

Document downloaded from:

<http://hdl.handle.net/10251/96962>

This paper must be cited as:

Capolino, G.; J. Antonino-Daviu; Riera-Guasp, M. (2015). Modern Diagnostics Techniques for Electrical Machines, Power Electronics, and Drives. IEEE Transactions on Industrial Electronics. 62(3):1738-1745. doi:10.1109/TIE.2015.2391186



The final publication is available at

<http://doi.org/10.1109/TIE.2015.2391186>

Copyright Institute of Electrical and Electronics Engineers

Additional Information

# Modern Diagnostics Techniques for Electrical Machines, Power Electronics, and Drives

## I. INTRODUCTION

FOR THE last ten years, at least three different Special Sections dealing with diagnostics in power electrical engineering have been published in the IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS [1]–[5]. All of them had their specificities, but the last ones, starting in 2011, were more connected to relevant events organized on the topic. In fact, these events have been clearly the only international forums fully dedicated to diagnostics techniques in power electrical engineering. For this particular issue, it has been decided to separate the different submissions into six parts:

- state of the art;
- general methods;
- induction machines (IMs);
- synchronous machines;
- electrical drives;
- power components and power converters.

The second section includes only one state-of-the-art paper, which is dedicated to actual techniques implemented in both industry and research laboratories. The third section includes three papers on diagnostic techniques not specifically aimed at a particular type of machine. The fourth section includes three papers devoted to diagnostics of rotor faults, two dedicated to stator insulation issues, and four papers dealing with mechanical faults diagnosis in IMs. The fifth section includes papers focusing on different types of synchronous machines. The first two papers deal with wound-rotor synchronous machines, the following three papers are dedicated to permanent-magnet radial flux machines, and the last one deals with permanent-magnet axial flux machines. Regarding the types of faults analyzed, there are three papers devoted to the diagnosis of interturn short circuits in the stator windings, i.e., one dedicated to the detection and location of field-winding-to-ground faults and a paper devoted to the diagnosis of static eccentricities. In the sixth section, two papers investigate issues related to faults in drive sensors, and one is devoted to fault detections in the coupling inductors. The last section includes two papers devoted to diagnosis of faults and losses analysis in switching components of power converters.

## II. STATE OF THE ART

In [6], the authors have screened the most recent papers published on the topic to draw the real “state of the art” on condition monitoring and fault detection of rotating electrical

machines, drives, and power electronics. As expected, since it is the most investigated electrical machine from the very beginning, a large part of the development has been dedicated to IMs. It is well known that most of the methods developed for IMs can be simply used directly or adapted for other types of rotating electrical machines or even for linear actuators or generators.

A large part of this paper is dedicated to IM fault detection since it has been the historical field of investigation for the last 30 years or so. In this way, rotor faults have been under focus mainly for squirrel-cage IMs with convenient signal processing techniques to tackle the fact that many faults cannot be detected easily when the machine load is light. The second largest part dealing with the IM fault detection is related to stator winding, including the insulation degradation and further early stage short circuits. It has been shown that the insulation degradation detection is the best way to prevent short circuits, but it is the most difficult to be implemented online. Moreover, early stage short circuits are easier to detect particularly by the use of a stray flux sensor, which is simple, cheap, and noninvasive for large-power IMs. Other methods to detect early stage short circuits are based on the impedance asymmetry on the stator side. In this last case, the sensors are based on both stator voltages and stator currents measurements. Then, the decision process for early stage short-circuit detection can be based on advanced artificial intelligence techniques, which are well known in this specific area. Finally, in the case of IMs, methods for mechanical failures detection have been investigated. Faults such as eccentricities, bearings, and gearboxes have been under focus. On the other hand, a brief analysis of the ongoing research in the field of multiphase IMs has been pointed out.

The same approach has been presented for permanent-magnet synchronous machines (PMSMs) or even synchronous generators (SGs) but with a shorter description since the main features of the IMs fault detection can be applied in the same way for PMSMs. However, the detection of demagnetization has been added as an important point specific to these machines. As in the case of IMs, a brief analysis of the ongoing research in the field of multiphase PMSMs has also been developed.

The last part of this paper has been dedicated to fault detection in power converters and power components as a part of diagnostic techniques associated with power electronics. For the power converters, specific techniques have been developed in order to speed up the detection process in order to avoid components breakage. These techniques have been successfully applied to inverters, matrix converters, and even to dc–dc converters. The problem of fault detection in dc link capacitors has also been analyzed. For the power components, things are much more difficult since they have fast switching capabilities and the

95 fault detection has to be as fast as possible. Therefore, the fault  
 96 detection techniques have been applied to both insulated-gate  
 97 bipolar transistors (IGBTs) and MOSFETs in order to protect  
 98 them from irreversible failures. In the same way, the very last  
 99 part of this paper is dedicated to fault-tolerant drives for which  
 100 multilevel and multiphase topologies have been developed in  
 101 the last ten years.

