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1	Bioactive glass/polymer composite scaffolds mimicking bone tissue		
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19			
20	Abstract		
21	The aim of this work was the preparation and characterization of scaffolds with mechanical and		
22	functional properties able to regenerate bone. Porous scaffolds made of chitosan/gelatin (POL)		
23	blends containing different amounts of a bioactive glass (CEL2), as inorganic material stimulating		

24 biomineralization, were fabricated by freeze-drying. Foams with different compositions

25 (CEL2/POL 0/100; 40/60; 70/30 wt %/wt) were prepared. Samples were crosslinked using genipin (GP) to improve mechanical strength and thermal stability. The scaffolds were characterized in 26 terms of their stability in water, chemical structure, morphology, bioactivity, and mechanical 27 28 behavior. Moreover, MG63 osteoblast-like cells and periosteal-derived stem cells were used to assess their biocompatibility. CEL2/POL samples showed interconnected pores having an average 29 diameter ranging from $179 \pm 5 \,\mu\text{m}$ for CEL2/POL 0/100 to $136 \pm 5 \,\mu\text{m}$ for CEL2/POL 70/30. GP-30 31 crosslinking and the increase of CEL2 amount stabilized the composites to water solution (shown by swelling tests). In addition, the SBF soaking experiment showed a good bioactivity of the 32 scaffold with 30 and 70 wt % CEL2. The compressive modulus increased by increasing CEL2 33 34 amount up to 2.1 ± 0.1 MPa for CEL2/POL 70/30. Dynamical mechanical analysis has evidenced that composite scaffolds at low frequencies showed an increase of storage and loss modulus with 35 increasing frequency; furthermore, a drop of E' and E" at 1 Hz was observed, and for higher 36 frequencies both moduli increased again. Cells displayed a good ability to interact with the different 37 tested scaffolds which did not modify cell metabolic activity at the analyzed points. MTT test 38 proved only a slight difference between the two cytotypes analyzed. © 2012 Wiley Periodicals, 39 Inc. J Biomed Mater Res Part A 100A:2654–2667, 2012. 40

41 Keywords: bioactive glass, chitosan, composite, gelatin, periosteal precursor cells

43 INTRODUCTION

44 The development of regenerative bone graft substitutes and bone tissue engineering scaffolds is an important area in the field of biomaterials and orthopedics, in a busy scenario for academia, 45 industry, and clinicians, especially since several commercial bone graft substitute products were 46 successfully applied in the clinics.¹ The strategy of designing scaffolds able to regenerate bone with 47 good mechanical and functional properties is a promising alternative to the use of allografts, 48 autografts, and metals. Scaffolds for bone repair should be based on biomaterials with adequate 49 50 properties such as biocompatibility, osteoconduction, bioactivity, osteoinduction, and biodegradation.² Bone regeneration usually employs three-dimensional (3D) porous materials. The 51 3D porous structure provides the necessary support for cells to proliferate and maintain their 52 differential function, and its architecture defines the ultimate shape of new bone.³ Moreover, 53 scaffolds for bone regeneration should mimic bone morphology, structure, and function. Bone is 54 composed of calcium phosphate (69-80 wt %, mainly hydroxyapatite), collagen (17-20 wt %), and 55 other components (water, proteins, etc.).⁴ For this reason, composites based on apatite crystals and 56 natural polymers have received increasing attention in bone tissue engineering applications due to 57 58 their ability to preserve the structural and biological phenotype of the damaged hard tissues in a biomimetic way.⁵ 3D sponge-like composite scaffolds based on bioactive glass and a genipin-59 60 crosslinked network of chitosan/gelatin were obtained by freeze-drying and investigated, having a similar composition to that of natural bone. Bioactive glasses are formed of different compositions 61 of SiO₂ with the addition of Na₂O, CaO, and P₂O₅; they react with physiological fluids and form 62 strong chemical bonds with the native tissue.^{6, 7} Bioactive glasses have successfully served as 63 skeletal substitutes and to fill bone defects in the oral cavity, largely because of their 64 osteoconductive properties.^{8,9} To retain these materials in a local defect site, bioactive glasses have 65 been incorporated into composites with synthetic polymers for improved delivery and 66

degradation.^{10, 11} While most osteoconductive biomaterials predominantly serve as a passive site 67 for cellular adhesion, proliferation, and differentiation, recent reports have demonstrated that 68 bioactive glasses may play a more active role in directing cellular behavior.^{12, 13} Bioglass® 45S5 69 has exhibited the potential to support the growth of osteoblasts and their precursors in vitro and to 70 favor osteoblast differentiation by stimulating the synthesis of phenotypic markers such as alkaline 71 phosphatase, Type I collagen, and osteocalcin.¹³⁻¹⁵ Moreover, chitosan, a naturally derived 72 polysaccharide, was used as organic component of the composite scaffold. It has gained much 73 attention as a biomaterial in diverse tissue engineering applications due to its low cost, large-scale 74 availability, anti-microbial activity, and biocompatibility.¹⁶ Chitosan films are highly brittle with a 75 76 strain at break of 40–50% in the wet state, while chitosan scaffolds with various shapes, pore sizes, and pore orientation can be obtained using freezing at a controlled-rate followed by 77 lyophilization.¹⁶ Furthermore, lysozyme-dependent chitosan degradation is influenced by the 78 degree of deacetylation (DD),¹⁷ local pH,¹⁸ and homogeneity of the source; lysozymal hydrolysis 79 is high in acidic conditions $(pH = 4.5 - 5.5)^{19}$ and decreases with increasing DD. The mechanical or 80 biological properties of chitosan can be significantly improved by blending with other polymers.²⁰ 81 Gelatin, a nonexpensive and commercially available biomaterial that has gained interest in 82 biomedical engineering, mainly because of its biodegradability, has been blended with chitosan to 83 improve the biological activity since (i) it contains Arg-Gly-Asp (RGD)-like sequences that 84 promote cell adhesion and migration, and (ii) it may form a polyelectrolyte complex with chitosan. 85 Gelatin-chitosan scaffold has been formed without or with cross-linkers such as glutaraldehyde²¹ 86 or enzymes,²² and tested for the regeneration of various tissues including skin^{,23} cartilage,²⁴ and 87 bone. 88

