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Additional Information

1 Airborne pollutant emissions from naturally ventilated buildings: proposed  
2 research directions

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5 Bjerg<sup>h</sup>, G.Q. Zhang<sup>a</sup>, S. Pedersen<sup>a</sup>, P. Kai<sup>a</sup>, K. Wang<sup>i</sup>, D. Berckmans<sup>j</sup>

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24  
25 *Key words: Naturally ventilation, emission, animal building, areal pollutants*

26  
27 **Abstract**

28 The present article describes the current research focus and the future research trends associated with  
29 investigating emissions from naturally ventilated buildings as identified at the technical session entitled  
30 “Emission from naturally ventilated buildings (Measurement, modelling, reduction and assessment)”,  
31 that was held during the International Commission of Agricultural and Biosystems Engineering  
32 (Commission Internationale du Genie Rural, CIGR) World Congress in Quebec, Canada, between the  
33 13<sup>th</sup> and 18<sup>th</sup> of June 2010.

34  
35 Current knowledge and measurement techniques can only provide reasonable estimates of emissions  
36 from naturally ventilated livestock buildings. Thus, further research and development are required. Its  
37 final goal is a point where the measurements are precise enough to validate simulation models and to  
38 obtain more consistent and accurate emission estimates. To achieve this, better synergy between  
39 mathematical modelling, physical modelling and field measurements of ventilation rates in naturally  
40 ventilated livestock buildings is required.

41  
42 The review of the research presented at the Quebec meeting identified the following intermediate goals:  
43 1. Investigate and determine error sources and measurement inaccuracies. Error analysis might be  
44 necessary to interpret results and establish research priorities.

- 45 2. Develop intelligent ventilation control systems that can handle highly fluctuating ventilation  
46 condition in naturally ventilated livestock buildings.
- 47 3. Develop practical field methods that can be used as reference standards.
- 48 4. Establish a dedicated facility that could be used to obtain precise reference measurements of  
49 ventilation rates in naturally ventilated building. To enable this, a parallel development of new  
50 technologies (instrumentation and methodology) is required.

51

## 52 1. Introduction

53 Environmental impact of ammonia (NH<sub>3</sub>) and greenhouse gases (GHG) as well as odour and aerosol  
54 emissions from livestock buildings has been identified as important issues in the last decades.  
55 Considerable efforts, (mainly on NH<sub>3</sub> emission) have been extended to (1) understand the mechanisms  
56 of emission, (2) to solve problems associated with measurement accuracy and (3) to reduce emissions.  
57 Despite all these efforts; there are still challenges and problems associated with measuring emissions  
58 from naturally ventilated (NV) buildings that agricultural engineers and scientists have to solve. NV  
59 livestock buildings need to have large openings to obtain required ventilation rates. Consequently, the  
60 difference between inside and outside air pressure is extremely small, i.e. often 1 Pa or lower, and  
61 outdoor wind direction and speed plays the main role for the air exchange in the building. This results  
62 in rapidly fluctuating airflow, changing air inlet and outlet locations and non-homogeneous pollutant  
63 distribution. Our knowledge about these dynamic conditions for airflow and pollutant emission is not at  
64 the level, where we can measure ventilation rates and pollutant/gas concentrations precise enough to  
65 validate simulation models and obtain consistent and accurate emission estimates.

66

67 With this background in mind, a technical session entitled “Emission from naturally ventilated  
68 buildings (Measurement, modelling, reduction and assessment)” was included in the World Congress  
69 of International Commission of Agricultural and Biosystems Engineering (CIGR) in Quebec on 13 -18  
70 June 2010. Agricultural engineers and scientists from all over the world gathered and discussed the  
71 latest achievements in order to identify future research opportunities. Participating scientists agreed to  
72 work together to publish this present Special Issue “Emissions from naturally ventilated livestock  
73 buildings” to clarify the important aspect of emission measurement from NV livestock buildings.

74

75 This article aims at describing the current research focus and the future research challenges associated  
76 with investigations of emissions from NV livestock buildings as identified at the Quebec meeting. For  
77 facilitating the interpretation, some of the research topics are cross referenced to the papers included in  
78 the conference proceedings and in this present Special Issue, where more detailed analyses and in-depth  
79 discussions can be obtained.

