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Milkability and milking efficiency improvement in Murciano-Granadina breed goats

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## ABSTRACT

21 The aim of this study was to verify the effect of cluster, udder characteristics and milking  
22 parameters on milkability and milking efficiency of Murciano-Granadina breed goats, in  
23 order to improve them. The cluster used is well adapted to the goats, except that the teat-floor  
24 distance is too short for the teat-cup used and the cluster rests on the platform instead of  
25 hanging from the udder, something apparently attributed to a poor udder conformation rather  
26 than an excessively long teat-cup. Udder parameters studied are classified as medium or  
27 medium-high by the Murciano-Granadina breed association, and do not seem to represent a  
28 problem for good milkability except for the teat sphincter strength, which reduced milk flows  
29 ( $P<0.001$ ) and increased milking times ( $P<0.001$ ). Maintaining 60% as pulsator ratio, a  
30 combination 42 kPa:120 ppm (vacuum level : pulsator rate) milking parameters reduced total  
31 milking time by 22 s per goat compared to 40 kPa:90 ppm, commonly used in this flock, but  
32 increased teat thickness measured before and after milking. Studies of longer duration are  
33 needed to ensure that the new milking parameters do not affect the udder health status.

34

35 **Keywords:** machine milking, milking efficiency, goat.

36

## INTRODUCTION

37 There is evidence (N. Fernández, unpublished data) that in some herds, including the one  
38 used in this experiment, the average milking time of Murciano-Granadina goats drops from  
39 about 5 to around 3 min as the lactation curve evolves, representing a mean milk flow  
40 between 600 and 700 mL/min, which is considered to be improved without harming the milk  
41 fractioning during milking or the health status of the udder. These flows are much lower than  
42 the 939 mL/min observed by Le Du and Benmederbel (1984), despite needing 35 kPa

43 average vacuum to open the teat sphincter in Saanen goats, suggesting some kind of problem  
44 that could result in low milkability and milking efficiency of those herds. Some of the  
45 parameters that determine milkability (Labussière, 1984) are milk fractioning and milk flows  
46 during milking. One of the usual ways of assessing milkability is through milk emission  
47 kinetics (Peris et al., 2010), as it gives milk fractioning during milking, the latency, the  
48 maximum and average milk flow and the total milking time, among other possible data. For  
49 milk fractioning interpretation when using a routine with machine stripping, the higher the  
50 percentage of the machine milking milk fraction and the lower the percentage of machine  
51 stripping milk fraction, the greater is the ability for milking (Labussière, 1984). A high milk  
52 flow is also positive for good milkability because it improves milking efficiency. Milk flow  
53 during milking may be affected by udder morphology characteristics (Marnet et al., 2000),  
54 especially teat sphincter strength (Marnet et al., 2001), or the features of the cluster used,  
55 especially by the mouthpiece lip flexibility (Fernández et al., 1997). In addition, the variation  
56 of the possible combinations among the operating parameters of machine milking (vacuum  
57 level, pulsator rate and pulsator ratio) can also affect milk flows and milk fractioning  
58 (Fernández et al., 1999). The aim of this study was to test the relationships among udder and  
59 cluster characteristics and milking parameters, as variables, in order to improve milkability  
60 and milking efficiency in Murciano-Granadina goats, using milk emission kinetics as  
61 assessment methodology.

## 62 **MATERIALS AND METHODS**

63 Housing and handling of the experimental animals followed the mandatory principles for care  
64 and use experimental animals in Spain (Real Decreto 1201/2005, Boletín Oficial del Estado  
65 252: 34367-34291).