89 The scaffolds were prepared by freeze-drying process that is a conventional technique for the 90 fabrication of porous materials in which pore structure is controlled by the ice crystal growth. 91 Optimal pore diameters for 3D porous structures for bone repair are in the 100–400 µm range.²⁵

92 In this work, physical, chemical, and mechanical properties and the bioactivity of composite porous scaffold were investigated. Moreover, to assess their biocompatibility and possible use for the 93 regeneration of osteochondral tissues, the interaction with MG63 osteoblast-like cells and 94 periosteal progenitor cells (PCs) was evaluated. The latter present a cell-surface marker profile 95 similar to mesenchymal stem cells (MSCs) that are prominent candidate cells to repair complex 96 skeletal tissue defects.²⁶ MSCs, in fact, have a pronounced expansion capacity, undergo no 97 allogeneic rejection after transplantation, and show a high plasticity. PCs also have the potential to 98 differentiate into bone, cartilage, fat, and muscle²⁷ and recent studies evaluating migration, homing, 99 100 or engraftment potential of human PCs strengthened the hypothesis of periosteum as an interesting cell source for a bone tissue regenerative medicine.²⁸ 101

102

103 EXPERIMENTAL SECTION

104 Materials and methods

105 Materials

Type A gelatin (CAS No. G2500-100G) from porcine skin was supplied from Sigma, Italy.
Chitosan derived from crab shell with 76.5% deacetylation degree was purchased from Sigma,
Milan, Italy. The degree of deacetylation was determined by FT-IR spectroscopy using the
following formula:²⁹

110 %DD =100- [(A₁₃₂₀/ A₁₄₂₀)-0.3822]/0.03133 (1)

where A_{1320} is the absorbance at 1320 cm⁻¹, and A_{1420} is the absorbance at 1420 cm⁻¹. Bioactive glass (CEL2, particle size < 30 µm) was prepared according to a published procedure.³⁰ Genipin (GP) was purchased from Challenge Bioproducts, Taiwan. All solvents used were of analytical grade and used without further purification.

115 Methods

116 Preparation of crosslinked CEL2/POL scaffolds

A 3% (w/v) CH-G solution in 0.5M acetic acid (Sigma, Italy) was prepared under stirring for 12 h 117 at 40°C. CH and G were mixed at 1:2 weight ratio. CEL2 was added to the polymeric solution 118 (POL) to obtain CEL2/POL composites with various weight ratios between the components: 0/100; 119 40/60; 70/30 (wt %/wt.). The composites were coded as follows: CEL2/POL 0/100; 40/60; 70/30. 120 For crosslinked samples, GP was added to CEL2/POL solutions at defined weight percentage (2.5 121 wt %/wt with respect to the gelatin/chitosan amount). Each mixture was kept at 50°C under stirring 122 until a gel started to form. The gel was spread on Petri dishes (different sizes according to the 123 124 specific tests) and freeze-dried (Scanvac, CoolSafe) at -20°C for 24 h to obtain porous polymeric 125 matrices. After freeze-drying, samples were washed several times alternating 0.1N NaOH solution and demineralized water to remove GP residues and then samples were freeze-dried again. 126

Analysis of the porosity and the microstructure of scaffolds using micro-computed tomography

Scaffold architecture was analyzed using micro-computed tomography (μ -CT) with a desktop micro CT scanner (SkyScan 1072, Aartselaar, Belgium). No contrasting agent was added and the samples had a minimum size of 4 × 4 × 2 mm3. The scanner was set at a voltage of 40 kV and a current of 248 A, and the samples were scanned at 8.71 µm pixel resolutions by approximately 350 slices covering the sample height of 2.5 mm. For imaging, the sliced 2D tomographic raw images were reconstructed using CT Analyzer software, and the threshold levels of the grayscale images were equally adjusted for all the samples to allow the measurement of the volume of pores, providing the data for scaffold porosity. 3D modeling was also used to analyze the scaffold structure in a nondestructive manner, using imaging software.

138 Swelling tests

The extent of swelling was determined by a conventional gravimetric procedure as reported in literature.³¹ Weighed amounts of crosslinked CEL2/POL scaffolds (13 mm diameter and 5 mm height, as measured by means of a caliber) were kept in Phosphate Buffer Saline (PBS, Sigma, Italy) at 37°C (pH = 7.4). Swollen porous matrices were drawn at various time intervals (6, 12, and 24 h), dried superficially by gentle contact with a filter paper and weighed for the determination of wet weight as a function of the immersion time.

145 The swelling percentage was calculated as

146
$$%Sw = [(Ws_Wi)/Wi] 100$$
 (2)

147 where W_i and W_s are the sample weights before and after swelling, respectively. Each test was 148 repeated three times for each composition and results were expressed as average value \pm standard 149 deviation.

