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Additional Information

Energy conversion from external fluctuating signals based on asymmetric nanopores

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Abstract

Electrical transduction from fluctuating external signals is central to energy conversion based on nanoscale electrochemical devices and bioelectronics interfaces. We demonstrate theoretically and experimentally a significant energy transduction from white noise signals using the electrical rectification of asymmetric nanopores in polymeric membranes immersed in aqueous electrolyte solutions. Load capacitor voltages of the order of 1 V are obtained within times of the order of 1 min by means of nanofluidic diodes which convert zero time-average potentials of amplitudes of the order of 1 V into average net currents. We consider single-nanopore and multipore membranes to show that the conversion processes can be significantly increased by scaling. The results concern a wide range of operating electrolyte concentrations. Because these concentrations dictate the pore resistance, the tuning of the load capacitance to optimize the system response at each concentration is also addressed. Finally, the experimental results are described theoretically by using simple equivalent circuits with a voltage-dependent resistance in series with a load capacitance.

KEYWORDS: nanopore, fluctuating signal, electrical rectification, energy conversion

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Introduction

The electrical transduction of fluctuating signals is central to energy conversion based on nanoscale electrochemical devices, being significant also for bioelectronics interfaces. We have demonstrated recently [1] that electrical rectification with nanofluidic diodes [2,3] allows significant energy conversion for the case of a single nanopore and large amplitude white noise signals. To this end, external electric potentials of zero average were converted into net currents, allowing an external load capacitor to reach a voltage of the order of 1 V in a time of the order of 1 min [1]. This fact clearly suggests that soft matter nanostructures operating in an aqueous ionic solution can effectively be coupled to conventional electronic elements like commercial capacitors. Because of the biomimetic nature of the pore, the results have clear implications for sensing and information processing using bioelectronic interfaces and nanopore-based biosensors [4-11]. We note in this context that the artificial nanopore used here shows electrical rectification and ionic selectivity characteristics similar to those observed in wide ion channels (e.g., the bacterial porin *OmpF* of *Escherichia coli*, a protein pore reconstituted on a planar lipid bilayer [12,13]).

We present here a significant extension of the above results concerning these biomimetic nanomaterials [1,12], paying attention to the energy conversion processes. First, we use both single-nanopore and multipore membranes in an effort to demonstrate that the conversion processes are robust and can be enhanced significantly by simple scaling. Second, we consider a wide range of electrolyte concentrations to better simulate real operating conditions. Third, we address the tuning of the load capacitance at each concentration (note that this concentration dictates the nanopore resistance). Finally, we show that the observed phenomena can be analyzed theoretically by using simple equivalent circuits with a voltage-dependent resistance in series with a load capacitance. This question should be significant to simulate the expected system response in each practical case.

Experiment and numerical methods

Nanopore. Polymer foils of polyethylene terephthalate (PET) of thickness 12 µm (Hostaphan RN 12, Hoechst) were irradiated either with single or 10⁴ swift heavy ions cm⁻² (Pb, U, and Au), with an energy of 11.4 MeV per nucleon, at the UNILAC linear accelerator (GSI, Darmstadt). A single conical pore was obtained by asymmetric track-etching methods [14,15], which give typical radii in the range 10 - 20 nm for the cone tip and 100 - 200 nm for the cone basis. The approximate pore radii can be obtained from the steady-state current (I) – potential (V_N) curve in each case, with $V_N = V_R - V_C$ (Fig. 1a and b) [14,15]. Three single pore samples were used to clearly show the electrical characteristics of the nanostructures. An additional sample was also prepared with a multipore membrane etched together with the single-pore membrane. The etching process results in carboxylic acid groups located on the pore surface. These groups are ionized in a 0.1 M KCl aqueous solution at pH = 7. Each nanopore has then a negative charge distribution along the axis, which is asymmetric because of the approximately conical pore geometry [16]. This charge asymmetry is responsible for the electrical rectification of the $I-V_N$ curve (Fig. 1b and c), which permits the transduction of white noise signal (Fig. 1d). Control experiments were also conducted at low pH (pH = 3, neutral pore [1]). Before and after each measurement, the pH was checked by using a Crison GLP22 pH-meter.

