes the load cases considered.

In order to verify the ULS restrictions in all the elements of the bridge, both the global and the local analyses have been considered. In the case of the global analysis, the checks consider shear, flexure, torsion, and flexure-shear interaction. To obtain stresses and deflections, a linear elastic analysis has been considered. When considering [31,32], these indicate that the resistance of the section must be included, in our design, the effective section has been selected and applying it both the shear lag reductions and the reduction of the section of steel plates classified as class 4. To achieve the above, a precision of 10^{-6} m has been considered for the iterative process. To obtain the value of the mechanical characteristics of the homogenized section, the relationship (n) between the longitudinal deformation modulus of concrete (E_{cm}) and steel (E_s) has been obtained according to Eq. (4). For the case of concrete creep and shrinkage, they were defined following the [31,33] standard. Likewise, a local model was developed to verify the beams, reinforcements, and diaphragms in the ULS floor, considering controls for shear, flexure, buckling, and minimum mechanical characteristics.

$$n = \frac{E_s}{E_{cm}} \tag{4}$$

The SLS considered for the analysis is the tension limit for materials, fatigue, and deflection. There is no apparent limit for deflection in Eurocodes, but the IAP-11 Spanish regulation [36] gives a maximum of L/1000 for the frequent combination of live loads deflection value, with L representing the span length. This has been considered as the maximum value of the deflection. In addition, we have considered geometrical and constructibility requirements.

Additionally, a numerical model has been implemented to obtain the stresses and carry out all the ULS, SLS, and geometric and constructibility checks. In the case of deflections and stresses, the model applies the perfect embedding forces method, taking the 34 bridge variables we selected as input data. The model divides each span of bridge into a defined number of bars. In this case, the total number of bars is 44, distributed in 12-20-12 corresponding to the three spans of the bridge; thus, discretize the bridge into bars of 5 m in length. Once the stresses have been obtained, the program performs structural checks and returns the measurement results, cost, emissions, and verification coefficients. These verification coefficients correspond to the quotient between the design values of the effects of the actions (E_d) and their corresponding resistance value (R_d) , as shown in Eq. (5). If these coefficient values are greater than or equal to one, then the Section complies with the imposed restriction.

$$\frac{R_d}{E_d} \ge 1 \tag{5}$$

2.4. Structure computational model description

The procedure used to obtain the deflections and stresses has been the perfect embedding forces method. This method consists in solving Eq. (6).

$$\mathbf{f} = \mathbf{K} \cdot \mathbf{d} + \mathbf{f}_0 \tag{6}$$

In this equation, \mathbf{f}_0 correspond to the perfect embedding forces vector. These forces would be obtained if each of the system bars had all the degrees of freedom constrained. **K** is the stiffness matrix of the system, generated by assembling the stiffness matrices of all bar elements. To get the stiffness matrix of each element, the average between both frontal and dorsal nodes' mechanical properties has been calculated. The complete section without considering the shear lag and panel reduction has been considered to obtain these mechanical properties. Finally, **d** and **f** are the deflections and stress vectors, respectively.

This procedure is repeated with all load cases. The following load cases have been considered loading the entire bridge length as a single load case: Self Weight, Dead Loads, Thermal Heating, Thermal Cooling, and Wind. In order to consider the different positions of traffic loads, every 5-m bar has been loaded separately, considering two separated loading cases, the punctual load and the distributed. This gives, as a result, 88 load cases for traffic load and a total of 93 if all load cases are considered. The results obtained from loading each bar have been combined to consider all loading possibilities regarding traffic load. After this, the load case envelope has been calculated to consider each section's maximum and minimum results.

Regarding combinations and envelopes, the envelope of all persistent and transitory situations combinations have been obtained for ULS. These combinations have been considered dominant action all live loads in different combinations. The envelope of all characteristic combinations has been considered for SLS regarding stress limitation.

3. Optimization algorithms

The detail of the discretization algorithms will be explained in this Section. First, the metaheuristics used to perform the optimization will be detailed in Section 3.1. Then the proposed hybrid algorithm, Section 3.2, which uses k-means as the discretization method will be explained. Later in Section 3.3, the algorithm that uses a transfer function as a discretization method is detailed. The following reference is recommended for a greater depth of transfer functions and their applications in combinatorial optimization [29]. We must emphasize that the k-means discretization method takes all the solutions, groups them, and later assigns the probabilities. In the case of transfer functions, each probability is assigned individually, without looking at the other solutions.

Fig. 2 shows the flowchart used to perform the optimization using cuckoo search and the sine cosine algorithms (SCA). As a starting point, the set of solutions is initialized, this set corresponds to a valid set, that is, it complies with the constraints imposed by the problem. Once the solutions have been initialized, it is asked whether the stopping criteria of the algorithm are met. In this case, the stopping criterion of the algorithm corresponds to the maximum number of defined iterations. In the event that the maximum number of iterations has not been

met, the hybrid algorithm is executed. As a first stage of the hybrid algorithm, the set of velocities for the different generated solutions is obtained. Subsequently to the set of solutions, the k-means clustering technique is applied in order to group the solutions and assign a transition probability to each group in the transition probabilities stage. The detail of these three stages will be explained in Section 3.2. Finally, a solution update criterion is established, in which it is evaluated if each of the variables or dimensions associated with a solution is updated. This is intended to balance the exploitation and exploitation of the search space. Solutions with good values of the fitness function will have few updates to be able to exploit the space. The detail of this update will also be made in Section 3.2

3.1. Swarm intelligence algorithms: SCA and CS

This section details the swarm intelligence algorithms used to address optimization. Specifically, the cuckoo search was chosen as it has successfully solved a large number of optimization problems, particularly in the area of civil engineering. Additionally, the parameterization of the original algorithm is quite simple. In the case of the sine cosine algorithm, the type of move it executes is based on the sin and cosine functions and is completely different from the move of cuckoo search. On the other hand, this last metaheuristic does not require proper parameter tuning.

