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1 Removal and fate of endocrine disruptors chemicals under lab-scale 2 posttreatment stage. Removal assessment using light, oxygen and 3 microalgae.

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12 **Abstract:**

13 The aim of this study was to assess the effect of light, oxygen and microalgae
14 on micropollutants removal. The studied micropollutants were 4-(1,1,3,3-
15 tetramethylbutyl)phenol (OP), technical-nonylphenol (t-NP), 4-n-nonylphenol (4-NP),
16 Bisphenol-A (BPA). In order to study the effect of the three variables on the
17 micropollutants removal, a factorial design was developed. The experiments were
18 carried out in four batch reactors which treated the effluent of an anaerobic
19 membrane bioreactor. The gas chromatography mass spectrometry was used for the
20 measurement of the micropollutants. The results showed that light, oxygen and
21 microalgae affected differently to the degradation ratios of each micropollutant. The
22 results showed that under aerated conditions removal ratios higher than 91 % were
23 achieved, whereas for non-aerated conditions the removal ratios were between 50
24 and 80 %, except for 4-NP which achieved removal ratios close to 100 %. Besides, mass
25 balance showed that the degradation processes were more important than the
26 sorption processes.

27 **Keywords:**

28 Alkylphenol, endocrine disruptor, microalgae, wastewater treatment plant.

29 **1. Introduction.**

30 In recent years, several micropollutants have been detected in natural
31 environments, mainly due to the use of manufactured products, such as surfactants,
32 pesticides or plastic reinforcements. Some of these chemicals are able to disrupt the
33 endocrine system. Therefore, those substances are called endocrine disruptor
34 chemicals (EDCs). EDCs are of global concern due to their widespread occurrence,

35 persistence, bioaccumulation and potential adverse effects on ecosystem functioning
36 and human health. Nevertheless, EDCs can be removed by the action of wastewater
37 treatment plant (WWTPs) (Clara et al., 2005; González et al., 2007).

38 4-(1,1,3,3-tetramethylbutyl)phenol (OP) and technical-nonylphenol (t-NP) are
39 known as alkylphenol (APs) and are degradation metabolites of alkylphenol
40 polyethoxylates (APEOs). The annual global production of APEOs is approximately
41 500,000 tons, which approximately an 80% correspond to nonylphenol polyethoxylates
42 (NPEOs), whereas the remaining 20% correspond to octylphenol polyethoxylates
43 (OPEOs) (Lin et al., 2010). APEOs are commonly used in the formulation of a large
44 variety of detergents, paints, lubricants, resins, and pesticides (Sharma et al., 2009).
45 The toxicity of APEOs increases with decreasing ethoxylates chain length (Careri et al.,
46 2003). Due to APs are more lipophilic than APEOs, these biotransformation
47 metabolites are more toxic than APEOs. The estrogenic activity observed appeared to
48 be confined to para- or 4 substituted compounds (Jobling and Sumpter, 1993).
49 Mentioned estrogenic activity became stronger with the increase in the number of the
50 alkyl carbons, being this activity maximized with a nonyl- chain. Phenol shows weak
51 estrogenic activity, whereas anisole was completely inactive (Tabira et al., 1999).
52 Several reports have demonstrated that these EDCs can accumulate due to high
53 stability and lipophilicity, and thus, EDCs can affect endocrine systems in fishes and
54 birds. Therefore, these compounds can spread to humans via the food chain (Jobling
55 and Sumpter, 1993; Manente et al., 2011).

56 4-n-nonylphenol (4-NP) is an alkylphenol, but it is not a metabolite of APEOs,
57 and thus, its occurrence in environment is infrequent (de Weert et al., 2010).
58 Moreover, its biodegradability is higher than OP and t-NP biodegradability due to the
59 linear chain of 4-NP presents a secondary carbon attached to C4 position of aromatic
60 ring which is less resistant than the quaternary carbon of t-nonylphenol under both
61 aerobic and anaerobic conditions (Corvini et al., 2006; Abargues et al., 2012; Porter et
62 al., 2012).

63 BPA is principally used in the production of epoxy resins and polycarbonate
64 plastics as a monomer. BPA can interfere in cell division mechanism, as well as mimic
65 the female estrogen E2 (Sharma et al., 2009; Gattullo et al., 2012). Several authors
66 confirmed that BPA presents poor biodegradation under anaerobic conditions in both
67 suspended and soluble fractions (Ike et al., 2006), whereas its biodegradability
68 increases under aerobic conditions (Kang and Kondo, 2002).