Measurements. A couple of Ag|AgCl electrodes immersed in the bathing solutions (Fig. 1a) allowed the fluctuating electric potentials to be applied. Note that the current entering the (highly charged) cone tip opening of the pore finds an electrical resistance lower than that entering the wide basis opening, which gives the observed electrical rectification. The current-voltage curves were measured with one picoammeter/voltage source (Keithley 6487/E). The voltages across the capacitor of Fig. 1a were measured with a multimeter (Keithley 2000/E). The recorded currents *I*(*t*) allowed to obtain the average currents *I*> of Fig. 2a.

Simulations. The nanopore is considered as a potential dependent resistance connected in series to the capacitor (Fig. 1a). To simulate the charging process, the electrical circuit was fed with fluctuating potential signals of amplitude V_0 . The charging process was described by the equation $dV_C(t)/dt = I(t)/C$, where $V_C(t)$ and I(t) are the capacitor potential and the current, respectively. The initial condition was $V_C(t=0)=0$ and the constant time step $\Delta t=0.05$ s, which is of the same order of magnitude as the steps in the experiments. $V_R(t)$ took random values between $-V_0$ and $+V_0$. The capacitor voltage was updated as $V_C \to V_C + I(V_N)\Delta t/C$ at each time step Δt , where $I(V_N)$ is the experimental current of Fig. 1b. The charging process eventually gave a maximum voltage $V_C(\infty)$. To describe the discharging process, we assumed the condition $V_R(t)=0$ in the simulations. The simulations were performed using a Python numerical code.

Results and Discussion

Fig. 1a shows the experimental set-up. A commercial capacitor of capacitance C is connected in series to either the single conical nanopore or the multipore membrane. The pore is immersed in two identical KCl aqueous solutions of concentration c_0 . Fig. 1b shows the steady-state current (I) – voltage (V_N) curves obtained for three single-pore membranes (samples 1–3) with different rectification characteristics (Fig. 1c). The results correspond to c_0 = 0.1 M and pH = 7, which gives an asymmetrically distributed, negative charge along the axis of the conical pore. This charge is due to the ionized carboxylate (COO $^-$) groups on the pore surface, which explains the rectification observed in the $I - V_N$ curves [2,15-17].

When a white noise, randomly fluctuating electric potential $V_R(t)$ of amplitude V_0 is externally applied in the Ag|AgCl electrodes (the *input* signal of Fig. 1d), a time (t)-dependent electric current I(t) with a non-zero time average < I > is obtained (the *output* signal of Fig. 1d).

This net current, which corresponds to sample 3 here, allows charging the load capacitor of Fig. 1a. Control experiments at low pH (not shown here) give zero net currents, $\langle I \rangle = 0$, because of the ohmic pore behavior (no rectification) [1]. These results confirm that $\langle I \rangle$ arises from the rectification of the external fluctuating signal by the asymmetric nanostructure and is not disturbed significantly by other internal noise sources of the electrical equipment [1]. Note also that the *output* electric current I(t) is slave of the *input* potential $V_R(t)$ because the period of this potential is much longer than the relaxation time characteristic of the small solution volumes found in nanopores [17-19] and ion channels [12]. This (adiabatic) limit is valid for low enough frequency signals [1,12,18-21].

Fig. 2a and b show the average currents $\langle I \rangle$ and electrical resistances R obtained for the single-pore samples 1–3, respectively. High average currents leading to significant capacitor charging are obtained for low pore resistances (Fig. 2b) and high rectifications (Fig. 1c). Fig. 2c and d show the charging and discharging curves for the three samples of Fig. 2a. In these experiments, the voltage amplitude is $V_0 = 1$ V, the load capacitance is C = 1 μ F, and the electrolyte concentration is $c_0 = 0.1$ M KCl. The saturation capacitor voltage $V_C(t \to \infty) \equiv V_C(\infty)$ obtained at long times (Fig. 2c) is determined by the rectification ratio of Fig. 1c (compare this figure with Fig. 2a for $\langle I \rangle$).

Remarkably, Fig. 2c shows that fluctuating potentials with amplitudes of the order of 1 V result in capacitor voltages of the order of 1 V within a few minutes. Note also that Fig. 2c shows the same time pattern in all charging curves because we use the same scheme for the input potential pulses (scaling the single point values to the fixed amplitude). This procedure would permit to identify other internal noise sources (wiring, capacitor, and voltage sources) in case they were present. The capacitor discharging follows an approximately exponential decay when the fluctuating external potential is disconnected (Fig. 2d). The resistance of the single pore is lower than $0.1 \text{ } G\Omega$ for most of the cases in Fig. 2b. Because the load capacitor of Fig. 1a has a

capacitance $C = 1 \mu F$ in these experiments, an equivalent RC circuit time is of the order of 10 - 100 s, which is in agreement with the experimental curves of Fig. 2c and d. In particular, the experimental charging times obtained are between 22 s (sample 3) and 82 s (sample 2).

