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Additional Information

Construction of RC building structures: ICITECH's experience during the last 30 years

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Abstract (150 – 200 words)

This paper contains a summary of the experience obtained by ICITECH's researchers at the *Universitat Politècnica de València* in the last thirty years of investigating reinforced concrete (RC) building structures under construction. During this period ambitious experimental campaigns and advanced computational simulations have been carried out, and new analytical methods have been formulated to assess slab-shore load transmissions in buildings under construction. From all these campaigns the following main conclusions can be derived: 1) the importance of considering construction processes when planning building projects; 2) the use of analytical methods to evaluate construction processes adapted to the current requirements of efficiency and sustainability; and 3) the need to improve the robustness of temporary shoring or propping structures. Improving the construction sector necessarily involves the implementation of the above measures in buildings under construction and the use of new monitoring and inspection technologies for the construction processes applied.

Keywords chosen from ICE Publishing list

Buildings, Structures & Design; Concrete Structures; Temporary Works.

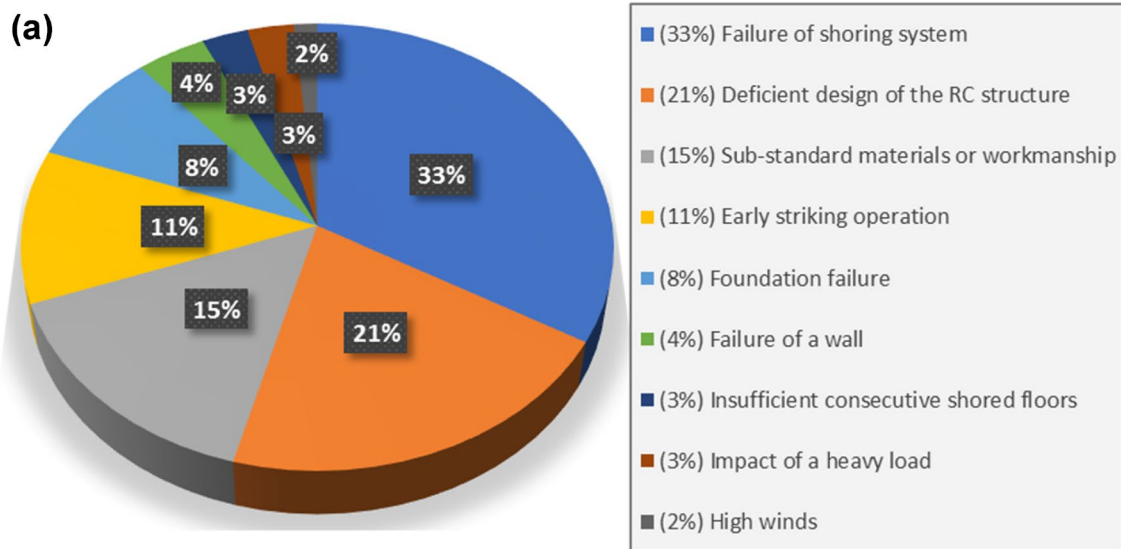
1 **1. Introduction**

2 The construction of RC building structures and the different processes used to construct them
3 have been widely studied since the mid 20th century (Buitrago *et al.*, 2018b). The method of
4 shoring or propping successive storeys is usually by shoring the last two, three or four floors
5 (Grundy & Kabaila, 1963; Adam *et al.*, 2017). This method allows new slabs to be poured while
6 the newly created loads are shared out between a number of lower floors, which during the
7 construction process may have to support higher loads than those they were designed to resist
8 in their service life, at a time when the lower floors concrete's mechanical characteristics are still
9 below their design level.

10 From a safety point of view, the fact of receiving high loads combined with the early age of the
11 concrete on the lower floors creates a high-risk situation that is usually greater than any likely to
12 occur in the building's service life and has been the cause of a significant number of historical
13 failures and collapses (Feld, 1974; Hadipriono & Wang, 1987; Kaminetzky & Stivaros, 1994; Peng
14 *et al.*, 1996; Epaarachchi, Stewart & Rosowsky, 2002; Yates & Lockley, 2002; Epaarachchi &
15 Stewart, 2004; Fang *et al.*, 2004; Uzoegbo & Harli, 2010; Yuan & Jin, 2011; Zhang, Rasmussen
16 & Ellingwood, 2012; Kaminetzky, 1976; Buitrago *et al.*, 2018c; Schellhammer, Delatte & Bosela,
17 2013). This document considers failures as a malfunction of the performance of the structure (e.g.
18 Serviceability Limit States; SLS) whereas collapses are limited to those cases of major failures
19 resulting in debris (e.g. exceeding Ultimate Limit States; ULS). Figure 1(a) shows the possible
20 reasons for structural failures during construction. It can be seen that in first place, with a
21 frequency of 33%, the most common cause of failure is collapse of the shoring or propping system
22 (Buitrago *et al.*, 2018c), which has been known to lead to the collapse of the entire structure, as
23 occurred in the Skyline Plaza in Virginia (Schellhammer, Delatte & Bosela, 2013), or failure in the
24 service and durability conditions with excessive deflections and cracking, which can affect the
25 short- and long-term behaviour of the structure (Adam *et al.*, 2017). Figure 1(b) gives an example
26 of a case in which the shores were buckled but without causing the structure to collapse, while
27 Figure 1(c) shows a slab with excessive deflections and cracking.