3.1.1. Sine Cosine Algorithm (SCA)

Sine Cosine Algorithm (SCA) was proposed in [37] and corresponded to a swarm intelligence algorithm that considers the sine and cosine functions to carry out the process of exploring and exploiting the search space. To carry out the movement of the solutions, P_i^t is additionally used, which corresponds to the position of the destination solution for iteration t and dimension j, and typically uses the best solution obtained so far. In addition to P_i^t , the algorithm uses four random numbers r_1, r_2, r_3, r_4 . As the algorithm starts to iterate, r_1 decreases. It starts at 2 and converges to 0 at the end of the optimization. On the other hand, r_2 takes values between 0, 2π . r_3 considers values between 0 and 2, and finally r_4 is used to select Eqs. (7) and (8) taking values between 0 and 1 and a threshold of 0.5.

The update method used is shown in Eqs. (7) and (8).

$$x_{i,j}^{t+1} = x_{i,j}^t + r_1 \times sin(r_2) \times |r_3 P_j^t - x_{i,j}^t|$$
(7)

$$x_{i,j}^{t+1} = x_{i,j}^t + r_1 \times \cos(r_2) \times |r_3 P_j^t - x_{i,j}^t|$$
(8)

3.1.2. Cuckoo search algorithm (SC)

The reproductive strategy phenomena observed in cuckoo species, which lay their eggs in the nests of other bird species, has inspired the CS algorithm. Such is the level of sophistication of cuckoo birds that in some cases even the colors and patterns of the eggs of the chosen host species are mimicked. In the analogy, an egg corresponds to a solution. The concept behind the analogy is to use the best solutions (cuckoos) to replace those that do not perform well. The CS algorithm uses three basic rules:

- 1. Each cuckoo lays one egg at a time and deposits its egg in a randomly chosen nest.
- 2. The nests with the best results, that is, with high-quality eggs, will be considered in the next generation.
- 3. The number of nests available is a fixed parameter. The egg laid by a cuckoo can be discovered by the host bird with a probability $p_a \in (0, 1)$

In Eq. (9) the movement of CS is defined. The symbol \oplus , denotes entry-wise multiplication, whereas $\alpha > 0$ denotes the step size. This step size specifies the maximum distance that a particle can travel in



Fig. 2. Discrete hybrid k-means algorithm flow chart.

a random walk over a set number of iterations. The Lévy distribution modulates the transition probability of the Lévy flights in Eq. (10).

$$x_{i,i}^{t+1} = x_{i,i}^t \alpha \oplus levy(\lambda) \tag{9}$$

$$levy(\lambda) \sim g^{-\lambda}, (1 < \lambda < 3) \tag{10}$$

3.2. K-means discrete algorithm

In this subsection, the detail of the algorithm that allows discretizing the SCA and CS metaheuristics is explained, these MH, naturally work in continuous search spaces. The k-means discrete algorithm (KMDA), uses the unsupervised learning technique k-means to cluster the solutions. As input parameters, KMDA considers the list of solutions ISol, the metaheuristic MH to be discretized, and the list of transition probabilities *transitionProbs*, where each group obtained by applying k-means is associated with a value of transition probability. In line 4, KMDA uses the metaheuristic that is being discretized, for this case, SCA or CS, however, it can be any continuous swarm intelligence metaheuristic, and together with the list of solutions ISol obtained in

the previous iteration, the movement of the metaheuristic is applied, obtaining the velocity for each solution in the list of solutions. The calculation of the velocity for each dimension of the solution vector is done using the Eqs. (7) and (9). The velocity in the metaheuristics is considered by $ISol_{i,j} = |x_{i,j}^{t+1} - x_{i,j}^t|$. vISol identifies the list of velocities associated with the list of solutions ISol.

Once the list of solutions vlSol has been obtained, the next step corresponds to grouping the velocities using the k-means technique for a number K of clusters. This applies in line 5 of the algorithm. The objective of applying k-means is to generate groups where the elements of each group have similar characteristics. In this case the groups that have velocities with small values and that therefore in continuous space would move very little, will be related to small transition values in our discrete space. As a result of clustering, lSolClustered is obtained, where the cluster is stored for each of the components of each speed associated with the list of solutions lSol.

Subsequently, each component's *dimSol* cluster is considered for each solution, and a transition probability is assigned. For the case studied here, a K = 5 was used and with transition probabilities [0.1, 0.2, 0.4, 0.8, 0.9]. The smallest value of the transition probability is

Parameter setting for the hybrid cuckoo search algorithm.

0	5		
Parameters	Description	Value	Scanned range
Ν	Number of nest	10	[5, 10, 20]
γ	Step length	0.01	0.01
ĸ	Levy distribution parameter	1.5	1.5
Κ	Number of clusters	5	[4, 5]
Iteration number	Maximum iterations	600	[200, 400, 600]

assigned to the cluster with the lowest average velocity, and in that order, the probabilities are assigned. The assignment of the transition probabilities was established intuitively and supported by previous experiences when solving binary problems. Following the idea that the first two clusters have the smallest velocities, small transition probabilities are assigned, with the aim of favoring the exploitation of space. The last two clusters that have the highest velocities, are assigned high probabilities to favor exploration of the search space, and the middle cluster has a probability of 0.4.

Finally, using a random number r_1 it is determined if the component $lSol_{i,j}$, is updated or stays the same. The higher the probability of transition, the greater the probability of change. Additionally, it is used a random number r_2 , making the update be considering the best value or randomly. In our case $\beta = 0.8$. The KMDA pseudocode is shown in algorithm 1.