102

### III. GENERAL METHODS

103 In [7], a robust electric motor fault decision-making algo-  
 104 rithm, particularly suited for harsh industrial environments, is  
 105 presented. The proposed technique is based on the simultaneous  
 106 utilization of multiple fault signature patterns, noise signal fre-  
 107 quency patterns, and fundamental harmonics current frequency  
 108 patterns in a whole motor current signal for diagnosis purposes.  
 109 As the authors pointed out, the identified pattern is proven to be  
 110 robust to the signal distortion and inherent monitor noise during  
 111 motor dynamic operation. In this paper, it is mathematically and  
 112 experimentally proven that the proposed diagnosis algorithm  
 113 provides highly accurate monitoring performance while mini-  
 114 mizing both false detection and missing detection rates under  
 115 high noise and nonlinear machine operating conditions. The  
 116 experimental results are obtained with a DSP-based IM drive  
 117 system, where motor control and fault diagnosis are performed  
 118 in real time. The faulty conditions considered in the work are  
 119 broken rotor bars and eccentricities. The authors include some  
 120 comments regarding its possible constraints related to industrial  
 121 applicability of the proposed technique, stating that since the  
 122 proposed method assumes prior knowledge of harmonics in  
 123 a motor current spectrum, small additional memory might be  
 124 required to implement the proposed method. In addition, a suf-  
 125 ficient frequency bandwidth of data acquisition and motor con-  
 126 trol is required, particularly for high-frequency signal detection.  
 127 In [8], a new online diagnosis of three-phase IM stator  
 128 faults using a signal-based method is proposed. The proposed  
 129 technique starts with a data preprocessing stage, in which prin-  
 130 cipal component analysis (PCA) is applied to current signals.  
 131 PCA enables the reduction of the three-phase currents space  
 132 to a two-dimensional space. Afterward, features are extracted  
 133 from PCA-transformed data using the kernel density estimation  
 134 (KDE) improved by fast Gaussian transform along with a point  
 135 reduction method. The automatic fault identification is achieved  
 136 by means of Kullback–Leibler divergence (KLD), which is used  
 137 as an index to identify the dissimilarity between two probability  
 138 distributions. The final goal is to ensure that the developed  
 139 technique can be used for online monitoring; this is possible due  
 140 to the remarkable computational cost reduction obtained with  
 141 the aforementioned enhancement techniques, in comparison  
 142 with the standard KDE. In this regard, before presenting their  
 143 developed algorithm, the authors perform a thorough descrip-  
 144 tion and analysis of the considered techniques, namely, PCA,  
 145 KDE, improved KDE by fast Gaussian transform, and point  
 146 reduction and KLD. This paper also includes experimental  
 147 results obtained with two different IMs and under three different  
 148 fault conditions: cracked rotor, out-of-tolerance geometry rotor,  
 149 and backlash. The tests are carried out at different load and  
 150 voltage levels to prove the proposed method effectiveness. The

authors emphasize that it is totally signal based since no IM 151  
 parameters are required. 152

In [9], a stochastic modeling-based prognosis approach 153  
 [extended Kalman filter (EKF)] is proposed for tracking the 154  
 remaining useful life (RUL) of bearings under different oper- 155  
 ating conditions. The proposed data-driven methodology relies 156  
 on both time and time–frequency domain features of vibration 157  
 signals obtained from the PROGNOSTIA platform. In this 158  
 regard, the authors reach original conclusions on the better suit- 159  
 ability of different features for different operating conditions 160  
 depending on the length of the test data set. For instance, the 161  
 authors show that the entropy feature is successful at detecting 162  
 the early stages of degradation, whereas the variance feature 163  
 is not very informative until the final failure stage. As the 164  
 authors point out, shorter test data sets provide less information 165  
 for RUL estimation yielding higher error rates, which is in 166  
 concordance with the conclusions of other works based on the 167  
 same data set. Once features have been extracted, an analytical 168  
 function, which best approximates the evolution of the fault, 169  
 is determined and used to learn the parameters of the EKF. In 170  
 this regard, the work gives a detailed description of the RUL 171  
 estimation based on EKF, and unlike other investigations, also 172  
 provides a procedure to estimate the confidence interval along 173  
 with the RUL estimates. The algorithm is finally applied to 174  
 bearing vibration data obtained from the mentioned platform, 175  
 illustrating the convergence of the algorithm, as well as its be- 176  
 havior under different conditions. The work includes a compar- 177  
 ison of EKF versus the regular KF showing better performance 178  
 of the proposed approach for all operating conditions. 179