28 The aim of the line of investigation, started by ICITECH's researchers 30 years ago and summed
29 up in this paper, is to improve the safety of RC building structures under construction and involves
30 diverse topics designed to cover the construction industry's current needs as regards shoring and

31 formwork, as well as other questions that so far have not been resolved by the scientific
32 community. The research has opened up new areas that had not been studied previously, such
33 as the particular type and widely used construction process known as partial striking or clearing,
34 studies of the robustness of temporary shoring structures, and establishing mitigation measures
35 against the risk of progressive collapse of buildings under construction. Throughout the years the
36 research has been accompanied by in-depth experimental campaigns and computational
37 simulations that finally formed the knowledge base on which the analytical methods and simplified
38 construction process calculations (described in the following sections) were developed to facilitate
39 the work of practitioners and improve the safety of buildings under construction.



40
41
42

Figure 1. Failures

43 2. Tests and computational modelling

44 Figure 2 shows a series of photos of some of the most important tests carried out, while Figure 3
45 gives the associated computational modelling studies. In the beginning, towards the end of the
46 1980s, a study was made of the evolution of the mechanical properties of different types of early-
47 age concrete in a variety of environments in order to determine the structural response of buildings
48 in different construction phases. Then, in the early nineties, the shores used in a clearing or partial
49 striking system in actual construction sites were monitored (Moragues, Catalá & Pellicer, 1994)
50 to estimate the real transmission of loads between slabs and shores in order to compare the
51 results with those obtained by computational simulations (Moragues, Catalá & Pellicer, 1996) and
52 simplified calculation methods such as that by Grundy & Kabaila (1963).

53 After 2004 the work on this line of research intensified, and from 2004 to 2008 a full-scale RC
54 building structure was constructed for purely experimental purposes. This building had 3 single-
55 bay floors with cantilevers on two sides. The main purpose of the experimental study was to
56 analyse the transmission of loads between slabs and shores in a clearing or partial striking system
57 (Alvarado *et al.*, 2009). Figure 2 contains a photo of the building during the pouring of the third
58 floor, which was totally shored, while the second had been cleared. This study also served to
59 validate a finite element model (see Figure 3) and extend the analysis to other types of
60 construction processes (Alvarado *et al.*, 2010).