Algorithm 1 k-means discrete algorithm (KMDA)

Algorithm T K-means discrete algorithm (KWDA)
1: Function KMDA(ISol, MH, transition Probs)
2: Input lSol, MH, transitionProbs
3: Output ISol
4: $vlSol \leftarrow getVelocities(lSol, MH)$
5: $lSolClustered \leftarrow appliedKmeansClustering(vlSol, K)$
6: for (each Sol_i in $lSolClustered$) do
7: for (each $dimSol_{i,j}l$ in Sol_i) do
8: $dimSolProb_{i,j} = getClusterProbability(dimSol, transitionProbs$
9: if $dimSolProb_{i,j} > r_1$ then
10: if $beta > r_2$ then
11: Update $lSol_{i,j}$ considering the best.
12: else
13: Update $lSol_{i,j}$ with a random value allowed.
14: end if
15: else
16: Don't update the element in $lSol_{i,j}$
17: end if
18: end for
19: end for
20: return lSol

3.3. Transfer function discrete algorithm

In the case of the algorithm that uses transfer functions, the structure is very similar to KMDA. Specifically, a transfer function is applied that aims to bring the velocity values, which can take values in \mathbb{R} , to values between [0, 1). In this case, a v-shape transfer function, $|\tanh(v)| = |\frac{e^{x}-e^{-x}}{e^{x}+e^{-x}}|$, was used. The fundamental difference is that KMDA calculates the speeds and then applies clustering by analyzing all the values of the solutions. This can be seen in lines 4 and 5 of algorithm 1. In the case of transfer functions, this is done individually within the for loops on lines 6 and 7 of algorithm 2.

1:	Function Discretization(<i>lSol</i> , <i>MH</i>)
2:	Input ISol
3:	Output ISol
4:	for (each Sol in lSol) do
5:	for (each dimSol in Sol) do
6:	$vdimSol \leftarrow getVelocity(dimSol, MH)$
7:	$dimSolProb \leftarrow appliedTransferFunction(vdimSol)$
8:	if $dimSolProb > r_1$ then
9:	if $beta > r_2$ then
10:	Update $lSol_{i,j}$ considering the best.
11:	else
12:	Update $lSol_{i,j}$ with a random value allowed.
13:	end if
14:	else
15:	Don't update the element in $lSol_{i,j}$
16:	end if
17:	end for
18:	end for
19:	return lSol

4. Results

In this Section, the experiments developed to evaluate the behavior of the discrete hybrid algorithm are detailed, in addition to analyzing the findings found when optimizing the bridge. The results are divided into four subsections. In Section 4.1 it is explained how the selection of the hyperparameters used by the algorithm was made. Later in Section 4.2, the results of the experiments that identify the contribution of the algorithm in the optimization result are detailed. Later in Section 4.3, the results are compared with other implementations.

Python 3.6 was used to create the algorithm, along with a PC running Windows 10, a core i7 processor, and 32 GB of RAM. To see if the difference is statistically significant, the Wilcoxon signed-rank [38]method was used. The 0.05 *p*-value was chosen. The methods described in [39] was used to choose the test. The Shapiro–Wilk normality test is used initially in this process. The Wilcoxon signed-rank is recommended to check the difference if one of the populations is not normal and has the same number of points.

4.1. Parameter setting

The methodology used to select the correct parameters was adapted from the procedure defined [27]. To obtain an adequate selection of the parameters, we used three measures defined by the Eqs. (11) to (13). For the generation of values, each combination of parameters was executed five times. The set of parameters explored and selected for CS is shown in Table 4. For the calculation of the best performance, each of the indicators is constructed to have values between 0 and 1. The closer to 1, the better the performance. These values are plotted on a radar chart and the area under the curve is calculated. The set of indicators that takes the largest area, corresponds to the best performance.

1. The percentage deviation of the best value obtained in the specific execution, compared to the best value obtained of all the runs:

$$bSolution = 1 - \frac{BestTotalValue - BestValue}{BestTotalValue}$$
(11)

2. The percentage deviation of the worst value obtained in the specific execution, compared to the best value obtained of all the runs:

$$wSolution = 1 - \frac{BestTotalValue - WorstValue}{BestTotalValue}$$
(12)



Fig. 3. Cost boxplots for Random0.5, Random0.3, and SCA Algorithms.

 The percentage deviation of the average value obtained in the specific execution, compared to the best value obtained of all the runs:

$$aSolution = 1 - \frac{BestTotalValue - AverageValue}{BestTotalValue}$$
(13)

4.2. Insight into discrete algorithm

This Section aims to evaluate the contribution of the KMDA operator in the result of the optimization of the bridge. Two random discretization operators were designed, *Random*0.5 and *Random*0.3. Specifically, these operators do not execute the clustering in line 5 of the algorithm 1 or the probability assignment in line 8. The value of *dimSolProb*_{*i*,*j*} is replaced by 0.5 in the case of *Random*0.5 and 0.7 in the case of *Random*0.3 (30% probability of transition). The rest of the code remains unchanged. These operators were applied to the SCA metaheuristics and the bridge cost optimization problem. The results are shown in Table 5 and Fig. 3.

In Table 5, the result of 30 executions for each of the operators mentioned above, together with the descriptive statistics, are shown. In this experiment, the objective function corresponds to cost optimization. From each of the optimizations, the bridge that obtained the best cost is registered, the emissions obtained for that bridge, and the time it took for the optimization. In the case of the cost results, we see that Hybrid SCA obtains the best values and smaller dispersion of the results. When emissions are analyzed, we see that the Hybrid SCA case is more robust in all indicators. Additionally, the latter suggests an essential correlation between optimizing the cost of the bridge and reducing its emissions. The Wilcoxon test shows that the results are statistically significant. When the execution times are analyzed, the results are similar in the three evaluated operators. When comparing the cost boxplots, Fig. 3, we visually observe the robustness of Hybrid SCA against random operators.