66

## 67 **Goats and General Procedures**

68 Forty multiparous ( $3\pm 0.4$  years) Murciano-Granadina breed goats ( $45\pm 2$  kg) were used at the  
69 experimental farm of the Universitat Politècnica de València (Spain). Mating was  
70 synchronized by intravaginal sponges (30 mg fluorogestone acetate and 450 IU PMSG;  
71 Chrono-gest, CEVA Salud Animal, Intervet, Salamanca, Spain) and all births took place over  
72 a 14-d period. At parturition, goats were assigned to an artificial rearing system, similar to  
73 McKusick et al. (2001), where kids were separated from their dams at kidding, fed of  
74 colostrum then artificially reared in straw-bedded pens (size =  $0.3\text{ m}^2/\text{kid}$ ; 2 bowl water  
75 troughs) from birth and goats were milked once-a-day until 36 wk of lactation. All goats  
76 received the same total mixed ration twice daily (at 0900 and 1800 h) and were kept together  
77 in the same pen (size =  $1.5\text{ m}^2/\text{goat}$ ; feeder =  $0.5\text{ m}/\text{goat}$ ; 5 bowl water troughs). The ration  
78 was formulated according to Sauviant et al. (2007) and consisted of: 1) a basal diet to meet  
79 minimum recommendations for maintenance plus 1.0 L milk/d (8.71 Mj NE; 99 g MP; 8.7 g  
80 Ca; 4.9 g P) included alfalfa hay (30% as DM), barley straw (26%), beetroot pulp (18%),  
81 orange pulp (26%), and 2) a commercial concentrate for dairy goats (6.78 Mj NE, 135 g MP,  
82 9 g Ca and 4 g P per kg of DM) to meet a total average milk yield of 2.5 L per goat per day,  
83 at the period of the experiment. Rations were offered to the does in an amount 10% higher  
84 than the calculated voluntary feed intake. A high line Casse type milking parlor (2 platforms;  
85 12 goats per platform; 6 milking units) was used; machine milking parameters were set to:  
86 vacuum = 40 kPa, pulsation rate = 90 ppm and pulsation ratio = 60%, until the experimental  
87 period. Does were machine-milked without any udder preparation and using the following  
88 routine: machine milking, machine stripping and post-milking teat-dipping (Proactive Plus.  
89 0.15% iodine, 4% glycerin, and 4% sorbitol-based emollient, DeLaval, Drongen, Belgium).

90 Machine stripping involved a vigorous udder massage for 15-20 s just before the teat-cups  
91 were removed.

## 92 **Experimental Design**

93 On 40 goats at weeks 17, 18 and 19 of lactation, for 11 consecutive days (day 1-11), the  
94 experiment was carried out. The study of udder morphology was conducted on day 1 of the  
95 experiment. Between days 2 and 9 of the experiment (8 d), the milk emission kinetics and teat  
96 thickness change after milking were performed on different combinations of vacuum and  
97 pulsator rate milking parameters, in a Latin square design 4 x 4: four groups of 10 goats, four  
98 combinations of parameters (40 kPa : 90 ppm; 40 kPa: 120 ppm; 42 kPa : 90 ppm; 42 kPa :  
99 120 ppm) and eight days (two milkings per combination). Pulsator ratio was always 60%. On  
100 10 and 11 days of the experiment, teat sphincter strength measurement was carried out.

## 101 **Cluster characteristics**

102 Characteristics of the cluster used are presented in Table 1 and Fig. 1, according to ISO 3918  
103 (2006). Most of the barrel measurements were taken from plaster moulds. The lip mouthpiece  
104 deflection corresponded to the descending value of the lip when a 0.5 kg weight was applied  
105 to a stopper closing the mouthpiece bore (O'Shea et al., 1983). Barrel rigidity was determined  
106 from the minimum necessary vacuum, applied to the liner end, needed to close the barrel  
107 within the shell (Le Du et al., 1978). Diameter of the barrel was measured 75 mm from the  
108 mouthpiece (ISO 3918, 2006).

## 109 **Morphology of the udder**

110 On day 1 of the experiment, the udder characteristics (teat length; teat width at the base; teat  
111 width at the central section; implantation angle from the rear; implantation angle from the  
112 lateral; udder height; Labussière, 1984), teat-floor distance, and, on days 10 and 11 of the

113 experiment, teat sphincter strength (**SS**) were measured. Teat sphincter strength was  
114 performed increasing the level of vacuum, from 0 kPa and without pulsation, applied at the  
115 end of the teat-cup until the appearance of the first spurt of milk (Marnet et al., 2001).  
116 Average values of SS measurements were considered.

### 117 **Milk emission kinetics**

118 Milk emission kinetics was used to evaluate the effect of four different combinations of  
119 milking parameters on milk fractioning, milk flow and milking time. A milk meter  
120 (MM25SG; DeLaval, Tumba, Sweden) and an own software for data interpretation were used  
121 for recording. Data collection was performed every 2s. The kinetic characteristics were taken  
122 from these records: machine milking milk volume (**MM**); machine stripping milk volume  
123 (**MS**); milk flow in the first minute after the onset of foremilk (**MF60**); machine milking  
124 average flow (**MMAF**); machine milking maximum flow (**MMMMF**); machine stripping  
125 average flow (**MSAF**); machine stripping maximum flow (**MSMF**); latency, time elapsed  
126 from teat-cup attachment to milk flow appearance in the claw; time for maximum machine  
127 milking (**TMMM**), time elapsed from teat-cup attachment to the maximum flow of MM;  
128 machine milking duration (**MMT**), time elapsed from teat-cup attachment to MM  
129 completion; time for maximum machine stripping (**TMMS**), time elapsed from MMT to the  
130 maximum flow of MS; machine stripping duration (**MST**), time elapsed to obtain MS; total  
131 milking duration (**TMT**), time elapsed from teat-cup attachment to the end of milking.