80

## 81 2. Overview of the Quebec meeting

82 Table 1 shows the results from categorization of the 24 presentations at the Quebec meeting. The  
83 majority of the presentations at the meeting focused on assessment methods. The main objectives of 11  
84 presentations were to evaluate/improve known assessment methods and 7 presentations aimed at  
85 development/demonstration of new assessment methods. Assessment methods and their measurement  
86 accuracy were the main focus of 14 and 13 presentations, respectively. Researchers were interested in  
87 improving assessment methods, and then especially the accuracy of ventilation rate measurements.  
88 Ventilation and /or airflow measurement in the livestock buildings was identified, as the main study  
89 object of 14 presentations. Ammonia emission was the main study objective of 13 presentations. This  
90 indicates that NH<sub>3</sub> emission is an important environmental issue in many countries. Carbon dioxide  
91 (CO<sub>2</sub>) measurement was the main study objective of 7 presentations. In most of the studies CO<sub>2</sub>  
92 concentrations were recorded in connection with the CO<sub>2</sub> mass balance method for determining

93 ventilation rates. There were only a few studies dealing with GHGs, i.e. CO<sub>2</sub>, methane (CH<sub>4</sub>) and  
94 nitrous oxide (N<sub>2</sub>O). Yet, it is no doubt that GHG emission from NV livestock buildings will have a  
95 more central role in research activities in coming years. It is expected that measurement of GHGs that  
96 are present in NV livestock buildings in very low concentrations (e.g. N<sub>2</sub>O) , will require improved  
97 knowledge and measuring methods due to uncontrolled air movements and fluctuating pollutant  
98 concentrations. It was interesting to note that at the Quebec meeting there was no study presented on  
99 odour emission from NV livestock buildings. Possibly, there are fewer incidences of odour nuisance  
100 reported in conjunction with NV livestock buildings when compared to mechanically ventilated (MV)  
101 buildings. This may mainly related with the type of animals normally raised in NV respectively MV  
102 buildings in the countries with intensive livestock farming. Many of the presentations at the meeting  
103 dealt with cattle buildings, as most cattle buildings are naturally ventilated. However, in the temperate  
104 and hot climate regions, pigs are also raised in NV livestock buildings. Therefore, emissions and odour  
105 nuisance from NV pig buildings are as important as emissions from cattle buildings in these parts of the  
106 world.

107

### 108 3. Measurement accuracy

109 Placement of measurement points in relation to measurement accuracy was one of the main subjects at  
110 the Quebec meeting. By using a scaled open type dairy building model in a wind tunnel, Ikeguchi and  
111 Moriyama (2010) studied the tracer gas method for determination of the air exchange rates. The study  
112 demonstrated that (1) the locations of gas sampling in relation to the gas injection points and (2)  
113 airflows in the building have crucial effects on the measurement accuracy when the constant emission  
114 method was applied. The reported magnitude of the error was large. In fact, tracer gas methods have a  
115 crucial weakness because these methods assume that the air and the tracer gases mix perfectly in the  
116 ventilated airspace albeit a perfect mixing can only be obtained under an ideal condition. In addition, it  
117 is also assumed that the measurement points represent the average ventilation efficiency or gas  
118 emission within the ventilated airspace. With this in mind, Özcan and Berkman (2010) studied  
119 measurement errors due to sampling positions by comparing the tracer gas method with a more precise  
120 measurement of the ventilation rate in a laboratory test installation. The experiments demonstrated that  
121 the measurement errors can be as high as 86% of the actual ventilation rate. By reviewing CO<sub>2</sub>  
122 production models and analyzing the results from field measurements, Zhang, Pedersen and Kai (2010)  
123 found that the potential error due to incorrect sensor placement increases progressively with the size of  
124 wall and roof openings and it can be the major error source in open buildings with high ventilation rates.  
125 The effect of the sensor placement on measurement accuracy is also influenced by the timing and the  
126 duration of the measurement due to the varying activity level over time and at different life stages of  
127 the animals.