4.3. Algorithm comparisons

This Section will evaluate KMDA's performance against other implementations that have effectively solved combinatorial problems. The first algorithm used was an implementation of simulated annealing (SA) proposed in [40] and used to optimize prestressed concrete precast road bridges and later applied to other structural design problems [28,41]. For the second comparison, the algorithm detailed in Section 3.3 is used, which performs the discretization procedure using the v-shape |tanh(v)| function. To make the comparison, all the algorithms are executed 30 times to optimize costs and 30 times to optimize CO₂ emissions. The results are recorded in Tables 6, and 7. Additionally, the results are shown through box diagrams in Figs. 4, and 5.

In Table 6, the cost optimization for SA, transfer SCA, hybrid SCA, and hybrid CS is shown. When analyzing the descriptive statistics, we see that the cost results obtained by the hybrid algorithms are very similar and superior to those for SA and transfer CSA in the minimum, maximum, average, and deviation obtained. When applying the Wilcoxon test, it indicates that the difference is not significant between the hybrid algorithms and if it is significant between hybrid SCA with respect to SA and transfer SCA. When applying the Wilcoxon test, it indicates that the difference is not significant between the hybrid algorithms and if it is significant between hybrid SCA with respect to SA, transfer SCA and transfer CS. In the case of the emissions obtained in cost optimization, we observe that both hybrid algorithms consistently obtain very similar results and are more robust than SA and transfer SCA. Again, the strong relationship between optimizing costs and reducing emissions of CO₂ is observed in the hybrid algorithms. When analyzing the times, we see that SA is 21.5% slower than Hybrid SCA, being this very similar to transfer SCA and hybrid CS. When comparing the boxplots, Fig. 4, the similarity of the hybrid methods is visually observed, and the robustness of the results concerning the other methods.

Table 7 shows the comparison between discrete algorithms that use k-means (Section 3.2), SA, and transfer functions (Section 3.3), optimizing CO₂ emissions. When analyzing the amount of CO₂ produced during the emissions optimization process, we see that the results of the hybrid method are better than the one that uses transfer functions and SA in all indicators. This is also visually verified by comparing the different boxplots in Fig. 5. However, when analyzing the costs obtained in the optimization of emissions, it does not behave equivalent to the optimization of costs. In this case, a significant dispersion is observed in all algorithms. The range between Max and Min is significant in all five algorithms. This correlation between cost optimization and emission reduction of CO₂ identified in Table 5, is related to the fact that the different grades of steel obtained from the BEDEC [30] database have the same amount of emissions. In the case of the CO₂ optimization, different elastic limit values are obtained for structural steel without producing essential variations in its objective emission function, but the highest in terms of cost.

In Table 8 the design variables results have been shown for cost and CO_2 optimization objectives. As it can be seen, there are some differences between cost and CO_2 optimization design results. The first one is the yield stress (f_{yk}) obtained for the best individual. It is observed that cost optimization results from this variable 275 MPa while CO_2 optimization gets 460 MPa. This difference is due to the difference in structural steel's cost and emission values. As shown in Table 1 as the cost increase, as the value of the yield stress increases, the value is the same for emissions for all yield stress values. Thus,

Cost minimization results for 30 executions of Random0.5, Random0.3, and discrete hybrid SCA algorithms.