69 The Directive 2000/60/EC, also known as Water Framework Directive (WFD), is
70 probably the most significant international legislation in the field of water from many
71 years and its aim is to improve, protect and prevent further deterioration of water

72 quality across Europe (Allan et al., 2006). WFD includes and protects different kinds of
73 water in Europe (surface water, groundwater, transitional and coastal) with the aim to
74 achieve and ensure a good quality for all of them. WFD includes as priority substances
75 the OP and 4-NP studied. Furthermore, Directive 2008/105/EC lays down
76 environmental quality standards (EQS) for priority substances and certain other
77 pollutants as provided for in WFD. The Directive 2008/105/EC establishes the extent
78 permitted of OP and 4-NP in inland and other surface waters. So, attention must be
79 paid on the fate of these substances in order to fulfill the WFD requirements.
80 Furthermore, the proposal for a Directive 2011/0429 (COD) added t-NP to the list of
81 priority substances, laying down EQS for these substances.

82 The removal of EDCs in WWTPs can be carried out by aerobic and anaerobic
83 process. Several works showed that the concentrations of OP and t-NP were increased
84 during anaerobic treatment, whereas it was observed an effective removal after
85 aerobic activated sludge treatment (Janex-Habibi et al., 2009). Elimination of OP, t-NP,
86 4-NP and BPA have been studied by several authors in conventional treatment plant
87 (CTP) or membrane bioreactor (MBR) operational configurations (Clara et al., 2005;
88 González et al., 2007). The removal ratios obtained in the MBR showed better results
89 than the ones reported for the CTP.

90 Besides, the microalgae culture can be used as removal system of EDCs. The
91 work of Nakajima et al., (2007) showed the removal of BPA by accumulation in
92 microalgae cells after an incubation period with microalgae culture. Other authors
93 observed the photodegradation of BPA is enhanced by algae. The algae may produce
94 some secretions which after irradiation can produce hydroxyl radicals that can
95 enhance the BPA degradation (Peng et al., 2006). The OP and t-NP removal can be
96 improved by the cyanobacteria cells, this effect was enhanced at low concentrations of
97 OP and t-NP (Stoichev et al., 2010). Whereas, the works developed by Corvini et al.,
98 (2006) proposed a mechanism for degradation of nonylphenols with bacterial strain
99 *Sphingomonas* sp. which initial step of degradation is an ipso-substitution.

100 The aim of this research was to study the removal and fate that OP, t-NP, 4-NP
101 and BPA experience in the presence of light, oxygen and microalgae. The experimental
102 study was designed as a posttreatment stage of a Submerged Anaerobic Membrane
103 BioReactor (SAnMBR) located in the Cuenca del Carraixet WWTP in Alboraya (Valencia,
104 Spain). Degradation experiments combining the studied variables were carried out in
105 batch reactors. In order to observe the fate of EDCs in the system, a mass balance was
106 performed considering both the soluble and the suspended fraction.

107 **2. Materials and methods**

108 2.1. Fractional factorial design and set up reactors

109 In order to study the effect of light (P), oxygen (O) and microalgae (M) on the
110 removal of micropollutants, a factorial experimental design was developed (Box and
111 Hunter 1961). A full 2^k factorial design requires all combinations of two versions (n) of
112 each variable (f). The total number of experiments carried out was $8 (n^f)$, which
113 corresponds to three variables (light, oxygen and microalgae) and two version for each
114 variable. The eight described experiments were reduced to five experiments (see Table
115 1). The removed experiments were those having the variable microalgae without
116 variable light, because microalgae growth is inhibited under those conditions.

117 The experiments were carried out in batch mode, and the experimental setup
118 was shown in supplementary Fig. S1, which consists of four Pyrex® reactors of 2.0 L of
119 total volume, with a working volume of 1.6 L. The reactors were kept under agitated
120 conditions in a Walk-in Ineltec climatic chamber (Tona, Barcelona, Spain), at 20 ± 1 °C.
121 The reactors were fed with 800 mL of a SAnMBR pilot plant effluent. The remaining
122 800 mL were filled with raw microalgae culture for “POM” (light, oxygen and
123 microalgae) experiment and 800 mL of pure water for “PO” (light and oxygen), “P”
124 (light) and “O” (oxygen) experiments.