150 **Bioactivity evaluation**

To study the bioactivity of samples, porous scaffolds (13 mm diameter and 5 mm height, as measured by means of a caliber) were soaked in 5 mL of SBF prepared according to the protocol described by Kokubo et al.,³² at 37°C and pH 7.4 for various time intervals (2, 7, and 14 days, refresh of solution once every 2 days). SBF has a composition similar to human blood plasma and has been extensively used for in vitro bioactivity test. At the end of each experiment, the specimens were removed from SBF and then abundantly rinsed with deionized water and freeze-dried for morphological analysis and compositional examination.

158 Mechanical characterization

The compressive strength of the scaffolds was measured using a mechanical testing machine (MTS, 159 QTest/10). Test specimens were cylinder-shaped composite foams with 1.6 cm diameter and an 160 average height of around 1-1.2 cm measured by means of a caliber. Five porous samples were 161 evaluated for each composition. The samples were tested at room temperature. The cross-head 162 163 speed was set at $0.01 \text{ mm} \cdot \text{s} - 1$ and the load were applied until the specimen was compressed to approximately 60% of its original length. The compressive stress-strain curves were thus obtained 164 and the average compressive modulus with its standard deviation was calculated for each sample. 165 166 Precisely, the modulus was determined as the slope of the initial linear portion of the stress-strain curve.33 167

168 Furthermore, dynamic mechanical analysis (DMA) was carried out on the prepared scaffolds to 169 investigate their behavior under cyclic compressive load. The scaffolds were tested in a dry state; specifically, the samples underwent dynamic compressive solicitation (load condition: sinusoidally 170 171 varying load of 110 mN superimposed to a static load of 100 mN) at increasing frequencies varying 172 from 0.1 to 40 Hz (DMA7 Perkin-Elmer analyzer). This frequency range is typical for load-bearing conditions in physiological situations.^{34, 35} Storage (E') and loss (E'') modulus, that are the real and 173 174 imaginary component, respectively, of the complex modulus equation image (equation image is 175 the imaginary unit), were recorded against frequency.³⁶

177 *In vitro* culture

Human osteoblast-like cell line MG63 and human periosteal-derived precursor cells (PCs) were 178 179 used for in vitro tests. MG-63 human osteoblast-like cells (ATCC, Rockville, MD) were grown in a controlled atmosphere (5% CO2; T=37°C) in Dulbecco's Modified Eagle's Medium (DMEM, 180 Sigma-Aldrich, Milan, Italy) supplemented with 10% fetal bovine serum (FBS), 1% nonessential 181 amino acids 2.0 mM L-glutamine, and 1% penicillin-streptomycin (all from GIBCO, Invitrogen, 182 Milan, Italy). After thawing, cells were routinely split 1:10 every 3-4 days and used between the 183 184 third and fourth passages. PCs cells were isolated from periosteal tissue of subjects undergoing 185 surgery for orthopedic trauma, after the obtainment of their informed consent. Tissue was 186 aseptically dissected, washed three times in PBS, cut into small pieces $(2-3 \times 2-3 \text{ mm})$, and placed 187 into culture dish in Dulbecco's Modified Eagle Medium: Nutrient Mixture F-12 (DMEM/F12 188 GIBCO), supplemented with 10% FBS and 1% penicillin-streptomycin (100 U/mL). The cells 189 were then allowed to adhere in standard cell culture conditions in a controlled atmosphere (5% 190 CO2; $T = 37^{\circ}C$). The medium was changed twice a week and cells were used between third and 191 sixth passage of subculture. To assess PCs mesenchymal stem cells phenotype cells were 192 characterized by FACSCalibur flow cytometry system (Becton Dickinson, CA,USA), using antibodies against the following surface antigens: HLA-DR, CD34, CD105, CD14, CD19, and 193 194 CD45 (Diaclone, Besancon, France); CD73 and CD90 (StemCell Technologies, Inc. Vancouver, BC, and Canada).37 195

196 Cell seeding

Before seeding the freeze-dried CEL2/POL2 scaffolds were disinfected in 70% ethyl alcohol
solution (ETOH; Sigma-Aldrich, Milan, Italy) for 2 h, washed two times in sterile PBS (GIBCO)
for 30 min and sterilized under UV 15 min for each side. To improve cell adhesion, scaffolds were

then conditioned overnight in 10% serum added DMEM or DMEM/F12 at 5% CO2, 37°C. The medium was then discarded and scaffolds considered ready for seeding. Cells were detached using 0.25% trypsin in 1 mM ethylenediaminetetraacetic acid (EDTA, Sigma-Aldrich, Milan; Italy) and seeded at a density of 1×104 cell/cm3 by applying 50 µL of cell suspension on the samples placed in at 37°C for 30 min in a humified chamber, to avoid the slip down of cells. Then 1.5 mL of the appropriate culture media was added to cover the samples placed in Corning® ultra-low attachment multiwell plates. Cells were cultured for 14 and 21 days.

207 Histology

Cultured scaffolds were fixed in 4% paraformaldehyde in 0.1M phosphate buffer, pH 7.4, at 4°C for 20 min and washed three times with PBS and cut. Sections were taken from the peripheral and the central part of the scaffold, stained with 1 mg/mL 4', 6-diamidino-2-phenylindole (DAPI D9542-Sigma-Aldrich) to stain cell nuclei, for 5 min at room temperature. Fluorescence images were photographed using a Zeiss AxioCam MRcs fluorescence microscope (Carl Zeiss Optical Inc., Germany) equipped with a Nikon DXM1200F Ultra High-Quality Digital Camera (NITAL S.p.A., Turin, Italy).