### 132 **Teat thickness**

133 Teat-end edema created by the milking machine was estimated with a cutimeter (n° 33865;  
134 Hauptner, D-42651 Solingen), measuring the teat thickness change immediately after  
135 milking, according to Hamann et al. (1996). The difference in thickness measured before and

136 after milking reflects changes in the mass of tissue and fluid in the teat (Hamann and Mein,  
137 1990). Teat thickness was defined as the distance (mm) between the cutimeter jaws for a  
138 given applied pressure. The cutimeter had a new spring that exerted a force of 6.7 N (400  
139 mm<sup>2</sup>, 0.01675 N/mm<sup>2</sup>), similar to Díaz et al. (2013). These authors demonstrated a high  
140 correlation between ultrasound and cutimeter methods for measuring teat-end edema after  
141 milking. Measurements of each teat were performed before and after milking, as the  
142 difference between the readings taken (mm = post-milking reading – pre-milking reading), on  
143 days 2 to 9 of the experiment, for the four milking parameter combinations, after milk  
144 emission kinetics recording and expressed in percentage of the value measured before  
145 milking. Measurements were taken in duplicate; after the first application, the cutimeter was  
146 opened and the thickness gauged again without changing the device's position (Isaksson and  
147 Lind, 1992).

#### 148 **Statistical analysis**

149 Variables from kinetic milk emission (milk yield and fractioning, flows and times) and  
150 percentage of teat-end edema were analyzed using the GLM procedure (SAS Inst. Inc., Cary,  
151 NC), with a model that included the fixed effects of day (8 days; days 2 to 9 of the experiment) and  
152 milking parameters (40 kPa : 90 ppm; 40 kPa: 120 ppm; 42 kPa : 90 ppm; 42 kPa : 120 ppm),  
153 the random effect of animal (1 to 40) and residual error. Separation of means, if appropriate, for  
154 the determination of a significant ( $P < 0.05$ ) main effect was using pairwise contrasts (PDIF  
155 option from SAS). The relationship between variables was carried out following the SAS  
156 Corr Procedure.

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## RESULTS AND DISCUSSION

160 Animal factor, for all studied variables, and milking parameters, for some of them (see Tables  
161 3 and 4), were statistically significant, while day factor was not significant in any case.

### 162 **Udder morphology and teat-cup design**

163 The average udder morphology values are presented in Table 2. Length and width of the teats  
164 are medium-high, while the remaining teat parameters are considered medium values by the  
165 Murciano-Granadina breed association (Ruiz, 2008). The sphincter strength value was 30.1  
166 kPa, with a low standard error but with a maximum of 38.5 kPa (not shown), a value very  
167 close to the milking vacuum (40 kPa) and higher than that reported by Marnet et al. (2001) in  
168 Alpine and Saanen breeds (26.1 kPa). These breeds were milked twice daily whereas in this  
169 experiment one milking per day was performed, as it is common in Murciano-Granadina  
170 breed. The high hardness sphincter in this breed could be related to the habitual high  
171 intramammary pressure (Marnet et al., 1999; Skapetas et al., 2008) due to the accumulation in  
172 the udder of milk produced for a day. Regarding the correlations among the teat  
173 characteristics, beyond those expected, such as significant and positive between length and  
174 width or significant and negative between angle implantation and length, the strength of the  
175 sphincter was not significantly related to any of the udder measurements taken.