Run	Random0.5			Random0.3			Hybrid SCA	Hybrid SCA		
	Cost (€)	CO ₂ (kg)	Time (s)	Cost (€)	CO ₂ (kg)	Time (s)	Cost (€)	CO ₂ (kg)	Time (s)	
1	3841685.5	9 423 182.3	7545.1	3854631.0	9 441 992.7	7434.5	3 830 092.8	9390104.1	7835.5	
2	3838056.5	9 417 710.5	8121.4	3841685.5	9423182.3	7892.6	3864886.9	9 480 536.6	7945.0	
3	3856001.6	9 455 1 45.0	6978.9	3868347.8	9 487 298.0	7112.7	3826395.0	9388407.3	7873.4	
4	4004603.5	9837622.5	7984.7	4041117.6	9915536.1	8001.2	3825919.0	9385589.0	7929.9	
5	3837584.6	9 406 572.5	6921.5	3863494.3	9 467 939.5	6893.2	3823801.1	9385004.6	7916.1	
6	3920211.2	9618810.5	8021.3	4009757.4	9837067.3	8021.3	3835442.1	9391386.1	7911.4	
7	3863494.3	9 467 939.5	7214.8	3835377.4	9395269.5	7324.6	3826324.6	9389542.7	7920.3	
8	4004603.5	9837622.5	7498.1	3973917.2	9747159.4	7568.3	3826206.4	9385730.7	7935.5	
9	3920211.2	9618810.5	8210.4	3844805.5	9422679.4	7901.4	3830234.3	9387716.3	7858.2	
10	3867325.2	9 485 202.2	7645.7	3938023.8	9657116.7	7923.5	3825188.7	9385235.2	7931.7	
11	3920211.2	9618810.5	7645.2	3912499.4	9593267.2	7234.8	3828878.5	9387047.9	7748.9	
12	3847797.6	9432071.6	8024.1	3840298.2	9419023.8	8024.1	3831864.4	9388519.9	7719.6	
13	3844078.0	9 432 582.0	7643.7	3847990.2	9432380.4	7701.4	3823462.5	9384378.1	7637.7	
14	3848079.2	9419256.1	7891.4	3844078.0	9432582.0	7903.2	3828178.8	9386856.2	7819.4	
15	3927551.4	9631163.6	7798.4	3920211.2	9618810.5	7923.2	3826847.5	9386123.4	7933.9	
16	3853756.2	9 458 527.3	7234.1	3847713.1	9 431 886.6	8001.5	3824311.6	9384796.6	7687.4	
17	3854631.0	9 441 992.7	8102.3	3851331.6	9451618.9	8114.7	3822723.1	9384013.6	6165.3	
18	4004603.5	9837622.5	7743.6	3829666.1	9398360.6	6902.6	3824024.1	9384655.0	7767.6	
19	3844695.3	9 425 683.0	7893.9	3844407.2	9425168.7	7745.2	3824115.0	9384852.9	7918.0	
20	3840156.4	9 402 992.6	7745.1	3853756.2	9458527.3	7801.4	3829979.1	9387820.3	7891.1	
21	3858728.1	9 455 868.2	7874.5	3846266.3	9424806.5	7931.6	3823245.0	9384270.9	7870.4	
22	3846266.3	9 424 806.5	7534.2	3856001.6	9455145.0	7345.2	3828654.6	9388464.0	7945.4	
23	3868347.8	9 487 298.0	7654.9	3858728.1	9455868.2	7791.5	3827333.5	9386286.3	7895.7	
24	3853062.4	9 444 842.4	7943.4	3930520.1	9638238.9	8002.3	3824394.8	9384837.7	7876.2	
25	4004603.5	9 481 380.6	7653.2	3866161.5	9 481 380.6	7754.8	3830913.2	9388051.0	7855.7	
26	3920211.2	9618810.5	7896.7	3853062.4	9444842.4	7931.9	3829366.5	9387824.7	7668.7	
27	3844407.2	9 425 168.7	7745.7	3867165.6	9474659.0	7742.5	3833463.0	9391767.1	7731.3	
28	3847873.6	9 432 179.5	7653.3	3847714.8	9447150.9	7509.8	3824394.8	9384837.7	7845.4	
29	3851331.6	9 451 618.9	7694.9	3844695.3	9425683.0	7654.7	3823562.7	9384427.5	7696.0	
30	3867165.6	9 474 659.0	7893.5	3938023.8	9657116.7	8032.4	3830124.4	9 388 127.9	7947.6	
Average	3 883 377.8	9512198.4	7713.6	3 879 048.3	9512058.6	7704.1	3828477.6	9 389 907.0	7789.3	
Max	4004603.5	9837622.5	8210.4	4041117.6	9915536.1	8114.7	3864886.9	9 480 536.6	7947.6	
Min	3837584.6	9 402 992.6	6921.5	3829666.1	9 395 269.5	6893.2	3822723.1	9384013.6	6165.3	
Std	55639.3	130762.0	312.2	54 164.3	134 417.5	340.2	7622.2	17 251.2	320.7	
Wilcoxon p-value	4.1e-4		1.7e-4							



Fig. 4. Cost boxplots for SA, discrete transfer SCA, discrete hybrid SCA, and discrete hybrid CS Algorithms.

the CO_2 optimization takes a higher yield stress value because the strength capacity of these steels is higher and is capable of resisting more stresses with less material. Regarding cells dimensions it can be seen that CO_2 best design gets higher values for both upper (h_{c_1}) an lower (h_{c_1}) cells heights. In the case of the cost objective function, the best individual gives a null value to the height of the upper cell. The objective of these cells is to reduce the distance between stiffened zones to reduce the web plate's reduction. For cost optimization, the upper cell does not accomplish this function or is almost not enough to be relevant for the design, while for CO_2 emissions objective function, it allows a better cross-section behavior and takes a positive value.

Regarding bottom flange stiffeners $(n_{s_{f_2}})$, both optimization objectives remove this elements for the optimium design. This is because, in negative bending moments, sections exist a concrete slab in the bottom flanges that do not allow the instability of the bottom flange plate, while in positive bending moment sections, this plate is in tension and, consequently, cannot buckle, and these elements are not necessary. Regarding the other variables, both optimization designs give a similar value being the higher difference in the beam height value (h_b) , where CO_2 optimization takes a lower value due to the increase in the yield stress (f_{yk}) that allow reducing the Section by increasing the structural steel resistance.

Cost minimization comparison for 30 executions of SA, discrete transfer function SCA and CS, discrete hybrid SCA, and CS algorithms. Time is measured in seconds.