215 MTT (3-dimethylthiazol-2,5-diphenyltetrazolium bromide) colorimetric assay

After incubation (14 and 21 days), the medium was removed; 200 µL of MTT (Sigma, Milan, Italy) solution (5 mg/mL in DMEM without phenol red) and 1.8 mL of DMEM were added to the cell monolayer; the multi-well plates were incubated at 37°C for further 4 h. After discarding the supernatants, the dark blue Formosan crystals were dissolved by adding 2 mL of solvent (10% HCl 1N in isopropanol, Sigma, Milan, Italy) and quantified spectrophotometrically (Secomam, Anthelie light, version 3.8, Contardi, Italy) at 570 and 690 nm. In the control cultures, the cells were placed

directly into adherent polystyrene culture plates at the same culture density as placed onto the
samples. The mean and the standard deviations were obtained from three different experiments of
the same specimen.

225 Morphological and compositional characterization (SEM-EDS)

Morphological analysis (SEM; Philips 525M) and compositional analysis (EDS, Philips EDS 9100) were performed on surfaces and fractured sections (in liquid nitrogen) of all composite specimens. The samples were sputter coated with silver prior to examination.

Samples from cell culture tests were fixed in 2% glutaraldehyde (Sigma-Aldrich) in 0.1M
cacodylate buffer (pH 7.4, Sigma-Aldrich), post-fixed in 1% osmium tetroxide (Sigma, Milan,
Italy), dehydrated in increasing ethanol (Sigma-Aldrich) concentrations, CPD-dried, mounted on
aluminum stubs, gold-sputtered by the Edwards Sputter Coater B150S equipment, and observed
with a Philips XL 20 SEM (FEI Italia SRL, Milan, Italy) microscope.

234 Statistical Methods

All quantitative data were presented as mean \pm standard deviation, unless otherwise noted. Statistical analysis was carried out using single-factor analysis of variance (ANOVA). A value of p <0.05 was considered statistically significant.

238

239 RESULTS AND DISCUSSION

240 Porosity and morphological analysis

The physical characteristics of a scaffold can be described by the average pore size, pore size distribution, pore volume, pore interconnectivity, and pore shape. Porosity (% vol) is defined as

the percentage of void space in a solid;³⁸ it is a morphological property independent on the material. 243 Pores are necessary for bone tissue formation because they allow migration and proliferation of 244 osteoblasts and mesenchymal stem cells, as well as the proper vascularization of the implant.³⁹ In 245 addition, a porous surface improves the mechanical interlocking between the implant biomaterial 246 247 and the surrounding natural bone, providing greater mechanical stability at this critical interface.⁴⁰ Optimal pore diameters for 3D porous structures for bone repair are in the 100-400 µm range,25 248 suitable for human osteoblast cell penetration, and a minimum pore size is required for tissue 249 ingrowth,⁴¹ interconnectivity for access to nutrients and transport of waste products and pore shape, 250 and roughness for better cell spreading.⁴² 251

The porosity analysis within the scaffolds was determined by µ-CT analysis. Pore distribution and 252 3D-reconstruction of scaffolds are shown in Figure 1 and Table I. The porosity was found to vary 253 254 from 67.1 to 84.8% depending on the percentage addition of CEL2. In particular, the total porosity decreased with increasing CEL2 amount because the bioactive glass particles were deposited onto 255 the G/CH walls and they filled part of void space of G/CH matrix, as confirmed subsequently by 256 SEM examination [Fig. 2(b,c)]. A 3D representation of the scaffolds is shown in Figure 1 and was 257 used to calculate the pore size distribution. All results demonstrated that the scaffolds exhibited a 258 porous distribution with both macropores (size between 75 and 300 µm) and micropores (size 1-259 260 75 µm), which presence is crucial for protein and cell adhesion. Detailed analysis indicated that 80% of pores within the resultant scaffolds had a pore size in the range of 75–300 µm. The mean 261 pore size was found to vary from 179.3 µm for CEL2/POL 0/100 scaffolds to 136.2 µm for 262 263 CEL2/POL 70/30 composites. Moreover, in all composite porous matrices, a high interconnected network of pores (about 95.6–97.5% by μ-CT analysis) was observed. Pore size may be controlled 264 by the temperature set in the freeze-drying process: pore diameters increase with increasing 265 temperature due to a higher ice crystal growth rate.⁴³ The pores within the scaffold arise from the 266

ice crystals that form during freezing of the G/CH solution. This process forces the polymer to form 267 268 aggregates in the interstitial spaces and creates an interconnected network of polymer fibrils. A previous study has reported that the pore size of a gelatin scaffold can be adjusted by altering the 269 polymeric concentration, the freezing rate and the pH value since these factors are known to affect 270 both the nucleation and the growth rate of the ice crystals.⁴⁴ A higher gelatin concentration and 271 higher freezing rate of the dispersion produced a lower porosity and smaller pores. Higher porosity 272 and larger pore sizes scaffolds could be obtained by a lower polymeric concentration and low 273 freezing rate. 274



Figure 1. Pore distribution and 3D-reconstruction of (a) CEL2/POL 0/100 (b) CEL2/POL 40/60

277 (c) CEL2/POL 70/30 scaffolds as obtained by μ -CT.