176 Analyzing the relations between udder morphology (Table 2) and liner characteristics (Table  
177 1 and Fig. 1), the diameter of the teats on the basis (55 mm) was greater than the internal  
178 diameter of the mouthpiece lip (21 mm), but only slightly greater than the assembly of  
179 mouthpiece lip diameter + mouthpiece mouth diameter (48 mm; 3 + 2 + 3, Fig. 1). The  
180 thickness (2.34 mm) and deflection (7.5 mm) of the lip were similar to those considered  
181 suitable (2 mm and 20 mm, respectively) by Fernández et al. (1997). These authors found that

182 mouthpiece lip deflection was more important than its diameter for a good milk fractionation  
183 during milking. The liner throat (40.8 mm) was slightly wider than the diameter of the teat in  
184 the middle (38 mm), whereas the suggestion is that the liner throat should be 1 to 2 mm  
185 narrower than the teat (Mein, 1992) to avoid teat movement and cluster climbing during  
186 milking. Mein (1992) also indicates that cow teats become longer by 40-50% during milking.  
187 In this experiment, this would represent an average teat length of 91.4 mm after elongation,  
188 which is much shorter than the liner barrel (144 mm). On the other hand, the length of the  
189 teat-cup (202 mm) was greater than the average distance between the lower surface of the  
190 udder and the floor of the milking platform (177 mm), which means that, for the majority of  
191 animals, the milking unit was not hanging from the udder but rested on the platform. This  
192 teat-floor distance is much lower than that reported by Peris et al (1999) for the same breed  
193 (242-258 mm), but the liner meets their recommendations for the same breed, in the sense  
194 that it should be longer than 120 mm. Teat-floor distance was correlated ( $-0.87$ ,  $P < 0.001$ ;  
195 result not shown) negatively with the height of the udder, which may indicate the need to  
196 control udder drop.

### 197 **Milk emission kinetics**

198 Milk fractioning was not altered by the milking parameter combinations tested (Table 3), and  
199 in all cases, the machine stripping milk volume (**MS**) represented a low percentage (from 7.8  
200 to 10.6%) of the total milk yield, when compared with that obtained (17%) by Peris et al.  
201 (1994), for the same breed.

202 All milk flows, except the maximum flow of MS, were affected by the milking parameters,  
203 the highest values corresponding, in general, to the higher vacuum and higher pulsation rate  
204 (42 kPa : 120 ppm). Thus, the combination 42 kPa : 120 ppm required less time for evacuation  
205 of the machine milking milk volume (**MM**) than the rest of the parameter combinations, but

206 similar to the 40 kPa :120 ppm for the total milking duration. This latter fact could be related  
207 to the greater amount of MS (+ 37 mL) to be evacuated after obtaining the MM. Therefore,  
208 the use of the 42 kPa : 120 ppm combination could reduce total milking duration at the max  
209 by 22 s per animal relative to 40 : 90 commonly used, which was one of the objectives of this  
210 work. However, when the vacuum level rises the udder health risk is greater because the teat  
211 edema increases (Table 4), so it is necessary to perform long-term studies with the  
212 combination of parameters 42 kPa : 120 ppm to be sure it does not affect the health status of  
213 the udder, taking into account, among other variables, microbiology and somatic cell count in  
214 milk. From Table 4, it is possible to infer that the increment of pulsation rate from 90 ppm to  
215 120 ppm, for the same level of vacuum (40 kPa or 42 kPa), increases teat edema after milking  
216 by 1.38% or 2.18%, respectively, while the increment of vacuum from 40 kPa to 42 kPa, for  
217 the same pulsation rate (90 ppm or 120 ppm), increases teat edema after milking by 2.61% or  
218 3.41%, respectively. This potential effect of vacuum level on udder health was also observed  
219 by Fernández et al. (1999). The fact that lower differences ( $P = 0.03$  and  $P = 0.08$ ) for milk  
220 flows were associated to the peak flows suggests that the morphological characteristics of the  
221 udder, possibly sphincter strength, are affecting them. The longer latency times correspond to  
222 the higher pulsator rate values, a fact that is difficult to explain, because they did not agree  
223 with the shortest times for machine milking time or total milking time obtained by 120 ppm.  
224 Fernández et al. (1999) also proved the relationship between a higher pulsation rate and a  
225 lower milking time.

## 226 **Milk emission kinetics and udder morphology correlations**

227 Correlations among the parameters of the milk emission kinetics and of the teat were virtually  
228 nonexistent (not shown), with the exception of those related to the sphincter ( $P < 0.001$ ,  
229 Table 4). The sphincter strength is correlated with all parameters of milk emission kinetics

230 except with fraction volumes of milk, and flows and durations of the MS (results not shown).  
231 These results differ from those obtained by Marnet et al. (1999), who found a positive  
232 correlation between the volumes of milk and sphincter strength, which they interpreted as the  
233 strength of the sphincter increasing as intramammary pressure rose. The parameters  
234 associated with MS can vary depending on the force exerted by the milker. However, the  
235 effect of the sphincter strength seems to be very important, as it relates ( $P < 0.005$ ) positively  
236 with all time parameters and negatively with all flow parameters that do not involve the  
237 milker. Similar results were found by Le Du and Benmederbel (1984), which led them to  
238 define the strength of the sphincter as one of the most important parameters to explain  
239 milkability of animals.