### IV. IMs

180

In [10], a detailed comparison between the two main groups 181  
 of transforms that are employed for IMs rotor assessment based 182  
 on transient analysis (continuous versus discrete transforms) 183  
 is presented. In this paper, the discrete wavelet transform and 184  
 the short-time Fourier transform are taken as representatives 185  
 of each respective group. The work begins with an overall 186  
 revision of the diagnosis based on transient analysis and the 187  
 inherent benefits that such methodology brings in comparison 188  
 to the conventional motor current signature analysis (MCSA) 189  
 approach. The authors remark on its usefulness in cases where 190  
 the MCSA may lead to incorrect diagnostic conclusions. A 191  
 detailed description of the operation of each group of trans- 192  
 forms is presented making special emphasis on aspects as 193  
 fault severity quantification or computational burden. In this 194  
 regard, the authors emphasize the following advantages of 195  
 the continuous tools versus their discrete counterparts: clearer 196  
 extraction of the low-frequency fault components evolutions, 197  
 possibility of tracking the high-order harmonics evolutions, 198  
 and easier fault discrimination. Afterward, the authors show 199  
 the results of applying each transform to data obtained with 200  
 real IMs. These results do not only consider trivial fault sit- 201  
 uations, where the conventional MCSA also works well, but 202  
 also some of the controversial cases, where the application 203  
 of the conventional methods often leads to false diagnostics, 204  
 namely, outer bar breakages in double cage IMs, IMs with rotor 205  
 axial duct influence, as well as combined faults. The authors 206

AQ1

AQ2

207 present a detailed discussion of the performance of each group  
208 of transforms based on their results concerning aspects such as  
209 quantification or computational time. In their conclusions, they  
210 ratify the aforementioned advantages of the continuous tools,  
211 and they also tear down the false myth concerning the higher  
212 computational burden of continuous transforms.

213 In [11], the authors analyze a diagnostic problem related to  
214 IMs with special magnetic structures. More specifically, this  
215 paper deals with the false broken rotor bar alarms that have been  
216 reported in cage IMs with a number of rotor axial ducts equal to  
217 the number of poles. In such cases, even in healthy conditions,  
218 two sidebands appear around the fundamental component; their  
219 frequencies are equal to those produced by a broken bar. This  
220 problem is documented through the analysis of three high-  
221 voltage IMs working in actual industrial applications that were  
222 misdiagnosed. The authors analyze the theoretical origin of this  
223 issue and conclude that the confusing sidebands are produced  
224 by the periodical variations of reluctance that the fundamen-  
225 tal flux wave undergoes during its relative rotation along the  
226 cross section of the rotor. Once the physical phenomenon is  
227 explained, the authors propose a diagnosis method based on the  
228 current sidebands originated by the fifth and seventh space har-  
229 monics of the flux wave. The authors state that these high-order  
230 harmonics hardly penetrate the rotor core and, consequently,  
231 are not affected by the rotor axial air ducts. This hypothesis is  
232 experimentally verified using specifically built prototypes.

233 In [12], the results of a fatigue test that is intended to  
234 reproduce, in the most natural way possible, the exposed rotor  
235 bar breakage process in an IM. For this purpose, a 1.5-kW  
236 two-pole squirrel-cage IM is monitored along 82 265 identical  
237 working cycles, each one comprising a heavy start-up, a pe-  
238 riod of stationary operation at rated load and, finally, a plug  
239 stopping. To accelerate the breakage process, one of the rotor  
240 rings was mechanized in order to weaken the junction between  
241 the end-ring and the bars. In addition, an incipient breakage  
242 was forced in one of the rotor bars. Afterward, the working  
243 cycle was repeated until the bar naturally cracked. Taking as  
244 bases the results of these tests, the authors carry out three  
245 different analyses. First, they compare the performances of sev-  
246 eral fault indicators described in the literature for tracking the  
247 fault components evolutions; transient and steady-state-based  
248 parameters are considered in this study. Second, an explanation  
249 of the breakage mechanism is given, based on a series of  
250 pictures of the breakage region, which were taken during the  
251 breakage development. Third, a physical model of the failure  
252 is introduced and, based on this model, the authors propose  
253 an algorithm for state estimation and prognosis analysis of the  
254 bars health.