125 The developed experiments under forced aeration were carried out with a
126 compress air stream (3 bar) (Atlas Copco, ZT-37-FF, Stockholm, Sweden). The compress
127 air was connected to a diffuser at the bottom of the reactors, so the bubbles kept the
128 reactors agitated. The value of oxygen saturation is 8.0 mg O₂/L at 20 ± 1 °C and
129 101.325 kPa (Lide, 2012). The dissolved oxygen was measured by OxiCal-SL Cellox 325
130 probe (WTW, Weilheim, Germany), connected to the Multi 340i meter (WTW,
131 Weilheim, Germany). In order to maintain the pH between 7.2 and 7.5 in the
132 microalgae culture reactor (POM), a stream of carbon dioxide was used. The pH was
133 measured by WTW SenTix 41 probe (WTW, Weilheim, Germany), connected to
134 Consort pH Meter model C861 (Turnhout, Belgium). Besides, the carbon dioxide
135 stream provides a source of inorganic carbon needed for microalgae growth. Both
136 gases, oxygen and carbon dioxide, were connected to the same diffuser.

137 The experiments under illuminated conditions were irradiated by four
138 fluorescent lamps (Sylvania GroLux, United Kingdom, London) of 18 W of nominal
139 wattage (590 mm width, 26 mm E.D.) which achieve a constant irradiation. The GroLux
140 lamp spectrum produces high concentration of photosynthetically active radiation
141 (PAR). PAR was measured in the illuminated surface of reactors, resulting in a value of
142 $120 \mu\text{E}/\text{m}^2\cdot\text{s}$. HOBO Photosynthetic Light Smart Sensor and HOBO Micro Station Data

143 Logger (MicroDAQ.com Ltd, Contoocook, NH, USA) were used in order to measure the
144 PAR.

145 The experiments under dark conditions were carried out with the reactors
146 wrapped with foil and the fluorescent lamps turned off.

147 Every reactor was spiked with 5.6, 24.0, 16.0 and 16.0 μg of OP, t NP, 4-NP and
148 BPA respectively. The chosen fortification corresponds to 5 times the average
149 concentration of the SAnMBR effluent pilot plant for each micropollutant (Abargues et
150 al., 2012).

151 The SAnMBR effluent used in the experiments comes from an anaerobic
152 bioreactor pilot plant of 1.3 m^3 total volume (0.4 m^3 head-space volume) connected to
153 two membrane tanks of 0.8 m^3 total volume each (0.2 m^3 head-space volume) which
154 treats urban wastewater (Giménez et al., 2011). Each membrane tank includes one
155 industrial hollow-fibre ultrafiltration membrane module (PURON® Koch Membrane
156 Systems (PUR-PSH31), 0.05 μm pore size). The SAnMBR pilot plant was located in the
157 Cuenca del Carraixet WWTP in Alboraya (Valencia, Spain).

158 The average wastewater characteristics of the SAnMBR effluent during the
159 studied period were: 309 ± 3 mg COD/L, 54 ± 14 mg BOD/L, 54 ± 6 mg $\text{NH}_4^+\text{-N/L}$, $8.5 \pm$
160 1.1 mg $\text{PO}_4^{3-}\text{-P/L}$, 70 ± 30 mg $\text{SO}_4^{2-}\text{-S/L}$, 128 ± 2 mg $\text{S}^{2-}\text{/L}$, 12 ± 3 mg COD/L of Volatile
161 Fatty Acids and 610 ± 110 mg $\text{CaCO}_3\text{/L}$ of Alkalinity. Solids, COD, BOD, sulphate,
162 sulphide, and nutrients were determined according to Standard Methods (APHA,
163 2005). The carbonate alkalinity and volatile fatty acids concentration were determined
164 by titration according to the method proposed by WRC (1992).

165 2.2. Reagents, solutions and microalgae culture

166 All the reagents were of analytical grade. 4-n-nonylphenol (4-NP) (CAS Number
167 104-40-5) and technical nonylphenol (t-NP) (CAS Number 84852-15-3) were obtained
168 from Riedel-de Haën (Seelze, Germany). 4-(1,1,3,3-tetramethylbutyl)phenol (OP) (CAS
169 Number 140-66-9) and bisphenol-A (BPA) (CAS Number 80-05-7) were purchased from
170 Sigma-Aldrich (Steinheim, Germany).

171 Ethanol was purchased from Panreac (Barcelona, Spain) and acetonitrile was
172 purchased from Sigma-Aldrich (Steinheim, Germany). The pure water was obtained by
173 means of a Synergy UV purification system purchased from Milli-Q (Millipore, Billerica,
174 MA, USA). Helium, nitrogen and carbon dioxide were purchased from Carbueros
175 Metálicos (Barcelona, Spain).

176 The stock solutions of standards were prepared in ethanol up to a maximum
177 concentration of 1000 mg/L. The more dilute solutions were prepared from stock

178 solutions directly in pure water up to a maximum concentration of 1 mg/L. All
179 solutions were kept at 4 °C until use.