Run	SA			Transfer SCA		Transfer CS		Hybrid SCA			Hybrid CS				
	Cost (€)	CO_2 (kg)	Time	Cost (€)	CO_2 (kg)	Time	Cost (€)	CO_2 (kg)	Time	Cost (€)	CO_2 (kg)	Time	Cost (€)	CO_2 (kg)	Time
1	3829112	9 393 007	9196	3854631	9 441 992	7497	3853274	9447811	7621	3830092	9390104	7835	3825644	9 385 453	7975
2	3845663	9442138	7589	3841685	9 423 182	7822	3853926	9 449 454	7741	3864886	9 480 536	7945	3825115	9 385 192	7976
3	3829827	9 390 569	9687	3868347	9 487 298	7889	3861618	9 468 696	7812	3826395	9388407	7873	3825644	9385453	7891
4	3834439	9395041	9719	3837467	9411814	7635	3837015	9413229	7635	3825919	9 385 589	7929	3830529	9387861	7959
5	3836720	9 393 995	9430	3863494	9 467 939	7786	3859823	9464319	7653	3823801	9385004	7916	3822875	9 384 095	7930
6	3832832	9 394 394	9198	3838032	9396760	7795	3 933 952	9636170	7563	3835442	9 391 386	7911	3827681	9 386 457	7983
7	3837598	9398873	9291	3835377	9 395 269	7317	3844299	9 425 351	7752	3826324	9389542	7920	3824141	9384712	8008
8	3841417	9 408 629	9271	3839077	9 400 419	7876	3832605	9397118	7976	3826206	9385730	7935	3827522	9386379	7971
9	3826259	9 391 263	9225	3844805	9 422 679	7832	3853274	9447811	7698	3830234	9387716	7858	3827541	9 386 388	7949
10	3837246	9 398 956	9691	3867325	9 485 202	7880	3857615	9 458 840	8043	3825188	9 385 235	7931	3825756	9 387 883	8055
11	3838964	9 399 136	9507	3833501	9406118	7556	3829202	9389102	7467	3828878	9387047	7748	3824519	9 384 899	8267
12	3844258	9 420 045	9668	3840298	9419023	7903	3861618	9 468 696	7894	3831864	9388519	7719	3831847	9388511	8292
13	3840202	9 408 438	9557	3844078	9432582	7509	3854516	9 450 954	7735	3823462	9384378	7637	3827980	9386681	8291
14	4701903	11582022	9856	3848079	9419256	7789	3836478	9 406 458	7642	3828178	9386856	7819	3823891	9 384 589	8267
15	4004603	9837622	9956	3920211	9618810	7820	3853274	9447811	7756	3826847	9386123	7933	3825444	9 385 765	8148
16	3837030	9407814	9504	3840156	9 402 992	7886	3860073	9 450 935	7985	3824311	9384796	7687	3823063	9384870	8210
17	3838077	9 398 394	9705	3851331	9451618	7740	3851195	9 427 987	7463	3822723	9384013	6165	3832782	9 401 328	8308
18	3826142	9389610	9793	3829666	9 398 360	7905	3848626	9422617	7683	3824024	9384655	7767	3828246	9386736	8370
19	3836306	9 393 541	9326	3844407	9 425 168	7902	3839130	9 400 681	7843	3824115	9384852	7918	3831724	9 388 450	8249
20	3829965	9 397 333	9912	3853756	9 458 527	7736	3839701	9402112	7722	3829979	9 387 820	7891	3824459	9 384 869	8236
21	3834063	9 395 196	9590	3846266	9 424 806	7921	3851195	9 427 987	7463	3823245	9384270	7870	3830466	9 387 831	7897
22	3838868	9 397 515	9535	3856001	9455145	7502	3879874	9 500 752	7985	3828654	9388464	7945	3825593	9 385 428	7645
23	3840493	9410516	9238	3858728	9 455 868	7583	3861537	9 457 936	7583	3827333	9 386 286	7895	3826446	9 385 925	7912
24	3836563	9 399 930	9617	3839779	9410778	7903	3 881 525	9 505 995	7793	3824394	9 384 837	7876	3827796	9386514	7914
25	3833027	9 394 227	9494	3866161	9 481 380	7729	3849452	9 428 558	7642	3830913	9 388 051	7855	3822766	9 384 035	7896
26	3834233	9 397 503	9412	3853062	9444842	7790	3841782	9 409 898	7856	3829366	9 387 824	7668	3822723	9384013	7024
27	3845712	9 417 868	9565	3867165	9 474 659	7781	3854384	9 440 750	7843	3833463	9 391 767	7731	3822723	9384013	5218
28	3832969	9 403 292	9984	3847714	9 447 150	7552	3858984	9 467 252	7748	3824394	9 384 837	7845	3825907	9 385 583	7943
29	3829559	9 389 435	8800	3844695	9 425 683	7660	3 851 331	9 448 449	7654	3823562	9 384 427	7696	3823593	9 384 442	7923
30	3834992	9 398 075	9775	3838056	9417710	7891	3 841 344	9 423 805	7962	3830124	9 388 127	7947	3830083	9 388 051	7914
Average	3 870 301	9 487 479	9470	3 850 445	9 440 101	7746	3854421	9446251	7740	3828477	9 389 907	7789	3 826 483	9386414	7921
Max	4701903	11582022	9984	3920211	9618810	7921	3 933 952	9636170	8043	3864886	9 480 536	7947	3832782	9 401 328	8370
Min	3826142	9 389 435	7589	3829666	9 395 269	7317	3829202	9389102	7463	3822723	9384013	6165	3822723	9384013	5218
Std	160135	403 661	443	17 047	43 542	159	19179	45 846	158	7 622	17 251	320	2954	3 1 3 7	570
Wilcoxon p-value	3.6e-4			1.4e-4											



Fig. 5. Emissions boxplots for SA, discrete transfer SCA, discrete transfer CS, discrete hybrid SCA, and discrete hybrid CS Algorithms.

5. Conclusions

The present work proposes a discrete hybrid KMDA method that uses the k-means unsupervised learning technique in conjunction with SCA and SC to solve a discrete optimization issue. It was specifically applied in this work to the design of a Steel–Concrete Composite Bridge. Two experiments were designed to demonstrate the superiority of KMDA in bridge optimization. The first experiment aims to compare the proposed approach to a baseline algorithm in which the discretization stage is executed by a random operator with fixed transition probabilities. *Random*0.3 and *Random*0.5. The results showed that the incorporation of the k-means operator allows obtaining better results, as well as the reduction of the dispersion of the objective values. In the comparison, it was obtained for cost optimization that Hybrid SCA reduced the value by 1.4% compared to *Random*0.5 and by 1.3% compared to *Random*0.3. In the comparison of the emissions of CO_2 , considering cost optimization, the hybrid SCA managed to reduce emissions by 1.3% in both cases. The Wilcoxon statistical test showed that the difference is significant. Regarding the execution times, these were similar in the different algorithms.