Figure 2. SEM micrographs and EDS spectra of CEL2/POL scaffolds: fractured section of (a)

281 CEL2/POL 0/100, (b) CEL2/POL 40/60, (c) CEL2/POL 70/30.

282 Table I. Pore Data of CEL2/POL Scallolds Obtained by μ -C

CEL2/POL sample	Porosity (%)	Pore interconnectivity (%)	Mean pore size (µm)
0/100	84.8	97.5	179.3
40/60	72.5	96.0	160.6
70/30	67.1	95.6	136.2

283

279

It should be noted that the μ -CT pore size analysis in this study was performed on dry scaffolds. Generally, the polymeric scaffold shrinks in the drying process. The scaffold will expand when wetted in aqueous solution as reported in the paragraph relative to swelling tests; so the pore size in the wet condition will be larger than that reported above.

288

SEM analysis was performed on selective portions of the composite scaffolds to evaluate the effect of composition on sample morphology. Figure 2 reports SEM images of the fractured sections with the corresponding EDS spectra of CEL2/POL scaffolds. Porous scaffolds showed a typical foamlike morphology with interconnected pores with a wide distribution of pore sizes and wall 293 thickness. As it can be observed in Figure 2, pore walls increased their thickness with increasing CEL2 amount, which gave the foams a more compact structure. For scaffolds containing 40 wt % 294 of bioactive glass, CEL2 clusters of several microns (60-80 µm) were observed, but in composites 295 containing 70 wt % CEL2, the particles appeared more uniformly distributed. EDS spectra of G/CH 296 scaffolds [Fig. 2(a)] showed the characteristic elements of gelatin and chitosan: carbon (C), 297 nitrogen (N), and oxygen (O) while EDS spectra of the composites showed also the characteristic 298 299 elements of CEL2: silicon (Si), potassium (K), sodium (Na), magnesium (Mg), calcium (Ca), and phosphorus (P) [Fig. 2(b,c)]. 300

301

302 Swelling tests

One of the main factors to contribute to biocompatible nature of biomaterials is the water content 303 which imparts several unique physiochemical properties to the material. A polymer matrix 304 imbibing an adequate amount of water shows similar properties to living tissue-like membranes: 305 physiological stability, low interfacial tension, permeability to biomolecules, etc.⁴⁵ Moreover, 306 swelling increases also the pore size and total porosity, thus maximizing the internal surface area 307 of the scaffolds. Scaffolds showing higher degree of swelling will have a larger surface area/volume 308 ratio thus allowing the porous matrices to have the maximum probability of cell infusion into the 309 310 3D scaffold as well as maximum cell growth by attachment to the scaffold surfaces. The increase in swelling also allows the scaffold to avail nutrients from culture media more effectively. 311 However, while the swelling would promote cell adhesion, it could lower its mechanical properties. 312 313 Thus for CEL2/POL composites, the influence of chemical composition of the composites on their water intake has been investigated. Figure 3 reports the swelling degree as a function of time for 314 composite porous matrices with different compositions. All composites showed a similar swelling 315 behavior as a function of time: swelling degree slightly increased as a function of time from 6 to 316

317 24 h. CEL2/POL 0/100 scaffolds displayed the maximum swelling degree at every time interval. 318 At 6 h, the swelling degree was about $884 \pm 47\%$, while at 12 and 24 h the swelling ratio was 973 319 $\pm 13\%$ and $1049 \pm 40\%$, respectively. For CEL2/POL 40/60 samples, at 6 h the swelling degree 320 was about $568 \pm 29\%$. At 12 and 24 h, the swelling degree increased not significantly. Moreover, 321 for CEL2/POL 70/30 composites, at 6 h swelling ratio was about $259 \pm 50\%$, while at 12 and 24 h, 322 the swelling degree slightly increased.





Figure 3. Swelling behavior of scaffolds as a function of time. Data are averaged on three measurements. Bars indicate standard deviation (n = 3).

At each time, swelling degree was found to decrease with increasing CEL2 amount. The results were not surprising and were attributed to the lower hydrophilicity of the inorganic phase as compared to the polymeric matrix: the increase in the inorganic fraction of the composite resulted in a decreased water sorption. In addition, the increasing polymer-bioactive glass interaction with increasing concentration of CEL2 resulted in a slower relaxation of polymer chains, which also decreased the swelling ratio.

334 Bioactivity evaluation

An essential requirement for an artificial material showing bioactivity is the formation of a 335 biologically active bone-like apatite on its surface when in contact with the physiological 336 337 environment. This property can be evaluated in vitro by incubation in SBF. There is an oscillating phenomenon of precipitation and dissolution processes in vitro, which is due to metastable SBF. It 338 was reported that the precipitation and dissolution processes of bone like apatite take place during 339 340 the immersion of bioactive materials in SBF. Hench reported that there is a good correlation of in vitro bone-like apatite formation from SBF and in vivo bone-like apatite (calcium phosphate) 341 formation needed to secure bone bonding.⁴⁶ CEL2/POL composite scaffolds were investigated after 342 343 immersion in SBF by SEM-EDS to check the formation of an apatite layer onto the composite surface. The interaction between the surface of the composites and SBF solution may be 344 responsible for the apatite nucleation. Various bioactive ceramics such as TCP and Bioglass® have 345 been developed to be used clinically in bone repair.⁴⁷ These have been found to bond with bone 346 through a layer of bone-like apatite formed on the surface of the ceramics when implanted into the 347 body. This apatite has been characterized as carbonate-containing HA and was not observed at the 348 interface between non-bioactive (or bio-inert) materials and bone.⁴⁸ 349