180 The microalgae used as inoculum were obtained from the walls of the
181 secondary clarifier of the Carraixet WWTP and kept in the laboratory under semi-
182 continuous feeding of SAnMBR effluent and with continuous illumination varying
183 between 114 and 198 $\mu\text{E}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$. Microalgae from the chlorococcales order of the
184 Chlorophyceae class and cyanobacteria were identified as the main groups present in
185 the inoculum (Ruiz-Martinez et al., 2012). The pH of the medium was adjusted to
186 7.2-7.5 by using CO_2 .

187 2.3. Analytical Methods

188 Solid phase microextraction (SPME), as pre-concentration technique, was used
189 for the determination of the interest analytes (Guillot et al., 2006; Tan et al., 2008).
190 The pre-concentrated was analysed by gas chromatography coupled to mass
191 spectrometry detector (GC-MS).

192 In order to know the fate and removal of micropollutants both soluble and
193 suspended fractions were analysed. The final result was obtained by averaging the n
194 (3) repetitions performed for both fractions. The analyses were performed at room
195 temperature.

196 2.3.1. Soluble Fraction Analysis

197 The SPME procedure was carried out with 20 mL of sample, which were placed
198 in a 20 mL clear vial screw top (Supelco, Bellefonte, PA, USA) with a magnetic stir bar
199 (VWR International Eurolab, Barcelona, Spain). Polyacrylate fibre (Supelco, Bellefonte,
200 PA, USA) was immersed inside the sample with constant stirring (1500 rpm) during 60
201 min. The fibre was immediately removed and placed in the injection port of the GC-MS
202 for micropollutants desorption during 15 s. The described method was adapted from a
203 previous work (Moliner-Martinez et al., 2013).

204 2.3.2. Suspended Fraction Analysis

205 The POM reactor samples were centrifuged at 5000 rcf for 5 minutes
206 (Eppendorf centrifuge 5804 R, Brinkmann Instruments, Westbury, NY, USA). The
207 supernatant was discarded, whereas suspended fraction was dehydrated by
208 freeze-dried. 0.10 ± 0.01 g of the dehydrated sample was accurately weighted and
209 placed in a 20 mL clear vial screw top with 2.5 mL of ACN. The standards and samples
210 were weighed with a Mettler-Toledo microbalance XP105 Delta Range (Greifensee,
211 Switzerland) with a resolution of 0.01 mg. The samples were sonicated in an ultrasonic
212 bath for 60 min at 65 °C (150 W, 40kHz, JP Selecta, Barcelona, Spain), and then were
213 centrifuged at 5000 rcf for 5 minutes. 2.0 mL of supernatant were placed in a 20 mL

214 clear vial screw top with a magnetic stir bar (7 mm E.D., 20 mm width) and 18.0 mL of
215 water were added. After that, the soluble fraction was pre-concentrated with the
216 SPME-GC-MS technique describe above.

217 2.4. Chromatographic conditions

218 The whole analyses were performed on a gas chromatography-mass
219 spectrometry system (GC-MS) using 6890N GC with 5973 inert MS Detector (Agilent,
220 Palo Alto, CA, USA) equipped with a split/splitless injection port and operated by MSD
221 Chemstation Software (Agilent, Palo Alto, CA, USA). The capillary column is a fused-
222 silica HP-5ms Ultra Inert (30.0 m, 250 μ m I.D., 0.25 μ m film thickness) (Agilent, Palo
223 Alto, CA, USA).

224 The transfer line is held at 280 $^{\circ}$ C, and the ion source at 250 $^{\circ}$ C. The MS worked
225 in selected-ion-monitoring (SIM) mode and the electron impact energy is set to 69.9
226 eV. The GC-MS was operated in splitless mode and the injection port temperature was
227 held isothermally at 280 $^{\circ}$ C. The temperature program used was as follows: initial
228 temperature of 50 $^{\circ}$ C, 30 $^{\circ}$ C/min to 140 $^{\circ}$ C, held for 1 min, 20 $^{\circ}$ C/min to 280 $^{\circ}$ C, held
229 for 4 min, 30 $^{\circ}$ C/min to 310 $^{\circ}$ C, held for 2 min, for a total run time of 19 min. Helium
230 was used as carrier gas with a flow of 1.0 mL/min.

231 2.5. Analytical parameters

232 In order to find the characteristic ions and the relative abundance of each
233 compound the GC-MS system was carried out in full scan mode (scan range from 100
234 to 300 m/z).

235 The selected ion monitoring (SIM) mode analysis was used to determine the
236 quality assurance parameters such as detection and quantification limits, precision and
237 linearity. The analytical procedure was validated in terms of linear dynamic range and
238 intra-day precision (Relative Standard Deviation, RSD).