Alternatively, the above energy conversion process can be enhanced by orders of magnitude using a multipore membrane (Fig. 3) instead of the single pore of Fig. 1 and Fig. 2. Indeed, Fig. 3a shows that steady state currents of the order of 0.1 mA can be obtained with a nanoporous membrane of approximately 10^4 conical pores/cm² at different electrolyte concentrations (the measured currents were of the order of 10 nA only in Fig. 1b). Also, the high capacitance C = 10 mF used in Fig. 3d allows collecting approximately 10 000 times the charge stored with the single pore (note that C = 1 μ F in Fig. 2c) for the same capacitor voltage. Although the energy conversion can be enhanced further by simple scaling, this enhancement cannot be maintained indefinitely. It has been experimentally demonstrated [22] that membrane samples with high pore densities ($\approx 10^6$ conical pores/cm²) obtained by track-etching display very low rectification ratios. This is due to the overlapping of adjacent pores that merge into each other, giving place to wide pores where the fixed charge effects are screened by the mobile ions. As a result, the membrane sample shows an almost linear current-voltage curve that would lead in our case to negligible capacitor charging [1].

The effect of the electrolyte concentration c_0 on the steady-state $I-V_N$ curve and electrical rectification of a multipore membrane is also shown in Fig. 3a and b. The increase of c_0 leads to an increase in the number of electrical carriers (ions here), and then to high currents (Fig. 3a). However, this effect gives low rectification ratios for high enough values of c_0 (Fig. 3b; a maximum rectification is achieved at $c_0 = 0.05 - 0.1$ M, as previously reported for single pore membranes [16]). It is well-known that the nanopore selectivity and rectification characteristics can be optimized at intermediate electrolyte concentrations [16,17] because these concentrations

are high enough for the absolute currents to be significant but low enough for electrical rectification to be significant [16].

Also, Fig. 3c shows that the membrane electrical resistance R decreases by a factor 10 when increasing the concentration c_0 from 0.01 M to 1 M. This experimental fact significantly modifies the electrical characteristics of the equivalent circuit in Fig. 1a, making it necessary to tune the capacitance C as a function of c_0 in order to obtain robust charging curves using the white noise signal (see Fig. 3d, obtained for a fixed capacitance C = 10 mF).

Fig. 4a shows the capacitance tuning effect for a multipore membrane and the load capacitances C=1 and 10 mF ($c_0=0.1$ M KCl and $V_0=2$ V here). For low values of C, the charging curve shows high noise and then the saturation capacitor voltage $V_C(\infty)$ is not well defined. A high value of C can solve this problem at the price of long charging and discharging times (Fig. 4a and b). Note also that $V_C(\infty)$ is dictated by the electrical rectification, not by the capacitance. The theoretical simulations for the charging (Fig. 4a) and discharging (Fig. 4b) curves reproduce the experimental trends.

Figs. 5a and b show the charging and discharging curves obtained using the multipore membrane for different voltage amplitudes V_0 , with C = 10 mF and $c_0 = 0.1$ M KCl. The capacitor saturation voltages $V_C(\infty)$ increase with the amplitude V_0 of the input signals and are achieved when the reverse current which opposes the charging process becomes equal to the net charging current [1]. Again, we use the same time pattern scheme for the input potential pulses as in Fig. 2c, scaling the single point values to the fixed amplitude. The theoretical charging (Fig. 4a) and discharging (Fig. 4b) curves reproduce the experimental trends. Note that $V_C(\infty)$ depends linearly on the white noise amplitude V_0 (Fig. 5a), which is correctly described by the theoretical simulations.