350

Figure 4 reports SEM images with the corresponding EDS spectra of the fractured section of CEL2/POL scaffolds after soaking in SBF for 2, 7, and 14 days, respectively. CEL2/POL 0/100 scaffolds did not induce the precipitation of calcium phosphate crystals at any test time as shown in Figure 4(a,d,g). As suggested by Cai and Kong.^{49, 50} CH and G are characterized by the lack of bioactivity, which severely limits their biomedical applications; thus this feature needs to be provided by the addition of biologically active materials. For composite scaffolds, after 2 days of incubation in SBF, small amount of calcium phosphate crystals were observed as shown in Figure

4(b,c) (SEM image and EDS spectra). After 7 days of incubation, substantial amount of apatite 358 microparticles with a diameter up to 2-4 µm were formed on the surface of the pore walls of the 359 composite scaffolds [Fig. 4(e,f)]. After 14 days of incubation, the whole pores of CEL2/POL 40/60 360 361 and 70/30 composites were entirely covered by a layer of apatite [Fig. 4(h,i)]. Furthermore, the EDS spectra displayed the presence of small amounts of Mg, Si, Na, and K ions incorporated in 362 the mineral phases, due to the remaining CEL2. In conclusion, an increasing incubation time of the 363 364 composite scaffolds in SBF (from 2 to 14 days) led to the formation of a higher amount of apatite. However, the interconnected macroporous structure of the scaffolds was maintained, which is 365 important for cell migration and mass transport when the scaffolds is implanted in vivo. Moreover, 366 after 14 days of immersion in SBF, EDS spectra recorded from the samples covered with the 367 inorganic aggregates deposited on CEL2/POL scaffolds after SBF tests [Fig. 4(h,i)] allowed the 368 calculation of Ca/P molar ratio which resulted in 1.58 and 1.61 for CEL2/POL 40/60 and 70/30, 369 respectively. These values are very close to the stoichiometric Ca:P value of hydroxyapatite 370 (1.67).⁵¹ Figure 5 shows the magnification of SEM micrographs relative to CEL2/POL 40/60 and 371 70/30 composites after 14 days of SBF immersion. The results indicate that the increasing addition 372 of CEL2 enhances the bioactivity of composite scaffolds containing chitosan/gelatin as the organic 373 phase. The mechanism of apatite formation in SBF was described by several researchers.^{52, 53} It 374 375 was reported that the formation of apatite on artificial materials is induced by functional groups which could reveal negative charge and further induce apatite deposition via the formation of 376 377 amorphous calcium phosphate. In this research, the major reason for the enhancement of apatite formation on the composite scaffolds might be the bioactive glass particles acting as nucleation 378 initiation sites. In fact, CEL2 is a highly bioactive glass and the ability of CEL2 to induce the 379 precipitation of HA (both as a macroporous scaffolds and as a filler in gelatin films) has been 380 previously documented.^{54, 55} An increasing amount of CEL2 in the composite scaffolds was 381

associated with the presence of a higher density of nucleation sites for HA, and as a result a higher
amount of apatite could be deposited at each time. Once the apatite nuclei have been formed, they
can grow spontaneously by consuming the calcium and phosphate ions present in the surrounding
fluid.

386



387

Figure 4. SEM micrographs and EDS spectra of CEL2/POL scaffolds after immersion in SBF for
different intervals: after 2 days (a) CEL2/POL 0/100, (b) CEL2/POL 40/60, (c) CEL2/POL 70/30,
after 7 days (d) CEL2/POL 0/100, (e) CEL2/POL 40/60, (f) CEL2/POL 70/30, and after 14 days
(g) CEL2/POL 0/100, (h) CEL2/POL 40/60, (i) CEL2/POL 70/30 (bar 100 μm).



393

Figure 5. SEM micrograph magnifications of CEL2/POL scaffolds after immersion in SBF for 14
days: (a) CEL2/POL 40/60 and (b) CEL2/POL 70/30.

396

397 Mechanical characterization

One of the major critical point in developing load-bearing scaffolds for bone tissue engineering is 398 399 the conflicting requirement of scaffolds with high porosity and mechanical strength. A highly porous structure is preferred in favor of cell growth and proliferation, but it is generally achieved 400 401 at the expense of mechanical strength. In the scientific literature, compressive strength of substrates has often been found to decrease with increasing pore size.⁵⁶ The mechanical properties of the 402 porous composite scaffolds in terms of compressive strength were tested using a mechanical testing 403 404 machine. The force was analyzed from stress-strain data obtained under a compressive load at a 405 constant speed.

Figure 6 shows the stress–strain curves obtained for the porous composite scaffolds by the excessive compression test at strain of 0–60%. During the test, the composites did not show a final fracture; rather, they underwent densification. The curves were classified in three distinct regions: linear elastic, collapse plateau, and densification regimes as reported in.⁵⁷ The values of elastic

modulus (E*), collapse strength, and strain (σ^* and ε^* , respectively), and collapse modulus ($\Delta\sigma/\Delta\varepsilon$) 410 411 were calculated from the curves are listed in Table II. A significant increase of compression Young's modulus was obtained by adding inorganic phase into the polymeric matrix, due to the superior 412 compression behavior of CEL2 as compared to POL phase. As shown in Figure 6 and in Table II, 413 414 the collapse strength and collapse strain were characterized by a different trend as a function of the 415 CEL2 amount. In particular, the increase of the inorganic phase caused a progressive slight decrease 416 in the deformability of the composite scaffold and an increase of the collapse strength and collapse modulus. 417



Figure 6. Stress–strain curves of the porous composite scaffolds compressed at a strain of (0–60%).