## 240 CONCLUSION

241 The cluster used to milk is adequate, although this flock looks to have a problem related to a  
242 poor udder conformation. For a pulsator ratio of 60%, a combination 42 kPa : 120 ppm  
243 (vacuum level : pulsator rate) of milking parameters reduced 22 s total milking time per goat  
244 compared to 40 kPa : 90 ppm, but affected teat thickness measured before and after milking.  
245 It is necessary to carry out a new experiment with the combination of parameters 42 kPa :  
246 120 ppm to be sure it does not affect the health status of the udder.

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318 **Table 1.** Characteristics of the commercial cluster

319 used in the experiment

Characteristics	N° in Fig. 1	
Cluster		
Total weight (g)		620
Claw		
Weight (g)		191
Volume (mL)		100
Rigid shell		
Weight (g)		80
Teatcup		
Length (mm)		202
Liner		
Weight (g)		59
External width of mouthpiece (mm)	1	58
Diameter of mouthpiece lip (mm)	2	21
Length of the mouthpiece lip (mm)	3	14
Thickness of the mouthpiece lip (mm)	4	2.3
Deflection of the mouthpiece lip (mm/0.5 kg)		7.5
Height of mouthpiece (mm)	5	12
Volume of mouthpiece (mL)	6	22
Throat of liner (mm)	7	41
Bore at the bottom of the liner (mm)	8	21
Length of barrel (mm)	9	144
Volume of barrel (mL)	10	74
Diameter of the barrel (mm)		20
Rigidity: tightening vacuum compression (kPa)		9.3

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324 **Table 2.** Udder morphology<sup>a</sup> of the goats (m ± SEM)

<b>L</b>	<b>W1</b>	<b>W2</b>	<b>α</b>	<b>L</b>	<b>SS</b>	<b>TF</b>	<b>H</b>
<b>(mm)</b>	<b>(mm)</b>	<b>(mm)</b>	<b>(°)</b>	<b>(°)</b>	<b>(kPa)</b>	<b>(mm)</b>	<b>(mm)</b>
63 ± 4	55 ± 4	38 ± 3	45.2 ± 3.3	46.6 ± 3.4	30.1 ± 0.5	177 ± 7	277 ± 0.5

325 <sup>a</sup>Udder morphology: L = teat length; W1 = teat width at the base; W2 = teat width at the  
326 central section; α = teat implantation angle from the rear; L = teat implantation angle from the  
327 lateral; SS = teat sphincter strength; TF = distance from the bottom of the udder to the floor;  
328 H = height of the udder.

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338 **Table 3.** Milk emission kinetics and milk fractioning

Item	Milking parameters (kPa : ppm) <sup>c</sup>				SEM	<i>P</i>
	40 : 90	40 : 120	42 : 90	42 : 120		
Milk fractioning <sup>d</sup> (mL/d)						
MM	2,083	1,980	2,091	2,027	44	0.28
MS	175	204	190	241	18	0.09
TM	2,258	2,184	2,281	2,268	50	0.65
Milk flow <sup>e</sup> (mL/min)						
MF60	809 <sup>a</sup>	805 <sup>a</sup>	847 <sup>ab</sup>	900 <sup>b</sup>	22	0.001
MMAF	733 <sup>a</sup>	732 <sup>a</sup>	753 <sup>a</sup>	810 <sup>b</sup>	19	0,01
MMMMF	1,203 <sup>ab</sup>	1,172 <sup>b</sup>	1,188 <sup>b</sup>	1,268 <sup>a</sup>	25	0.03
MSAF	300 <sup>a</sup>	351 <sup>b</sup>	344 <sup>ab</sup>	372 <sup>b</sup>	16	0.01
MSMF	644	677	677	749	30	0.08
Time <sup>f</sup> (s)						
Latency	5.4 <sup>a</sup>	6.6 <sup>b</sup>	5.1 <sup>a</sup>	6.1 <sup>ab</sup>	0.4	0.02
TMMM	88	90	83	84	4.3	0.62
MMT	186 <sup>a</sup>	174 <sup>a</sup>	180 <sup>a</sup>	160 <sup>b</sup>	4	0.001

TMMS	13	12	13	15	1	0.35
MST	33	30	30	37	2	0.07
TMT	219 <sup>a</sup>	204 <sup>ab</sup>	209 <sup>a</sup>	197 <sup>b</sup>	3	0.001

339 <sup>a-b</sup> Within a row, means without a common superscript differ ( $P < 0.05$ ).