128

129 Another error source for CO<sub>2</sub> mass balance method is the imprecise knowledge of CO<sub>2</sub> production in  
130 the buildings. The total CO<sub>2</sub> production includes CO<sub>2</sub> produced by the animals and CO<sub>2</sub> emitted from the  
131 manure. It is influenced by many factors such as feeding level, nutrient composition, animal activity  
132 and manure handling methods. It also varies diurnally, seasonally and over different growing stages.

133

134 The lack of a reliable reference method is the main reason for these error sources and their effects on  
135 the reliability of emission measurements in NV livestock buildings are not fully understood. Although  
136 establishment of a facility that provides reference measurements of ventilation rates in NV livestock  
137 building appears to be an elusive goal today; it is still highly desired. It would improve the ability of  
138 researchers to investigate and determine error sources and underlying mechanisms for measurement  
139 inaccuracies. Also more in-depth studies of the nature and contributions of individual errors sources to  
140 the overall measurement inaccuracy are necessary. The knowledge that might be generated by such  
141 research efforts would be an essential tool for development and selection of proper measurement  
142 techniques with higher accuracy at reasonable costs. The cost aspect is important as the measurement

143 technique selected will only be used universally, if it can be obtained cost effectively. More detailed  
144 analyses and in-depth discussions on the origin and magnitude of errors are given by Calvet et al.  
145 (2012). Ogink et al. (2012) suggested to develop a practical field method that can be used as a 'reliable  
146 standard' reference. They found that improvements in tracer gas ratio methods might lead to a widely  
147 applicable reference method.

#### 148 149 4. Methods to determine ventilation rates

##### 150 4.1 CO<sub>2</sub> mass balance method

151 Reliability of the data on CO<sub>2</sub> production in the buildings and CO<sub>2</sub> concentration differences ( $\Delta\text{CO}_2$ )  
152 between inside and outside of the building was an issue discussed at the Quebec meeting. Zhang,  
153 Pedersen and Kai (2010) reviewed the CO<sub>2</sub> production models and analyzed the results from field  
154 measurements of five dairy cattle buildings in order to estimate the feasibility of applying CO<sub>2</sub> production  
155 models for determination of the ventilation rates in NV livestock buildings. In animal buildings where the  
156 manure is not stored in the building for a long period, the CO<sub>2</sub> production from the manure handling system  
157 is small compared to the CO<sub>2</sub> production from animals. However, in animal buildings with deep litter (i.e.  
158 animal buildings where the depth of the litter is more than 0.5m), the CO<sub>2</sub> production from the litter can  
159 be significant. Because of this, it is difficult to estimate the ventilation rate in buildings with deep litter.  
160 They also noticed that the animal CO<sub>2</sub> production varies diurnally about  $\pm 20\%$  due to animal activity.  
161 However, they also found that the diurnal variation in CO<sub>2</sub> production is of minor importance in open  
162 animal buildings with high ventilation rates. This is because the dominating error is caused by the  
163 difficulty of acquiring reliable CO<sub>2</sub> concentration measurements due to fluctuating airflow in such  
164 buildings. Calvet et.al. (2010) reported that a correction of ventilation rates for animal activity for CO<sub>2</sub>  
165 production was necessary to determine effects of dark and light photo period on the ventilation rates in  
166 MV buildings for broilers.

##### 167 168 4.2 Tracer gas method

169 The tracer gas method enables measurement of ventilation rates in occupied buildings under real  
170 conditions. Use of the tracer gas method may facilitate an accurate estimation of ventilation rates since  
171 it takes into account the effect of occupancy and other conditions under actual field conditions, (such as  
172 the effects of structural components of the buildings, e.g. open doors and windows). SF<sub>6</sub> is a widely  
173 used tracer gas; but it is also a very potent GHG. Also Krypton85 is used as tracer gas although it has a  
174 human health hazard potential. This is due to the sensitivity of the detection method that allows the  
175 determinations of very high ventilation rates. Kiwan et al. (2010 and 2012) applied the method for  
176 determination of the air exchange rates in two NV buildings for dairy cattle. They compared it with the  
177 CO<sub>2</sub> mass balance method and with calculations based on a natural ventilation theory called discharge  
178 coefficient method. They found that the Krypton85 method is an appropriate technique to be used on  
179 farms; but further development is required. It deals with optimization of sensor location/distribution  
180 and mixing of tracer gas and air. The method is relatively unexploited compared with the CO<sub>2</sub> mass  
181 balance method. Nevertheless, it may gain more attentions as isotope measurement enables a high  
182 number of measuring points and delivers accurate concentration data with high spatial and time  
183 resolution.