239 The limit of detection (LOD) and limit of quantification (LOQ) were determined
240 experimentally as the lowest concentration giving a chromatographic peak three times
241 the signal/noise ratio and ten times the signal/noise ratio, respectively.

242 2.5.1. Soluble fraction

243 Table 2 shows LOD, RSD, calibration line parameters, correlation coefficient and
244 lineal range for the analysis of the soluble fraction. The LOD values ranged from 2 to
245 500 ng/L.

246 The determined regression coefficients were always higher than 0.99, except
247 for 4-NP whose coefficient was 0.98. The precision for the methods was evaluated by

248 the statistical parameter RSD. The RSD values of the soluble fraction were obtained by
249 spiking aqueous samples with 1.0, 5.0, 10.0 and 50.0 µg/L for OP, 4-NP, t-NP and BPA
250 respectively of nominal concentrations. Satisfactory values equal or lower than 20 %
251 were obtained in all cases.

252 2.5.2. Suspended fraction

253 Table 3 shows LOD, RSD, calibration line parameters, correlation coefficient and
254 lineal range for the analysis of the suspended fraction. The LOD values ranged from 10
255 to 1000 ng/kg. The determined regression coefficients were ranged from 0.96 to 0.98,
256 except for BPA, whose regression coefficient was 0.90.

257 The RSD values of the suspended fraction were obtained by spiking the solid
258 sample with 0.4, 2.0, 4.0 and 20.0 µg/kg for OP, 4-NP, t-NP and BPA respectively.
259 Spiked solid samples were immediately sonicated and analysed. The obtained results
260 were lower than 18 % in all cases.

261 3. Results and discussion

262 3.1. Degradation of micropollutants without microalgae, oxygen and light

263 In order to check the spontaneous degradation of micropollutants, an
264 experiment without the variables light, oxygen and microalgae was carried out. The
265 observed relative concentration (C/C_0) was calculated as the concentration at specific
266 time divided by the initial concentration of each micropollutant. The C/C_0 was kept
267 between 90 % and 102 % showing that the natural degradation of micropollutants was
268 not significant, due to the RSD of the method was between 13 and 20 %.

269 3.2. Effect of light, oxygen and microalgae on micropollutants removal

270 The average characteristics of the microalgae culture reactor (POM) during the
271 experiment were 500 ± 200 mg TSS/L, 24 ± 10 mg NH_4^+ -N/L, 0.27 ± 0.07 mg NO_2^- -N/L,
272 1.1 ± 0.4 mg NO_3^- -N/L and 1.4 ± 1.3 mg PO_4^{3-} -P/L. The average values of dissolved
273 oxygen were 8.2 ± 0.5 , 8.1 ± 0.3 and 8.2 ± 0.4 mg O_2 /L for "POM", "PO" and "O"
274 experiments respectively. In order to remove the dissolved oxygen (DO) concentration
275 in the experiment "P", the reactor was bubbled with nitrogen during 30 min, reducing
276 the concentration value of DO to 1.8 ± 0.9 mg O_2 /L. Figure 1 shows the evolution of the
277 micropollutants soluble concentrations during the experiments.

278 The results obtained for OP and t-NP, in the soluble fraction, showed that in
279 "POM", "PO" and "O" experiments the micropollutants were removed faster than in
280 the "P", experiment, achieving removal ratios above 95 % after 22.5 h (the first quarter
281 of experiment) for aerated experiments. The removal ratios in the "P" experiment
282 were close to 50 % for both micropollutants. The removal ratios after 90 h were higher

283 than 96 % for “POM”, “PO” and “O” experiments while for “P” experiment the removal
284 ratios were lower than 66 % for OP and t-NP.

285 For 4-NP the four experiments achieved similar removal rates that the ones
286 achieved for OP and t-NP. The removal ratios were higher than 90 % after 22.5 h for
287 the “POM”, “PO” and “O” experiments and close to 75 % for the “P” experiment. After
288 90 h, the removal ratios were 100 % in all experiments. This behaviour can be
289 explained due to 4-NP is easier to degrade, because this micropollutant could undergo
290 the ipso-substitution mechanism described in literature (Corvini et al., 2006; Porter et
291 al., 2012).

292 The removal results obtained for BPA showed that aerated experiments
293 produced faster removal than the non-aerated experiment. The obtained removal
294 ratios in aerated experiments were between 91.9 and 99.8 % after the first 22.5 h.
295 Whereas, the non-aerated experiment showed removal ratios close to 80 %. The
296 removal ratios after 90 h were higher than 96 % for “POM”, “PO” and “O”. However
297 the removal ratio for “P” experiment was only 79.8 %. This value is significantly lower
298 than the values obtained in the aerated experiments.