Figs. 6a shows the energy $E = CV_C(\infty)^2/2$ stored in the load capacitor as a function of the concentration c_0 at $V_0 = 2$ V. Fig. 6b shows this energy as a function of the voltage amplitude V_0 at $c_0 = 0.1$ M. This energy is of the order of 1 mJ for a noise amplitude of 1 V and C = 10 mF. The maximum of E achieved at intermediate values of the electrolyte concentration c_0 (Fig. 6a) is given by the maximum of $V_C(\infty)$, which is dictated in turn by the maximum electrical rectification observed in Fig. 3b. Note also that E depends on V_0^2 in Fig. 6b because of the linear dependence between $V_C(\infty)$ and the noise amplitude V_0 in Fig. 5a.

Finally, the energy stored in the load capacitor (Fig. 6a and b) can be compared with the *input* energy $E_{in} = \int_0^T I(t)V_R(t)dt$. To obtain the latter energy, we assume an effective time $T = 3\tau_{ch}$ for the limiting value of the voltage capacitor [1], where τ_{ch} is the charging time. From the experimental time traces obtained for the multipore membrane, the *output* energy is between 1.7% ($V_0 = 0.5 \text{ V}$) and 11% ($V_0 = 3 \text{ V}$) of the *input* energy. Additional experiments with single pore and multipore membranes submitted to other zero-average, periodically fluctuating potentials (square wave, sinusoidal, and triangular input signals) were also carried out, giving experimental efficiencies in the range 1 - 10 %. These values are relatively large because of the high amplitude of the input signals used. Maximum energy conversion efficiencies of the order of 1 % [23] and up to 10 % [24] have been theoretically predicted with electro-osmotic flow processes based on negatively charged conical nanopores.

Note that the above energy conversion processes are based on nanodevices integrated in small area membrane samples. In particular, practical energy harvesting aspects and long term storage have not been addressed. Simple order of magnitude estimations show that much higher membrane areas than that used here (less than 1 cm²) would be necessary for charging a small battery within reasonable times. Therefore, we expect our results to be useful only for small-

scale energy transduction processes in nanopore-based sensors and bioelectronics interfaces immersed in electrolyte solutions.

Conclusions

We have shown theoretically and experimentally that significant energy conversion from external fluctuating signals (white noise) can be achieved using the electrical rectification of nanofluidic diodes. In particular, load capacitor voltages of the order of 1 V can be obtained in times of the order of 1 min with asymmetric single-nanopore and multipore membranes which convert zero time-average potentials of amplitudes of the order of 1 V into average net currents. We have used these membranes to demonstrate that the process is robust and can be enhanced significantly by simple scaling.

We have considered different electrolyte concentrations and operating conditions, addressing also the tuning of the load capacitance at each concentration (pore resistance). The experimental results suggest that soft matter nanostructures can be electrically coupled to conventional electronic elements, which is an essential characteristic for energy transduction in sensing nanopores and biological interfaces [4,12]. The experimental results can be described theoretically by using simple equivalent circuits with a voltage-dependent resistance in series with a load capacitance.

We note finally that the *input* signal amplitudes could be decreased to 0.1 V only for relatively thin, wide pore biological ion channels such as the *OmpF* porin of *Escherichia coli* bacteria [12] at the price of decreased physico-chemical robustness. Note also that these small pores should allow the use of external signals with higher frequencies than those employed here for our artificial biomimetic nanomaterials [21]. Additional work concerning this question is now in progress.

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Figure captions

Fig. 1

(a) Scheme of the experimental set-up. (b) the steady-state current (I)-voltage (V_N) curves for three different samples of a membrane with a single conical pore. (c) the single pore electrical rectification as a function of V_N . (d) fluctuating electric potential V(t) (white noise) of amplitude V_0 obtained from an external voltage source (input) and instantaneous electric current I(t) (output) for sample 3.

Fig. 2

(a) The average current $\langle I \rangle$ as a function of the voltage amplitude V_0 for the three samples of Fig. 1. (b) the electrical resistance $R = V_N/I$ as a function of the voltage V_N . (c) the net current $\langle I \rangle$ is used to charge the load capacitor in the circuit of Fig. 1 to voltages V_C for $V_0 = 1$ V. (d) the capacitor discharging curves corresponding to the charging curves of (c). The load capacitance C = 1 µF and the electrolyte concentration $c_0 = 0.1$ M KCl in these experiments.

Fig. 3

(a) The steady-state $I-V_N$ curves of a multipore membrane. (b) the membrane electrical rectification as a function of c_0 . (c) the electrical resistances R as a function of V_N . (d) the capacitor charging curves for the white noise fluctuating signal. All experimental curves have been obtained at salt concentrations c_0 between 0.01 and 1 M KCl.