##### 184 185 4.3 Direct measurement

186 Kiwan et al. (2010) installed 24 impeller anemometers in two NV dairy buildings along the side wall  
187 facing the dominant wind direction (upwind side) to measure the horizontal air velocity through the  
188 openings. They emphasized that the selection of measuring locations is a crucial factor for accurate  
189 measurements as it must ensure a sufficient accuracy in all expected openings of the curtain-wall.

190  
191 Simultaneous monitoring of airflow and gas concentration at carefully selected multiple locations may  
192 provide better emission estimates than what is achieved today. However, non-homogeneous and

193 fluctuating gas distribution and airflow put demands on the number of measurement locations,  
194 measurement frequencies and measurement periods. Practical measurement methods that can achieve  
195 all this cost effectively need to be developed. Wireless sensor networks with spatially distributed  
196 autonomous devices to sample gas concentrations and airflow data, maybe a candidate technology.  
197

198 Ultrasonic anemometers that provide high frequency measurements of 3D air velocities are robust and  
199 easy-to-use instruments to monitor fluctuating airflow in relatively challenging and aggressive  
200 environments like animal buildings. They provide turbulent characteristic data indicating the airflow  
201 pattern around the measurement points. Multi point 3D ultrasonic anemometers are readily available..  
202 By using such instruments, Fiedler et al. (2012) determined air velocities and turbulence characteristics  
203 in two NV buildings for dairy cattle to reveal effects of outside boundary conditions (approaching wind  
204 direction and velocity as well as obstructions due to other buildings) on inside airflow.  
205

#### 206 4.4 Imitation of naturally ventilated livestock building (NVB) with mechanically ventilated 207 building (MVB)

208 In a turkey grow-out building, Jacobson, Hetchler and Noll (2010) demonstrated a method to determine  
209 ventilation rates (on a per animal basis) in a NVB. The method is based on the assumption that NVB  
210 and MVB were similar to each other in all aspects except regarding ventilation principles will produce  
211 similar relationships between CO<sub>2</sub> concentrations and ventilation rates per animal basis. The procedure  
212 of the determination of the ventilation rate in NVB was as follows: CO<sub>2</sub> concentration differences  
213 between outside and inside of the MVB and the NVB ( $\Delta\text{CO}_{2\text{M}}$  and  $\Delta\text{CO}_{2\text{N}}$ ) were measured  
214 continuously along with the ventilation rate ( $\text{VR}_{\text{M}}$ ) in MVB. Then, ventilation rates ( $\text{VR}_{\text{N}}$ ) in the NVB  
215 were determined by multiplying the ratio  $\Delta\text{CO}_{2\text{M}}/\Delta\text{CO}_{2\text{N}}$  with the ventilation rate  $\text{VR}_{\text{M}}$  measured in  
216 the MVB. This is essentially a modified CO<sub>2</sub> mass balance approach. It relies on the same assumption  
217 regarding homogeneity of CO<sub>2</sub> in the room and placement of the measurement points as the CO<sub>2</sub> mass  
218 balance method. It has, therefore, the same weakness. However, the utilization of  $\Delta\text{CO}_{2\text{M}}/\Delta\text{CO}_{2\text{N}}$  and  
219  $\text{VR}_{\text{M}}$  that were determined in real animal buildings permits estimations based on near real conditions.  
220 This is probably the strength of the method compared with the ordinary CO<sub>2</sub> mass balance method,  
221 which uses prediction equations (for CO<sub>2</sub> and heat production) derived basically from laboratory  
222 experiments, which could differ significantly from actual farm conditions.  
223