299 In general the removal observed after 90 h in the “P” experiment was less
300 effective than in the other three experiments, except for 4-NP. The main difference
301 among the experiments was the lower DO concentration in the “P” experiment. The
302 DO value for “P” experiment was 1.8 ± 1.0 mg O₂/L, whereas for “POM”, “PO” and “O”
303 experiments was 8.2 ± 0.8 mg O₂/L. This observation is in accordance with literature
304 which suggests that the oxygen is necessary for attacking the aromatic rings (Lika and
305 Papadakis, 2009).

306 3.3. Mass Balance

307 The mass balance was calculated once the experiments were finished (90 h).
308 The suspended fraction, in “POM” experiment, was separated from supernatant by
309 centrifugation and analysed.

310 Two methods for carrying out the mass balance are described in the literature
311 (Carballa et al., 2007; Estrada-Arriaga and Mijaylova, 2011). The first method uses
312 measured data for soluble and suspended fractions, whereas the second method uses
313 the solid-water distribution coefficients to calculate the concentrations in the sludge
314 from those measured in the soluble phase. The method based on measure data was
315 used in this work. The mass of each micropollutant in influent (M_I) and effluent (M_E)
316 were determined according to the equations (1) and (2). The removal in the system
317 was studied separating the two processes: sorption (M_S) and degradation (M_D),
318 defined in Equations (3) and (4) respectively. The removal ratios by sorption processes

319 (R_S) and by degradation processes (R_D) were evaluated with the equations (5) and (6)
320 respectively.

$$321 \quad M_I = V \cdot S_I \quad (1)$$

$$322 \quad M_E = V \cdot (S_E + \text{TSS} \cdot X) \quad (2)$$

$$323 \quad M_S = V \cdot \text{TSS} \cdot X \quad (3)$$

$$324 \quad M_D = M_I - M_E - M_S \quad (4)$$

$$325 \quad R_S = 100 - ((M_S/M_I) \cdot 100) \quad (5)$$

$$326 \quad R_D = 100 - ((M_D/M_I) \cdot 100) \quad (6)$$

327 where M is the mass of EDCs (μg), V is the volume treated in batch system (L), S
328 is the micropollutant concentrations in the soluble fraction ($\mu\text{g/L}$), X is the
329 micropollutant concentrations in the suspended fraction ($\mu\text{g/kg}$) and TSS is the total
330 suspended solids concentration each mass flux of "POM" reactor (kg/L). The influent is
331 the permeate of SANMBR system, thus the concentration of TSS in influent is zero.

332 Table 4 shows the mass fluxes of micropollutants and the removal ratios based
333 on sorption and degradation processes in the soluble and suspended fractions for
334 "POM" experiment and for the soluble fraction for the other experiments. Low values
335 of R_S were observed in "POM" experiments indicating that accumulation in the
336 microalgae was insignificant. The R_S values ranged from 0.06 to 4.17 % respect to the
337 initial spiked concentration. This observation was in accordance with Nakajima et al.,
338 (2007). On the other hand, the removal of the soluble fraction was higher, being the
339 values of R_D higher than 90 % for all the micropollutants studied.

340 Comparing all the experimental conditions, high total removal ratios (R_S+R_D)
341 were achieved for t-NP. Values higher than 98 % were observed for aerated
342 experiments, whereas for "P" experiment the total removal ratio was 65 %. The R_D for
343 OP was higher than 98 % for aerated experiments, whereas it was closer to 50 % for
344 "P" experiment. Although the branched chemical structure of OP and t-NP make them
345 resistant to degradation, the aerated conditions produced removal ratios higher than
346 98%. The total removal ratios observed for 4-NP were higher than 99.9 % in all
347 experiments, which evidenced that this micropollutant is highly degradable. This
348 observation was in accordance with literature (Corvini et al., 2006; Porter et al., 2012).
349 The BPA shows the lowest R_D for aerated experiments, which was kept between 91
350 and 99 %. Whereas under non-aerated conditions BPA the removal ratio was close to
351 80 %. The OP shows the lowest removal ratio under non-aerated conditions, thus OP
352 seems to be the micropollutant more resistant to light.

353 Comparing aerated experiments, the total removal ratios obtained for OP, t-NP
354 and BPA were higher than 96 % for “PO” and “O”, whereas for “POM” the value ranged
355 from 96.1 to 98.8 %. This could be attributed to the microalgae were able to shield the
356 light, therefore the low removal ratio produced by photons was partly inactive.
357 Moreover, the micropollutants degradation under aerated conditions can be fulfilled in
358 less than 20 h.