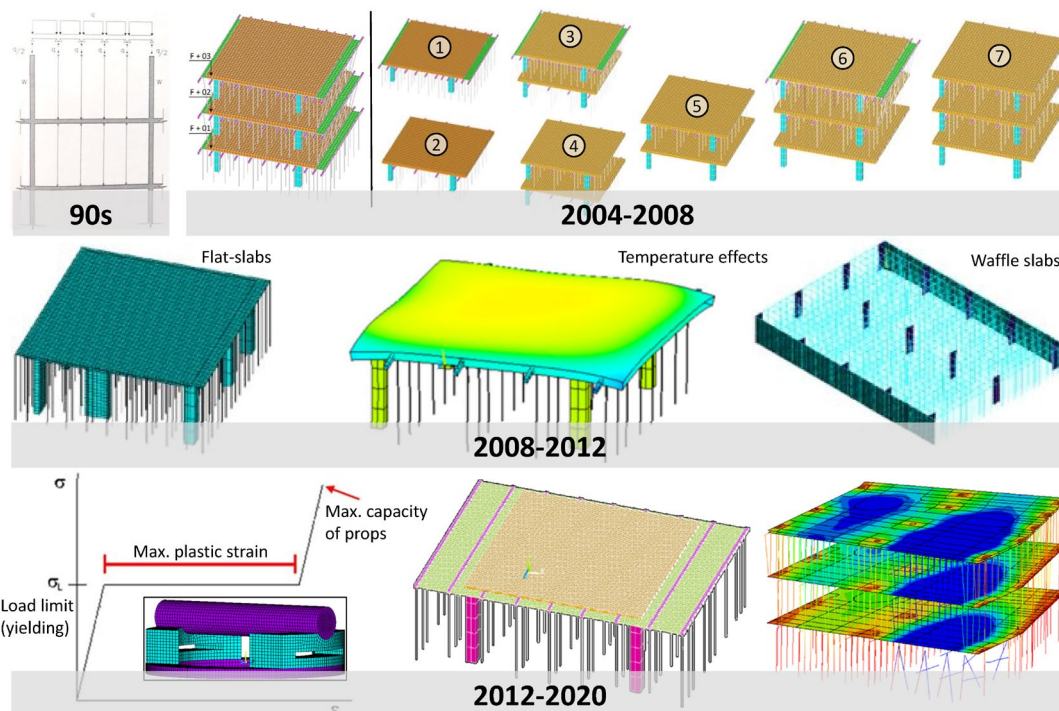
61 In the next stage, between 2008 and 2012, a variety of real buildings under construction with flat-
62 slabs, waffle slabs or girderless hollow floor slabs using clearing or partial striking were monitored
63 (Gasch *et al.*, 2013, 2015) and the effects of temperature were analysed in uniform increments or
64 in the form of a gradient on the distribution of loads between slabs and shores (Gasch, Alvarado
65 & Calderón, 2012).

66 In the final period, from 2012 to 2018, work was done on studying the robustness of temporary
67 shoring structures and mitigating the risks of the collapse of the entire shoring system or even of
68 the entire building (Buitrago, Sagaseta & Adam, 2018). During this time the new load-limiter (LL;
69 see Fig. 2) device was developed (Buitrago *et al.*, 2015, 2018a) and validated in an application to
70 a full-scale RC building test (Buitrago *et al.*, 2021). The device was later patented (Calderón *et al.*,
71 2017) and put on the market (Encofrados J. Alsina S.A., 2020) and its effectiveness in
72 mitigating the risks of progressive shoring system collapse was confirmed by computational

73 simulations (Buitrago, Sagaseta & Adam, 2020). The load limiter works as a structural fuse to
 74 control and limit the load a shore/prop can bear. To limit the load, the LL activates a plastic
 75 mechanism with the formation of three hinges at a design limit load, so permitting: (i) the
 76 shore/prop to have small vertical deflections: (ii) the limitation of the load of this shore-LL unit and
 77 (iii) a transfer of the excessive loads to the neighbouring shores/props via the slabs.



78 **Figure 2. Tests.**
 79



80 **Figure 3. Computational modelling.**
 81

82 3. Analytical methods

83 Analytical methods have traditionally been used to make the calculation of complex phenomena
84 easier, especially those with simplified procedures. This is also the case of the construction
85 procedures based on shoring a number of successive floors. Some of the most frequently used
86 methods are those by Grundy & Kabaila (1963), Duan & Chen (1995) and Fang et al. (2001), who
87 simplified all the construction stages into a one-dimensional model of springs arranged in a series
88 to represent the behaviour of individual bays (see Figure 4). However, these methods left a lot of
89 room for improvement and in most cases were not experimentally validated, or were not
90 developed to be applied to certain construction processes such as clearing or partial striking
91 (Adam *et al.*, 2017; Buitrago *et al.*, 2018b). In order to cover these needs, analytical calculation
92 methods were developed in the line of research that was begun more than 30 years ago to
93 estimate slab-shore load transmission and could be adapted to all the existing construction
94 processes. These new analytical methods are based on the whole range of knowledge generated
95 throughout a period of many years in the experimental and computational simulation fields. Figure
96 4 shows the sequence and briefly describes each of the analytical methods so far developed
97 within the framework of the present line of research.

98 Calderón, Alvarado & Adam (2011) first developed a new simplified method that significantly
99 improved on its predecessors by considering the actual boundary conditions of individual bays
100 with the help of the Equivalent Frame Method (EFM). In this way the computed mean slab
101 deformation was more realistic and provided better correlation against the experimental results.
102 This simplified method is now being used by formwork manufacturers (e.g. Encofrados J. Alsina
103 S.A. (2020)), is beginning to be recommended in building codes (e.g. Guideline for EHE-08
104 (2014)) and has been used to design optimal building processes (Buitrago *et al.*, 2016b).