In the second experiment, the result of the proposed hybrid technique was compared with another frequently used method to discretize

CO2 minimization comparison for 30 executions of the discrete transfer function and discrete hybrid SCA and CS algorithms.

-	*						0				
Run	SA		Transfer SCA		Transfer CS	Transfer CS		Hybrid SCA		Hybrid CS	
	Cost (€)	CO ₂ (kg)	Cost (€)	CO ₂ (kg)	Cost (€)	CO ₂ (kg)	Cost (€)	CO ₂ (kg)	Cost (€)	CO ₂ (kg)	
1	4103199.1	9394472.7	3826062.4	9388245.3	4 531 487.4	10115112.3	4 420 699.5	9384170.2	4 421 107.9	9384371.6	
2	4104830.5	9393422.6	4 107 363.5	9 398 200	4931000.7	10230565.0	3828339.5	9386782.2	4091626.2	9384500.2	
3	4095750.7	9386615.5	4 106 480.8	9419624.4	4789317.2	10033694.7	4092720.6	9385866.9	4 093 543.7	9385445.5	
4	4101735.1	9390010.9	3830420.8	9390027.3	4607448.4	9710063.3	4092681.4	9385020.4	4 421 714.6	9384676.8	
5	4 431 949.9	9390386.3	4 423 829.8	9388224.6	4724373.8	9870644.4	4 428 155.9	9 387 845.9	3823916.4	9384601.8	
6	4 428 021.6	9387786.7	4 104 429.3	9413019.9	4735134.9	9912923.2	3829500.6	9 387 354.6	3823680	9384485.3	
7	4 428 243.3	9 393 282.6	4 444 861.3	9 427 586	4730550.6	9924267.8	4 427 399.4	9 387 473	4091769.9	9384571.1	
8	4 424 257.7	9387914.4	3845183.8	9417923.6	4503658.7	9765664.9	4 093 430.2	9 385 389.5	3823245	9384270.9	
9	4099351.4	9395896.2	3828004.3	9391991.1	4212280.9	10052411.1	3831646.9	9388412.7	4 421 527.7	9384578.5	
10	3836602.7	9 407 896.6	4 434 043.8	9399596.9	4666593.6	9725656.3	3827295.3	9386273.6	4 093 543.7	9385445.5	
11	4 436 583.5	9399830.4	4 440 365	9 405 285.5	4841631.0	10686873.0	4 091 126.9	9384254.1	3824016.6	9384651.2	
12	4099070.8	9 391 395.7	4098731.9	9398154.5	5058456.2	10 525 430.7	3824275.7	9384778.9	3823245	9384270.9	
13	3837692.9	9394543.3	4 097 483.5	9395141.9	4 257 869.8	9838989.8	4 093 666.6	9385506.1	3826336.9	9385795.0	
14	4098859.5	9394851.7	4 447 519.4	9 406 304.8	4957796.6	10944461.4	4 091 859.4	9385667.9	3827656.8	9386445.7	
15	4092562.3	9385573.4	4149564.8	9 501 199.2	4721028.2	9992277.7	3828232.5	9386739.1	4 426 817	9387185.9	
16	4 437 303.8	9398323.1	4111137.6	9411014.2	4925090.5	10312531.2	4091796.4	9384584.1	4096921.1	9387110.4	
17	4100494.5	9392570.7	4103984.7	9 401 026.2	4977891.6	10121176.4	3829720	9 387 462.8	4101662	9389447.4	
18	4 424 307.7	9386325.9	3852755.9	9455679.3	4 552 468.0	10031915.7	4 090 883.3	9384585.2	3824016.6	9384651.2	
19	4102823.5	9396581.4	3 831 846.9	9398755	4611778.6	10355530.8	4 100 425.2	9388837.8	4 093 460.5	9385404.4	
20	4 428 702.7	9390314.8	3853687	9444022.8	4928246.3	10324582.5	3823782.1	9 384 535.6	4 423 239.1	9385422.2	
21	4 430 019.3	9392768.3	3834232.5	9393079.5	4894711.7	10129787.8	3825979.5	9385618.9	3825050.6	9385167.1	
22	4102389.5	9 391 525.7	3843360.9	9 430 497.2	4878828.2	10058610.4	4 096 206.3	9 386 758	4568165.1	9384308.4	
23	3829423.6	9 390 490.5	4 132 163.3	9459204.2	4891768.4	10 229 330.1	4 094 423	9385878.9	3823948.5	9384617.7	
24	4106712.4	9395756.6	4 111 394.3	9413642.1	4 598 949.9	10 406 844.4	3826340.7	9 385 796.9	4092556.6	9384958.9	
25	3833087.7	9391660.1	3835567.5	9 409 985.7	4763740.6	9977672.0	4 095 292.9	9 386 307.8	3826660.3	9385954.4	
26	3823206.8	9384338.0	4 109 800.5	9 405 586.3	4614532.1	9738456.8	3828734.7	9 386 977.1	3823948.5	9384617.7	
27	4 428 242.5	9392728.7	4 442 164.1	9 424 594.9	5249949.1	10943039.5	3823782.1	9 384 535.6	3832507.4	9388836.8	
28	3832154.7	9388663.3	4108189.4	9 406 482.7	4371744.8	9740572.8	4 100 432.8	9388841.5	3825740.1	9 388 369.9	
29	4 428 372.5	9397013.8	4 445 608.5	9410269.7	4872910.1	10028070.8	3828738.5	9 386 978.9	4 090 843.3	9384114.8	
30	4096391.3	9387611.7	3837284.5	9 401 492.1	4576118.0	9997514.0	3832291.8	9388730.6	4092556.6	9384958.9	
Average	4 167 411	9392617.2	4087917.4	9413528.6	4732578.5	10124155.7	4 002 995.3	9386265.5	4039167.5	9385469.5	
Max	4 437 303	9 407 896.6	4 447 519.4	9 501 199.2	5249949.1	10944461.4	4 428 155.9	9388841.5	4568165.1	9389447.4	
Min	3823206	9384338.0	3826062.4	9388224.6	4212280.9	9710063.3	3823782.1	9384170.2	3823245.0	9384114.8	
Std	226 692	4878	232 227.7	24665.3	231 256.6	328 416.3	192 413.8	1423.3	241 158.4	1414.8.9	
Wilcoxon		2.7e-4		1.2e-4		2.7e-6					
p-value											