#### 224 5. Methods to determine gas emission rate

225 Hassouna et al. (2010) proposed a new method of determining gas emission rates from cattle buildings.  
226 The study used gas-concentration gradients and mass-balance deficits of carbon which were estimated  
227 on the basis of livestock-related data (e.g., feeds, production, effluents) as well as intermittent  
228 measurements of outdoor and indoor gas concentrations (water, H<sub>2</sub>O, CO<sub>2</sub>, NH<sub>3</sub>, CH<sub>4</sub>, and N<sub>2</sub>O),  
229 temperature and relative humidity. The method was validated with water-budget observations and  
230 simulation model predictions of CH<sub>4</sub> and CO<sub>2</sub> emissions exclusively from animals. For the studied  
231 buildings with slurry evacuated twice a day, a good agreement was found between CO<sub>2</sub> and CH<sub>4</sub>  
232 emissions estimated with the new method and those predicted by the simulation model. Whereas for the  
233 deep litter cattle buildings, it was observed that the emissions of CH<sub>4</sub> and CO<sub>2</sub> were higher than the  
234 emissions predicted by the simulation models.  
235

236 The tracer gas ratio method, which is widely used to measure emissions from NV livestock buildings,  
237 relies on the assumption that the ratio between the emission rates of the pollutant and the tracer gas is  
238 equal to the ratio between the pollutant and tracer gas concentrations (Ogink et al., 2012). Schrade et al.  
239 (2010a; 2010b) applied the method with two different tracer gasses, (SF<sub>6</sub> and SF<sub>5</sub>CF<sub>3</sub>) in order to  
240 determine ammonia emissions from two different sources, i.e. a NV dairy building and the  
241 neighbouring outdoor exercise area. A photo acoustic sensor for NH<sub>3</sub> quantification and a recently  
242 developed GC-ECD method, which simultaneously quantifies the tracer gasses, were used. The diluted

243 tracer gases were continuously injected directly above the emitting areas via tube systems with 46  
244 critical capillaries, thereby mimicking the source of the NH<sub>3</sub> emissions. An air-collection system at a  
245 height of 3 m consisting of a Teflon hose and 39 glass critical capillaries 3 m apart was used for  
246 sampling of the tracer gases and NH<sub>3</sub>. A set of relevant descriptive data such as weather conditions,  
247 climate in the building and at the outdoor exercise area, animals' area usage, aisle/exercise-area, soiling  
248 and nitrogen balance, were used to characterise measurement conditions. The method demonstrated its  
249 ability to quantify seasonal effects and variations between individual farms.

250  
251 Reliable and robust sensors, which can provide high frequency concentration measurement of relevant  
252 gasses (e.g. NH<sub>3</sub>, GHGs, odorous compounds, SF<sub>6</sub>,) have to be developed and used in the livestock  
253 buildings for multi-location measurement of gas concentrations.

## 254 255 6. Modelling of gas emission

256 Modelling of gas emission involves studies on (1) pollutant production in the substrate (manure etc),  
257 (2) transfer from the liquid to the gas phase (3) transfer through the boundary layer (4) mixing inside  
258 the building envelope and (5) transport to the wider environment. Hassouna et al. (2010) and Schrade et  
259 al. (2010) presented studies on modelling of pollutant production. Wu, Kai and Zhang (2010)  
260 determined NH<sub>3</sub> concentrations and air velocities around simulated manure surfaces in a wind tunnel in  
261 order to get fundamental understanding on the nature of the NH<sub>3</sub> evaporation from manure, i.e. gas  
262 emission and transportation within and near the boundary layer. A review study of Bjerg et al. (2012a)  
263 presented in this Special Issue deals with ammonia release modelling. For the modelling of gas mixing  
264 inside the building envelope, researchers are working with two model categories: 1) CFD  
265 (Computational Fluid Dynamic) models (Bjerg and Andersen, 2010 and Choi et. al. 2010; Bjerg et al.  
266 2012c), which require detailed geometrical modelling and 2) lumped models, which are faster to use  
267 and have greater potential to simulate the influences of weather conditions (Liberati and Zappavigna,  
268 2010; Bjerg et al. 2012b). Lumped model simplifies the description of the airflow and approximate its  
269 behaviour under certain assumptions. It requires less geometrical details and computational time. These  
270 models might be applied to aid design of low emission buildings and to design intelligent online  
271 ventilation and emission control systems in NV livestock buildings. However, there are still substantial  
272 challenges related to generating experimental data for the development and validation of the models  
273 (Bjerg et al. 2012a, b, c). Ultimately, a set of models or a comprehensive simulation model, which can  
274 handle all processes, (i.e. from pollutant production in the substrate to the wider environment) is  
275 needed.