359 **4. Conclusions**

360 The total removal ratios for OP, t-NP and BPA were higher under aerated
361 conditions than under non-aerated conditions. However, it was observed a complete
362 removal for 4-NP in all experiments. The chemical oxidation is the key variable in the
363 micropollutants removal and photodegradation was only effective on 4-NP. The
364 removal by sorption was much lower than by degradation. Therefore an aerobic step
365 should be required to remove the studied compounds from the SAnMBR effluent.
366 Further studies must be performed in order to optimise the DO concentration.
367 Moreover, the photosynthetic activity of microalgae in terms of DO supplier should be
368 assessed.

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375 coastal areas in the Comunitat Valenciana” and by the Spanish Research Foundation
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380

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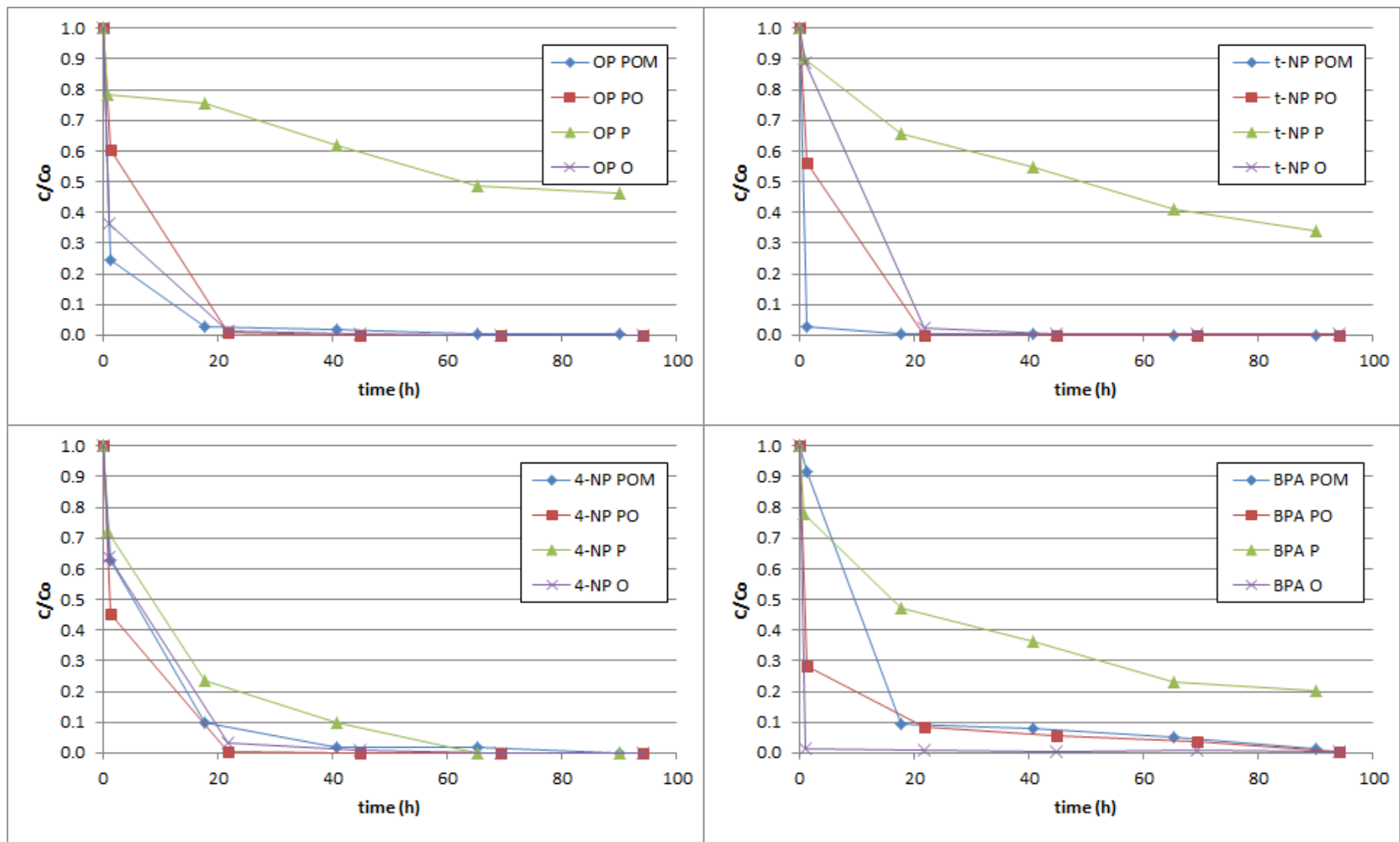
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Figure captions.