105 Buitrago et al. (2016a) later proposed a modification to Calderón, Alvarado & Adam's method
106 (2011) to obtain the maximum load on shores, computed as the load on the shore placed in the
107 position of maximum slab deformation.

108 In the same year, Buitrago et al. (2016c) proposed a second modification to determine the load
109 on individual shores by simplified methods. Before developing this method, the 3D problem was
110 always oversimplified by using 1D analysis, whereas this new method considers the 3D effects.
111 This method was validated by the experimental results from different types of slabs.

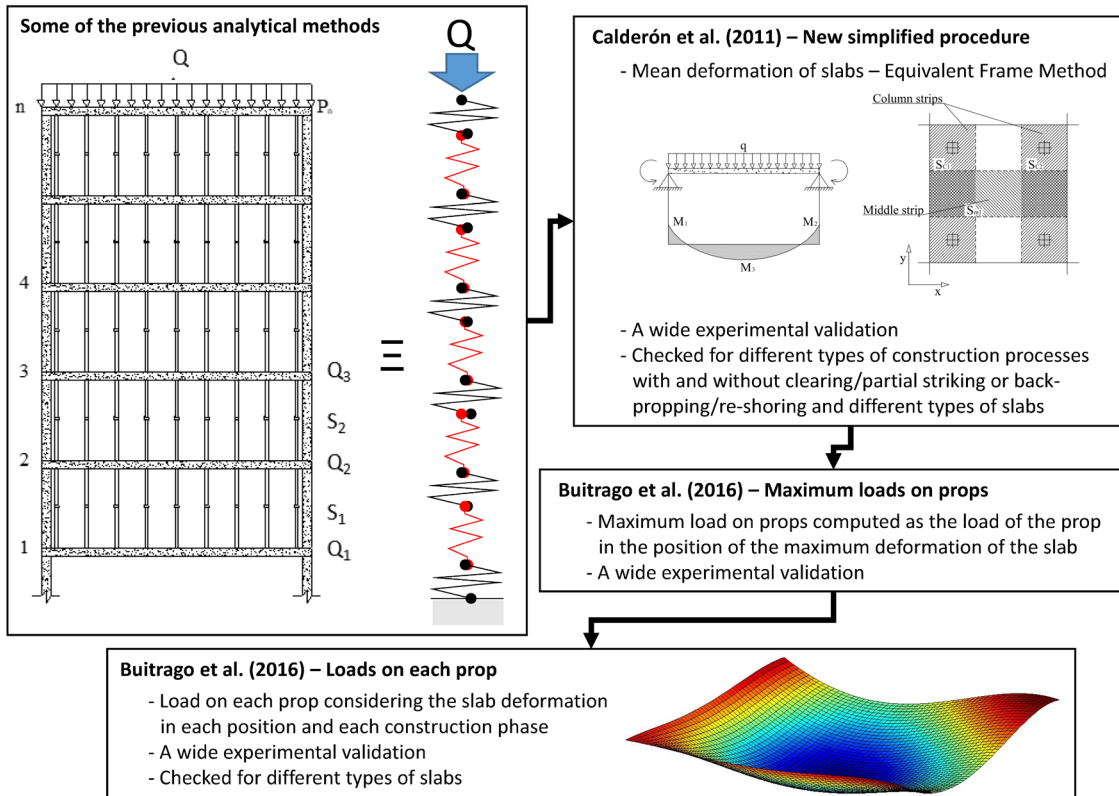


Figure 4. Analytical methods.

112

113

114

115 4. Conclusions

116 This paper sums up more than 30 years' experience in researching RC building structures in the

117 ICITECH laboratories at the *Universitat Politècnica de València*, including extensive experimental

118 campaigns together with the formulation of new analytical methods to evaluate load transmissions

119 between slabs and shores in buildings under construction. This has allowed us to cover the needs

120 of both the private sector and the scientific community and might also have produced an important

121 impact on the safety of structures and society as a whole. Some recent statistics (Buitrago *et al.*,

122 2018c) showed that an average of 12.4 collapses are reported every year, involving 2.6 floors

123 each. In addition, an average of 76 deaths and 133 injuries are reported every year. By using the

124 research outputs (new methods to estimate the transmission of loads and load limiters), a 47% of

125 the causes of these collapses could be avoided (see Figure 1), such as those referring to: (i)

126 failure of the shoring system, (ii) early striking operation, or (iii) insufficient consecutive shored

127 floors. Among the main conclusions reached are the importance of using analytical methods to

128 assess the latest construction processes and the need to improve the robustness of temporary

129 shoring structures.

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138 Pallarés.

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