255 In [13], a diagnostic method based on parameter estimation,  
256 which is applied to the detection of interturn short circuits in  
257 IMs, is proposed. The detection algorithm is based on three  
258 blocks that are cyclically executed: The first block is a coupled  
259 circuits model of the IM, able to simulate faults in the stator  
260 windings; in this model, the faults are characterized by three  
261 parameters ( $\mu f$ : fault location;  $\mu s$ : severity of the fault; LL:  
262 load level). The second block is an objective function whose  
263 value depends on the errors between the measured currents  
264 and the currents calculated by the model. The third block is a

global optimization algorithm, called hyperbolic cross points 265  
algorithm. It efficiently seeks the combination of parameter 266  
values, which minimize the objective function under the tested 267  
operation conditions. The authors claim that the proposed al- 268  
gorithm reliably locates, with a reduced number of iterations, 269  
the global minimum of the objective function, avoiding errors 270  
due to local minima. The state of the IM, i.e., the severity and 271  
location of the fault, is characterized by the set of parameters 272  
that lead to the global minimum of the objective function. The 273  
authors validate the method by simulations and laboratory tests, 274  
showing that it can detect a fault affecting 8% of the turns of a 275  
phase with a processing time of 106 s. 276

In [14], a method for monitoring the insulation health of 277  
IMs is proposed. As the authors highlight, the objective of 278  
this work is not to detect sudden insulation faults but to ob- 279  
serve a trend of the insulation state indicator over time. The 280  
method is applicable to IMs fed by voltage-source inverters. It 281  
relies on an offline test, which consists of applying a voltage 282  
step, obtained by switching the inverter, to the tested phase. 283  
The subsequent reaction current is recorded and employed to 284  
evaluate the winding condition. This current is based on high- 285  
frequency oscillations, which vanish after a few microseconds. 286  
It is shown that the current evolution depends on the parasitic 287  
turn-to-turn and winding-to-ground capacitances that change 288  
during the aging process of the insulation. The authors propose 289  
two insulation state indicators, which are intended for phase 290  
evaluation (ISI) and global winding evaluation (SISI). These 291  
parameters are computed comparing the current spectra and 292  
reference spectra, obtained in healthy condition. The method 293  
is validated on two quite different IMs, rated 280 V, 5.5 kW and 294  
1428 kW, 2183 V, respectively. 295

In [15], a new technique based on stray flux measurement is 296  
proposed for bearing fault detection in IMs. The method relies 297  
on the statistical processing of the measurements of this quan- 298  
tity in different positions around the IM. The usefulness of the 299  
proposed method is mainly justified based on the simplicity and 300  
the flexibility of the custom flux probe with its amplification 301  
and filtering stage. The authors first present a detailed literature 302  
survey about the use of stray flux measurement in the IMs fault 303  
diagnosis area, emphasizing the advantages of such approach 304  
in comparison with other techniques. Afterward, their proposed 305  
method is described; it requires at least ten data acquisitions of 306  
the stray flux, performed under identical conditions, both for 307  
the healthy machine (considered as reference) and the same 308  
machine having diverse bearing faults. The authors prove the 309  
validity of the method in a real IM, considering three different 310  
types of bearing failure (crack in the outer race, hole in the 311  
outer race, and deformation of the seal) under different load 312  
conditions. In addition, different positions for the flux mea- 313  
surement with their custom probe are considered, as well as a 314  
comparison with a commercial probe, leading to a total number 315  
of 32 analyzed cases. Their subsequent discussions lead to 316  
interesting conclusions as to the suitability of the method even 317  
to detect damages in the bearing seal, the good performance 318  
of their probe for higher loads or the general higher effectivity 319  
of the custom probe versus the commercial one for stray flux 320  
measurements, among others. The only requisite of the method 321  
is that it needs an initial data set as “healthy reference” for 322



323 comparisons to the successive measurements during the IM  
324 lifetime.

325 In [16], a methodology for diagnosing localized defects in  
326 the outer race of IM bearings is introduced. The method relies  
327 on the spectral analysis of the squared envelope of the stator  
328 current in an optimized frequency band, characterized by a  
329 central frequency  $f_c$  and a bandwidth  $Bw$ , which contains the  
330 nonstationary components with frequencies related to fault. The  
331 optimum frequency interval is selected using the kurtogram of  
332 the current as a decision tool: it simply consists of selecting the  
333 central frequency/bandwidth combination that maximizes the  
334 spectral Kurtosis in the kurtogram. Advanced algorithms such  
335 as the fast kurtogram or the wavelet kurtogram are used in this  
336 work to compute the kurtogram in a computationally efficient  
337 way. The method is validated by means of laboratory tests,  
338 using two bearings with forced faults, consisting of holes with  
339 different diameters. Under these strong defect conditions, this  
340 technique enables a clear detection of the fault components,  
341 although as the authors state, the method needs to be validated  
342 with small and real defects.