Fig. 4

Experimental (points) and theoretical (continuous lines) capacitor charging (a) and discharging (b) curves for the multipore membrane and the load capacitances C = 1 and 10 mF. The electrolyte concentration $c_0 = 0.1$ M and the voltage amplitude $V_0 = 2$ V.

Fig. 5

Experimental (points) and theoretical (continuous lines) capacitor charging (a) and discharging (b) curves obtained using the multipore membrane instead of the single pore membrane in Fig. 1a for different voltage amplitudes V_0 . The load capacitance C = 10 mF and the electrolyte concentration $c_0 = 0.1$ M in these experiments.

Fig. 6

The energy E stored in the load capacitor as a function of the concentration c_0 at $V_0 = 2$ V (a) and the voltage amplitude V_0 at $c_0 = 0.1$ M (b). In the two cases, C = 10 mF.

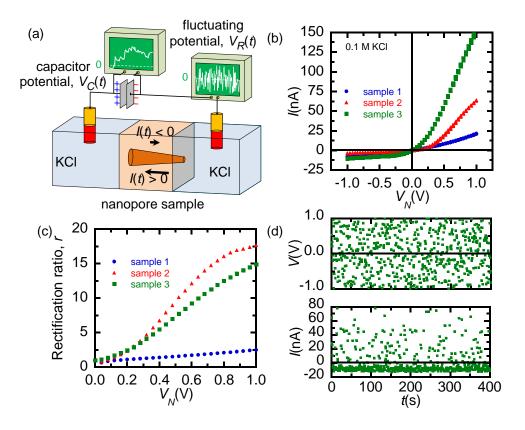


Fig. 1

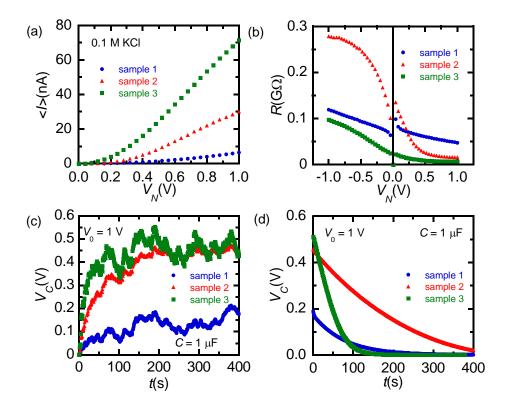


Fig. 2

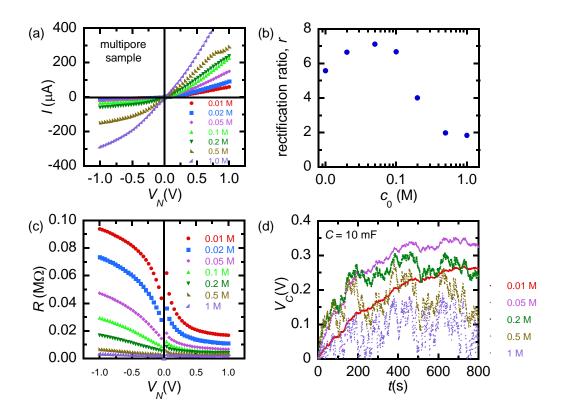


Fig. 3

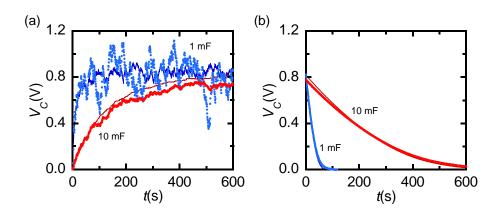


Fig. 4

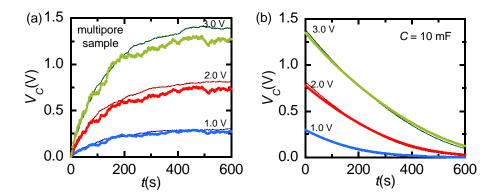


Fig. 5

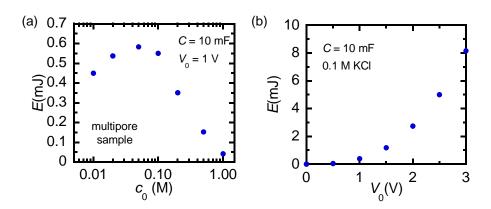


Fig. 6