algorithms, transfer functions. Additionally, a version of SA adapted to solve civil engineering optimization problems was included. In the case of transfer functions, the solution only uses its information to discretize, unlike k-means which first analyzes the group of solutions and then discretizes. From the results of the experiments, it is once again observed that the proposed hybrid technique is superior in the results obtained. Particularly in the case of cost optimization, it is observed that Hybrid SCA reduced costs on average compared to SA by 1.1% and compared to transfer SCA by 0.57%. In the case of Hybrid CS, the result was very similar to that of Hybrid SCA, the latter being 0.05% higher on average. In the case of CO_2 optimization, we again observed that the hybrid algorithms were superior to those using transfer function and SA. Hybrid CS outperformed Transfer CS by 7.8%, and up to 0.07% compared to SA. In the case of Hybrid CSA, it outperforms Transfer CSA by 0.3% and SA by 0.07%.

Finally, an analysis of the optimum obtained was conducted, observing that outstanding results are also obtained for CO_2 emissions when costs are optimized. However, the reciprocal, that is, when emissions are optimized, does not imply that costs are optimized. This was related to the fact that different steel grades have different costs but generate the same emissions.

As a new line of research, we identified that optimization consumes a significant amount of time, near to 8000 (s), with which developing algorithms that allow reducing optimization times allows exploring a more significant number of configurations and more complex situations. When an analysis of the execution times is carried out, we observe that the primary time is consumed to evaluate the constraints. It is hypothesized that by incorporating a deep learning model that does not have essential execution times, the constraints could be modeled and replaced, thereby improving the times used in optimization. Along the same lines, to try to reduce the number of calculations, another idea to explore is to use upper bound strategies (UBS) [42] to reduce the total number of structural analyzes in design optimization.

CRediT authorship contribution statement

D. Martínez-Muñoz: Conceptualization, Software, Investigation, Data curation, Writing – original draft, Writing – review & editing, Visualization. J. García: Conceptualization, Methodology, Validation, Formal analysis, Investigation, Writing – original draft, Writing – review & editing, Visualization, Project administration. J.V. Martí: Validation, Writing – review & editing, Supervision. V. Yepes: Validation, Resources, Writing – review & editing, Supervision, Project administration, Funding acquisition.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Design variables results for best, mean, minimum, maximum, and standard deviation values.

Variables	Unit	Cost op	otimizatio	n		CO ₂ optimization				
		Best	Mean	Min	Max	Best	Mean	Min	Max	
b	m	7	7	7	7	7	7	7	7	
$alpha_w$	deg	55	63	45	87	71	62.3	45	90	
h_s	mm	200	200	200	200	200	200	200	200	
h_b	cm	298	304	250	381	286	311	250	388	
h_{fb}	mm	410	438	400	610	620	480	400	680	
t_{f1}	mm	25	27	25	57	25	26	25	39	
b_{f1}	mm	300	309	300	480	300	300	300	300	
h_{c_1}	mm	0	264	0	960	9	333	0	830	
t _{c1}	mm	16	16	16	17	16	16	16	16	
t_w	mm	16	16	16	16	16	16	16	16	
h_{c_2}	mm	33	38.8	00	90	41	32.8	0	86	
t _{c2}	mm	18	19	16	25	18	19	16	25	
b_{c_2}	mm	300	302	300	370	300	300	300	300	
t_{f_2}	mm	25	25	25	29	25	25	25	25	
h_{s_2}	mm	150	150	150	150	150	150	150	150	
$\phi_{\it base}$	mm	6	6	6	6	6	6	6	6	
ϕ_{r_1}	mm	6	6	6	6	6	6	6	6	
ϕ_{r_2}	mm	6	6	6	6	6	6	6	6	
n_{r_1}	u	200	278.4	200	436	200	282	200	425	
n _{r2}	u	200	280	200	403	228	270.8	200	418	
s_{f_2}	mm	300	322.1	200	550	200	328	200	550	
$n_{s_{f_2}}$	u	0	0	0	0	0	0	0	0	
sw.	mm	450	327.5	200	600	200	347.6	200	600	
s _t	mm	240	306	200	600	200	322.6	200	600	
d _{st}	m	3.3	2.407	1	4.2	2.52	1.2	1	5	
d_{sd}	cm	6	6.5	4.1	9.7	4.8	6.3	4	9.9	
b_{fb}	mm	1000	450	200	1000	200	430	200	1000	
$t_{f_{fb}}$	mm	33	29	25	35	29	29	25	34	
$t_{w_{fb}}$	mm	27	28	25	35	26	29	25	35	
f_{ck}	MPa	25	25	25	25	25	25	25	25	
f_{yk}	MPa	275	275	275	275	460	328	275	460	
f_{sk}	Мра	500	500	500	500	500	500	500	500	
h _{sc}	mm	100	100	100	100	100	100	100	100	
ϕ_{sc}	mm	16	17	16	22	16	16.3	16	22	

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