420 The cross-head speed was 0.01 mm \cdot s⁻¹

421

422 Table II. Elastic Modulus, Collapse Strength and Strain, and Collapse Modulus Calculated from

423 the Corresponding Stress–Strain Curves

CEL2/POL sample	<i>E</i> * (kPa)	σ* (kPa)	ε* (%)	Δσ/Δε (kPa)
0/100	1227.2 ± 116.4	203.5 ± 21.8	21.7 ± 3.0	203.7 ± 41.2
40/60	1403.0 ± 111.2	214.1 ± 6.4	19.9 ± 2.1	350.1 ± 38.2
70/30	2120.6 ± 106.9	374.0 ± 7.1	17.5 ± 2.1	737.2 ± 38.6

424

It is generally accepted that the scaffolding material for bone tissue engineering should have 425 mechanical strength as close as possible to the strength of the bone to be repaired or substituted. In 426 this study, a compressive modulus of 2.1 MPa was obtained for CEL2/POL 70/30 scaffold by 427 adjusting processing conditions to achieve a highly densified porous structure. The obtained 428 scaffolds, containing 70 wt % CEL2, had a compression Young's modulus comparable to the 429 modulus of alveolar bone.⁵⁸ Moreover, the composite matrices are expected to be suitable 430 candidates for the articular cartilage/subchondral bone regeneration. As described above, a graded 431 432 biomimetic osteochondral composite scaffold is necessary. Different methods were reported in literature to prepare bi-layered scaffolds,⁵⁹⁻⁶¹ generally based on two consecutive different 433 procedures (e.g. sintering and freeze-drying). In our case, graded scaffolds could be easily obtained 434 by casting the mixture solutions before gelling: the lower water solubility and higher density of 435 CEL2 as compared to the polymeric phase caused the progressive precipitation of CEL2 at the 436 bottom of Petri dishes during solvent evaporation. 437

Both storage and loss modulus (E' and E") were measured in the frequency range 0.1–40 Hz, which are typical frequencies found in physiological situations in load-bearing applications.⁶² The storage modulus (E') is about one order of magnitude higher than the loss modulus (E") indicating an elastic nature of the scaffolds. The storage and loss modulus behavior as a function of the frequency of the loading cycle is reported in Figure 7(a,b). The trend of both moduli is quite similar in each single scaffolds batch (CEL2/POL 0/100, CEL2/POL 40/60, or CEL2/POL 70/30), whereas the

behavior differs in the case of different series (wholly polymeric or composite samples). As regards 444 the wholly polymeric scaffolds, storage and loss modulus remained roughly constant at low (below 445 1 Hz) and mid (1-10 Hz) frequencies, and showed an increase for higher frequencies. On the 446 contrary, composite scaffolds (CEL2/POL 40/60 and CEL2/POL 70/30) are characterized by a 447 more complex behavior, and the corresponding curves plotted in Figure 7(a,b) can be divided into 448 three distinct regions. At low frequencies (below 1 Hz), both storage and loss modulus of porous 449 composites increased with increasing frequency; afterward, there was a drop of E' and E" around 450 1 Hz, and for higher frequencies both moduli increased again. there is an increase in E" for high 451 452 frequencies, which suggests that the material exhibits some dissipation capability for high 453 frequencies. Moreover, it is worth to underline that the storage modulus is about one order of magnitude higher than the loss modulus, which indicates the predominantly elastic nature of the 454 prepared composite scaffolds in dry state. Although the Young's modulus, which was calculated 455 from the slope of the initial part of the stress-strain curve, can be considered conceptually similar 456 to the storage modulus, they could not be directly compared as the latter one is dependent on 457 frequency. However, according to Malafaya et al.,63 we considered E' and E'' acquired at a 458 frequency of 1 Hz as reference values for purpose of comparison (Table III). These values of 459 storage modulus are comparable, as order of magnitude, to those of Young's modulus acquired 460 461 under static conditions for all the three scaffold batches.



463

Figure 7. Dynamic mechanical analysis of CEL2/POL scaffolds showing: (a) the storage (E'), (b)
loss (E") modulus behavior, and (c) the loss factor (tan δ) for increasing frequencies under dynamic
compression solicitation.

467

470

Table III. Mean Values of Storage (E') and Loss (E") Modulus of the Different Scaffolds Series

CEL2/POL sample	<i>E</i> ' (kPa)	<i>E</i> " (kPa)
0/100	920	180
40/60	1768	295
70/30	3220	916
70/30	3220	916

469 Acquired at a Frequency of 1 Hz

471 The loss factor tan $\delta = E''/E'$, measuring the ability of dissipating the cyclic mechanical energy in

472 form of heat, is plotted in Figure 7(c). Composite scaffolds show a remarkable dissipation ability,

related to damping properties, especially at low and high frequencies, which can be a very usefulfeature in view of *in vivo* implantation.