340 <sup>c</sup>Kilopascals : Pulsations per minute.

341 <sup>d</sup>Milk fractioning: MM = machine milking milk volume; MS = machine stripping milk  
342 volume: TM = total milk volume.

343 <sup>e</sup>Milk flow: MF60 = milk flow in the first minute after the onset of foremilk; MMAF =  
344 machine milking average flow; MMMF = machine milking maximum flow; MSAF =  
345 machine stripping average flow; MSMF = machine stripping maximum flow.

346 <sup>f</sup>Time: Latency = time elapsed from teat-cup attachment to milk flow appearance in the claw;  
347 TMMM = time for maximum machine milking flow; MMT = machine milking duration;  
348 TMMS = time for maximum machine stripping flow; MST = machine stripping duration;  
349 TMT = total milking duration.

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356 **Table 4.** Percentage of teat-end edema (mm) created by different combinations of vacuum  
 357 level and pulsator rate of milking machine

Milking parameters (kPa : ppm) <sup>c</sup>					
40 : 90	40 : 120	42 : 90	42 : 120	SEM	<i>P</i>
- 1.42 <sup>a</sup>	- 0.04 <sup>ab</sup>	1.19 <sup>b</sup>	3.37 <sup>b</sup>	1.1	< 0.0001

358 <sup>a-b</sup> Within a row, means without a common superscript differ ( $P < 0.05$ ).

359 <sup>c</sup>Kilopascals : Pulsations per minute.

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371 **Table 5.** Correlations among some parameters of milk emission kinetics and the teat  
 372 sphincter strength

Item	Milk emission kinetics parameters <sup>a</sup>						
	Latency	MMT	TMMM	TMT	MF60	MMAF	MMMMF
Teat	0.68	0.69	0.60	0.65	- 0.62	- 0.59	- 0.63
sphincter strength	***	***	***	***	***	***	***

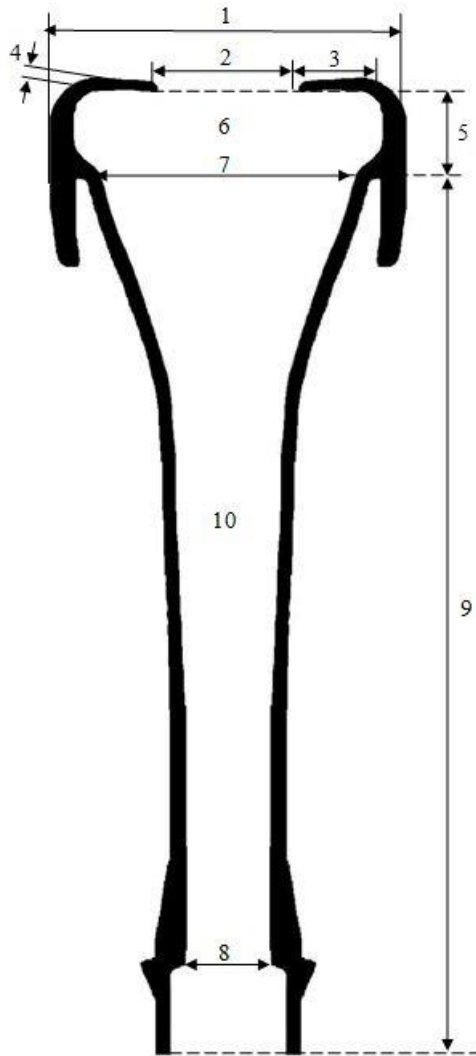
373 \*\*\* $P < 0.001$ .

374 <sup>a</sup>Kinetic parameters: MMT = machine milking duration; TMMM = time for maximum  
 375 machine milking; TMT = total milking duration; MF60 = milk flow in the first minute after  
 376 the onset of foremilk; MMAF = machine milking average flow; MMMF = machine milking  
 377 maximum flow.

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**Figure 1.** Section of the liner used in the experiment

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