276  
277 Youssef et al. (2010) demonstrated the usefulness of model-based procedures for the determination of  
278 NH<sub>3</sub> emission from manure storage. The model was developed based on the knowledge that NH<sub>3</sub>  
279 emission is strongly related to some easily measurable variables such as near manure surface air  
280 temperature and manure surface temperature. This method allows a continuous modelling of the NH<sub>3</sub>  
281 emission rates. They found that a steady-state regression model was good enough for calculation of the  
282 cumulative NH<sub>3</sub> emission over the whole measuring period.

283  
284 Determining proper measurement locations requires good knowledge about airflows in the buildings.  
285 To obtain such knowledge, CFD modelling may be useful. Validation of the model can probably be  
286 done by using the data obtained by multi-position instrumentation of 3D ultrasonic anemometers.

287  
288 Modelling is a cost effective method of obtaining knowledge about the performance of new technical  
289 solutions developed for emission reduction. Thus, many researchers invested efforts in model  
290 development. An important aspect of this work is the validation of the models, which is normally done  
291 by comparing the results obtained from the model with the experimental measurements. This means  
292 that no model, in principle, can be more accurate than the validation measurements. Unfortunately, as

293 mentioned before, the current techniques used in the experimental studies can only provide reasonable  
294 estimates of emissions.

295

#### 296 7. Flux chamber

297 Use of flux chambers for determination of pollutant emission from surfaces, e.g. floors and manure  
298 pits, appears to be a useful method for evaluation of abatement technologies. Mosquera et al. (2010)  
299 investigated characteristics of flux chamber measurements and studied spatial and temporal variation of  
300 floor surface emissions. For a good estimation of the NH<sub>3</sub> emissions from floors, they recommend to  
301 measure NH<sub>3</sub> emission at different floor sections throughout a number of days and under different  
302 weather conditions. Studies of Wheeler et al. (2010) aimed at comparing NH<sub>3</sub> emissions from dairy  
303 manure as a whole-room mass balance calculation versus emission measurements performed within the  
304 room using portable flux chambers. Steady-state flux and non-steady-state recirculation flux chambers  
305 were used. The later was shown to be provide more accurate estimates by measuring 90 to 119% of  
306 ammonia emissions of the whole room's mass balance calculations. The steady-state flux chamber  
307 method, although universally recognized in USA for emission evaluations, demonstrated strong  
308 tendencies for underestimations. The flux chambers can potentially be used to also determine emissions  
309 of pollutants other than NH<sub>3</sub>. Yet, at the Quebec meeting, there was no study involving measurements  
310 of other pollutants, e.g. CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub>O and particulate. A more detailed review of flux chamber  
311 methods is given in this Special Issue by Ogink et al. (2012).

312

#### 313 8. Abatement methods

314 By a laboratory experiment Wu, Kai and Zhang (2010) demonstrated the possibility of using pit  
315 exhaust in pollutant abatement: The most polluted air is drawn through pit exhaust and purified before  
316 it is released to the outside. According to their estimation; 70-80% of the NH<sub>3</sub> emission can be reduced  
317 by a pit exhaust rate of about 10% of the total ventilation rate. Van Dooren and Mosquera (2010)  
318 investigated the potential effects of two emission reduction principles: (1) Reducing floor emission by  
319 using a fast removal of urine and a separate removal of faeces by scrapers and (2) Reducing pit  
320 emissions by covering the slurry in the pit. They used the flux chamber method to estimate the effects  
321 and found more promising prospects with the first principle, i.e. reducing floor emission. Rets et al.  
322 (2010) cut concrete slatted floor elements out of the existing floor and brought them into closed  
323 chambers to measure NH<sub>3</sub> emission from the floor elements. The study was aimed at investigating the  
324 impact of the manure removal from the slatted floor. A special cleaning device, designed to combine  
325 the advantages of a wet, mechanical cleaning-method was used. It featured high-pressure water  
326 nozzles, mechanical star-discharge-rotors and a rubber-scraper. However, no significant effect on the  
327 NH<sub>3</sub> emission was detected by cleaning of the slats. In CFD modelling Bjerg and Andersen (2010)  
328 demonstrated a potential reduction of ammonia emissions from NV livestock building by adjusting the  
329 size of ventilation opening according to outdoor wind conditions in order to avoid over ventilation and  
330 consequently increase ammonia emission in windy periods. In addition the work demonstrated that a  
331 significant further reduction can be obtained by cleaning a minor airstream expelled mechanically from  
332 the pit beneath the slatted floor.