Investigation of the mechanical properties of glass/polymer scaffolds by DMA is new with respect to previous literature. However, we cannot ignore that the results presented in this work represents a preliminary achievement, as the samples were tested in dry state; more accurate data could come from DMA on the composite scaffolds in wet state, to better mimic the physiological conditions in which the materials will be potentially used.

480

481 Cell compatibility

482 Overall, cells displayed a good ability to interact with the different tested scaffolds which did not 483 modify cell metabolic activity at the analyzed points (i.e. 14 and 21 days). Histological sections 484 stained with DAPI demonstrated the presence of a small amount of cells in the central part of the 485 scaffold (Fig. 8).

486



488 Figure 8. Section of the central part of CEL2/POL 30/70 scaffold that evidenced the presence of



490 Comparing the data obtained at 14 and 21 days of culture, MTT test proved only a slight difference 491 between the two cytotypes analyzed (Fig. 9). On CEL2/POL 0/100, an increase in cell proliferation 492 was observed only for PCs while no changes were detected for MG63. A significant (p < 0.01) 493 increase in cell proliferation for both cell cytotypes cultured on CEL2/POL 40/60. Interestingly, 494 while no differences were detected in MG63 cultured on CEL2/POL 70/30 a significant (p < 0.01) 495 reduction of this parameter was detected for PCs.





498 Figure 9. Histogram of MTT test performed on MG63 (a) and PCs (b) cultured on CEL2/POL

499 100/0, 40/60, and 30/70 for 14 and 21 days.

500

- 501 SEM observations of PCs cultured on the different scaffolds were consistent with MTT data,
- showing changes in cell morphology (Figs. 10 and 11). At 14 days of culture, cells on CEL2/POL

503 0/100 were elongated forming a uniform sheet on the scaffolds' surface [Fig. 10(a,d)]. At 21 days, 504 cells resulted more spreaded and tried to grow inside pores [Fig. 11(a,d)]. On CEL2/POL 40/60 [Figs. 10(b) and 11(b)] cells were elongated and less uniformly distributed in comparison with 505 CEL2/POL 0/100. This phenomenon may be at least in part related to not uniform surface of the 506 507 scaffold that hampered initial cell adhesion and, consequently, cell proliferation. The reduced cell 508 density was more evident on CEL2/POL 70/30, which were the scaffolds with the most uneven 509 surface. On these scaffolds, cells displayed a more irregular morphology that stretched out to cross scaffold macroporosity [Fig. 10(c,f)]. This irregular star-shaped aspect was maintained also at 21 510 511 days of culture [Fig. 11(c,f)], suggesting that different chemical composition, affecting scaffold macro- and microstructure and stiffness, could influence cell differentiation,^{64, 65} as already shown 512 in our previous work.66 Cell proliferation decreases as differentiation signs increased. In this 513 respect, our results suggest that scaffolds with an increased amount of inorganic phase (i.e. 514 CEL2/POL 70/30) may stimulate PCs differentiation into an osteoblastic progeny. In contrast, MG-515 63 cells appear to hold different cross-talks with the different tested scaffolds than PCs. These cells 516 are immortalized, immature and have a high proliferative potential that probably slow down their 517 differentiation capability without any additional treatment. 518



Figure 10. SEM observation of PCs cultured for 14 days on CEL2/POL 100/0 (a,d), CEL2/POL
40/60 (b,e), and CEL2/POL 30/70 (c,f). Scale bar a–c 100 μm; scale bar d–f 20 μm.

523

524 CONCLUSIONS

Freeze-dried CEL2/POL scaffolds (0/100; 40/60; 70/30 wt %/wt) showed an interconnected 525 network of macropores with 100-200 µm average size as shown by SEM and µ-CT analysis. As 526 the amount of CEL2 increased, the total porosity and the mean pore size slightly decreased because 527 the bioactive glass particles deposited onto the polymeric pore walls and filled part of the void 528 space of the matrix. Furthermore, composites containing CEL2 were particularly interesting due to 529 their stability in aqueous solution as evidenced by swelling tests and to their pronounced bioactivity 530 and expected consequent bone-bonding ability during in vivo trials. In fact, they are expected to 531 react with physiological fluids, forming hydroxyapatite layers on the film surface containing 532

inorganic phase and creating strong bonds to hard and soft tissues through cellular activity. As evidenced by SBF immersion tests, an increasing CEL2 amount greatly enhanced the bioactivity of the scaffold: glass particles behaved as nucleation sites for apatite crystallization. The elastic modulus of the composites with the highest glass content (70 wt %) was found to be comparable to that of alveolar bone. DMA carried out on the composite scaffolds in dry state shows that the samples exhibit a remarkable dissipation ability especially at low and high frequencies; this damping effect could be a useful feature in view of in vivo implantation.

Additional work is in progress to increase the mechanical resistance of the scaffolds by the substitution of gelatin with collagen in the organic phase and the use of combined crosslinking techniques and/or blending strategies with the aim to extend the application of CEL2-based composites to the repair of other bone defects.

Morphological and biochemical analysis performed with a continuous cell line (MG63) and with human periosteal-derived stem cells seeded on the CEL2/POL scaffolds showed that cells maintain their metabolic activity and ability to proliferate on the scaffold. Differentiation and over proliferation occurred to PCs, at the increase of bioactive glass concentration, reveal the capacity of tested scaffold to modulate osteogenic properties.

Therefore, the proposed scaffolds, which are resorbable, bioactive, and capable to modulate cell proliferation/differentiation processes, may be interesting tools in osteochondral tissue regeneration. Further studies are in progress to validate this hypothesis.

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