Figure 1. Effect of light, oxygen and microalgae combination; "POM" (light, oxygen and microalgae), "PO" (light and oxygen), "P" (light) and "O" (oxygen) on the micropollutants in soluble concentrations. Removal is shown through of the variation of relative micropollutants concentration with time. The initial concentrations were 3.5, 15.0, 10.0 and 10.0 µg/L for OP, t-NP, 4-NP and BPA respectively. The average exposure total time was 90 h for each experiment



518

519 Fig. 1

520

521

Tables.

522

Treatment combination	Value of variables			Code		
	O (mg O ₂ /L)	P (μE/m ² ·s)	M (cells/L)	O	P	M
POM	8.2±0.5	120	2,25·10 ¹⁰	+	+	+
PO	8.1±0.3	120	0	+	+	-
P	1.8±0.9	120	0	-	+	-
O	8.2±0.4	0	0	+	-	-
1	1.8±0.9	0	0	-	-	-

523

524

Table 1. A typical factorial design established for three variables; oxygen (O), light (P) and microalgae (M) at two levels.

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527

EDC	LOD (ng/L)	LOQ (ng/L)	$a \pm s_a$	$b \pm s_b$	r^2	Range (ng/L)	RSD(%)
OP	2	6,7	$(-18 \pm 4) \times 10^5$	$(11 \pm 5) \times 10^3$	0,990	2 - 6000	18
t-NP	25	83,3	$(-6 \pm 2) \times 10^6$	$(5 \pm 0.2) \times 10^3$	0,990	25 - 50000	18
4-NP	8	26,7	$(-8 \pm 3) \times 10^6$	$(12 \pm 0.5) \times 10^3$	0,98	5 - 10000	20
BPA	500	1666,7	$(-4 \pm 2) \times 10^5$	$(4.4 \pm 0.2) \times 10^2$	0,990	500 - 50000	16

528

529 **Table 2.** Analytical parameters obtained for micropollutants with SPME-GC-MS
530 for soluble fraction. LOD, LOQ, calibration line parameters (where “a” is y-
531 intercept and “b” is slope), correlation coefficient (r^2), linear dynamic range and
532 intra-day precision (RSD) are shown.

533

534

EDC	LOD (ng/kg)	LOQ (ng/kg)	$a \pm s_a$	$b \pm s_b$	r^2	Range (ng/kg)	RSD(%)
OP	10	33,3	$(-20 \pm 8) \times 10^5$	$(14 \pm 1) \times 10^3$	0,98	10 - 10000	12
t-NP	50	166,7	$(-6 \pm 5) \times 10^6$	$(6.4 \pm 0.5) \times 10^3$	0,96	100 - 100000	7
4-NP	20	66,7	$(-11 \pm 4) \times 10^6$	$(16.0 \pm 0.8) \times 10^3$	0,98	20 - 20000	17
BPA	1000	3333,3	$(2.6 \pm 0.9) \times 10^6$	$(7 \pm 1) \times 10^3$	0,90	1000 - 100000	11

535 **Table 3.** Analytical parameters obtained for micropollutants with SPME-GC-MS
536 for suspended fraction. LOD, LOQ, calibration line parameters (where “a” is y-
537 intercept and “b” is slope), correlation coefficient (r^2), linear dynamic range and
538 intra-day precision (RSD) are shown.

539

Set-up	Sample	Mass Flux ($\mu\text{g/d}$)			
		OP	t-NP	4-NP	BPA
POM	M _I	0.73	3.13	2.08	2.08
	M _E	0.01	0.04	0.00	0.08
	M _S	0.0076	0.0696	0.0013	0.0869
	M _D	0.71	3.02	2.08	1.92
	R _S (%)	1.05	2.23	0.06	4.17
	R _D (%)	97.75	96.47	99.90	91.89
PO	M _I	0.73	3.13	2.08	2.08
	M _E	0.00	0.00	0.00	0.00
	R _D (%)	99.98	99.98	100.00	99.82
P	M _I	0.73	3.13	2.08	2.08
	M _E	0.34	1.06	0.00	0.42
	R _D (%)	53.84	65.98	100.00	79.84
O	M _I	0.73	3.13	2.08	2.08
	M _E	0.00	0.01	0.00	0.01
	R _D (%)	99.93	99.76	100.00	99.51

541 **Table 4.** Mass flux ($\mu\text{g/d}$), sorption removal ratio (R_S) and biodegradation
542 removal ratio (R_D) of the carried out operational conditions.