333

#### 334 9. Conclusions/ Future research directions

335 Current knowledge and measurement techniques can only provide reasonable estimates of emissions  
336 from NV livestock buildings. Further research and development are required to develop measurements  
337 that are precise enough to validate simulation models and to obtain more consistent and accurate  
338 emission estimates. To achieve this better synergy between mathematical modelling, physical  
339 modelling and field measurements of ventilation rates in NV livestock buildings is required.

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341 The review of the research presented at the Quebec meeting identified the following intermediate  
342 research and development goals:



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1. Investigate and determine error sources and measurement inaccuracies. Error analysis might be necessary to interpret results and establish research priorities.
2. Develop intelligent ventilation control systems that can handle highly fluctuating ventilation condition in NV livestock buildings.
3. Develop practical field methods that can be used as reference standards.
4. Establish a dedicated facility that could provide precise reference measurements of ventilation rates in naturally ventilated buildings. To enable this, a parallel development of new technologies (instrumentation and methodology) is required.

## Reference

List of the proceedings and the abstracts presented at the technical session titled “Emission from naturally ventilated buildings (Measurement, modelling, reduction and assessment)”, Section II: Farm Buildings, Equipment, Structures and Livestock Environment Conference, XVIIth World Congress of the International Commission of Agricultural and Biosystems Engineering (CIGR)  
Available online: <https://www.bioeng.ca/publications/meetings-papers?catid=19> (Use CSBE No. to find the proceedings or abstracts)  
(The numbers in square brackets refer to the reference number shown in Table 1.)

Berg, W., Fiedler, M., Kiwan, A., & Brunsch R. (2010): Measurements of air ventilation rates in naturally ventilated dairy cattle buildings, (CSBE100762), [1]

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Table 1: Results from categorization of the 24 presentations at CIGR 2010 technical session on emission from naturally ventilated buildings.

Category group	Category	Number of presentations	Reference number <sup>a</sup>
Aims of the study	To evaluate / improve known assessment methods	11	1,2,4,6,9,11,14,15,21,22,24
	To develop / demonstrate new assessment methods	7	5,7,10,13,17,20,23
	To develop design / management tool	1	12
	To develop / evaluate abatement technology	3	2,16,19
	To determine emission rate inventory	2	9,18
Major topics	Assessment method	14	3,4,5,6,7,9,10,11,13,17,18,20,22,23
	Measurement accuracy	13	1,3,4,6,8,9,11,13,14,15,21,22,23
	Factors influencing emissions	3	9,17,18
	Building design	2	5,12
	Abatement technology	4	2,16,19,24
Major study objects	Ventilation / Airflow	14	1,2,4,6,7,8,9,10,11,14,15,20,22,24
	Internal climate	2	12,20
	NH <sub>3</sub>	13	2,3,7,8,10,13,16,17,18,19,20,21,23
	Dust	1	5
	CO <sub>2</sub>	7	1,4,6,7,8,10,22
	Other gasses (CH <sub>4</sub> , N <sub>2</sub> O)	3	3,7,8
	Microorganism	1	5
Animal species	Cattle	13	1,2,3,7,11,12,13,16,17,18,19,21,22
	Pig	6	5,8,9,12,20,23
	Poultry	2	4,10
	Rabbit	1	6
Principal methods of assessment	CO <sub>2</sub> mass balance	6	1,3,4,6,10,22
	Tracer gas method	7	1,8,9,11,14,17,18
	Direct measurements	2	11,24
	Imitate NVB with MVB <sup>b</sup>	1	10
	Modelling	5	2,5,7,12,23
	Flux chamber / element isolation	4	13,16,19,21

<sup>a</sup> Refer to the numbers in square brackets shown in the reference list.<sup>b</sup> NVB = Naturally ventilated building; MVB = Mechanically ventilated building