343 In [17], the authors have presented the gear tooth damage  
344 fault detection using the IM as a sensor but measuring its stator  
345 currents. The basic principle is to use the torque oscillations  
346 as a means to bring to the IM currents the image of what is  
347 happening in the mechanical part related to the machine shaft.  
348 Therefore, the electromagnetic torque has been developed as  
349 a mean part plus an oscillation part for both healthy and faulty  
350 cases and characteristic frequencies of the oscillating parts  
351 have been identified. A simplified model of the mechanical part  
352 has been developed to compute these characteristic frequencies  
353 from a theoretical point of view and to relate them to the IM  
354 currents. In order to detect the different frequencies related to  
355 the mechanical failure, a fault profile reconstruction has been  
356 defined and a fault index has been proposed. The proposed  
357 methodology has been applied to a simple test rig with a  
358 three-phase IM connected by its shaft to a pinion and a wheel  
359 with very small surface wear damage on one tooth for each  
360 part. Both simulation and experimental results have confirmed  
361 the validity of this new technique of mechanical fault detection.

362 In [18], a method called spectral kurtosis with reference is  
363 employed to design a system's healthy reference. This approach  
364 is afterward evaluated for mechanical unbalance detection in  
365 IMs using the stator currents instantaneous frequency. As the  
366 authors explain, the definition of a healthy reference enables  
367 the computation of normalized fault indicators whose values  
368 are independent of the system characteristics. This means a  
369 significant advantage when diagnosing systems with different  
370 power, coupling, inertia, and load. In this paper, the authors re-  
371 view the concept of kurtosis and demonstrate its ability to detect  
372 outliers within a reference distribution. They introduce a new  
373 kurtosis-based indicator,  $SK_R$ , which includes a new reference  
374 set, and they prove its ability to generate a system's healthy  
375 reference and to detect any drift from it. The authors evaluate  
376 this indicator using synthetic signals and also experimentally  
377 verify its efficiency when applied to the current instantaneous  
378 frequency for the detection of low levels of mechanical unbal-  
379 ance. Their results prove the  $SK_R$  detection capacity with a  
380 single fault threshold for a wide range of load conditions and

ratify the usefulness of creating a system's healthy reference for 381  
the robust detection of weak mechanical unbalances, avoiding 382  
false alarms for different operating conditions and showing a 383  
great robustness against load variations. 384

## V. SYNCHRONOUS MACHINES 385

In [19], an SG model that enables the simulation of stator 386  
interturn short circuits is presented. The novelty of this work is 387  
that it develops a hybrid model, in which the Winding Function 388  
Approach (WFA) is combined with the  $dq0$  transform. As the 389  
authors remark, the proposed model takes advantage of the 390  
suitability of WFA for detailed and simple representation of 391  
the faults and, at the same time, enables the calculation simplic- 392  
ity that is provided by the  $dq0$  representation. Consequently, a 393  
very precise model that is suitable to run online is achieved. In 394  
addition, this model accounts for the effect of local saturation of 395  
the magnetic circuit due to the fault currents. Local saturation 396  
and saliency are taken into consideration through a modified 397  
airgap function, which facilitates the accurate computation of 398  
the inductance of the shorted turns. The model is extensively 399  
validated by laboratory tests and compared with a model based 400  
on the  $dq0$  transform. The authors conclude that the proposed 401  
model provides more accurate results than the  $dq0$  model 402  
although its performance with incipient faults needs to be 403  
improved. 404

The work presented in [20] deals with the accurate local- 405  
ization of field-winding to ground faults in SGs. First, the 406  
authors analyze in detail a previously developed method for 407  
the online detection of excitation-system faults to ground that 408  
is valid for generators with static excitation. The method allows 409  
discriminating if the fault takes place in the ac side or in the dc 410  
side of the excitation system. In the event of faults in the dc side, 411  
the method approximately forecasts the location of the fault in 412  
the excitation winding. However, this procedure depends on the 413  
value of the fault resistance  $R_f$ , which has to be estimated; this 414  
fact leading to a wide margin of indetermination. The main 415  
contribution of this work is a new algorithm that, from the 416  
measured quantities, accurately calculates the value of the fault 417  
resistance  $R_f$ . The method is validated through laboratory tests 418  
and also on a 106-MW SG operating under real conditions in 419  
a hydroelectric power plant. From the test results, the authors 420  
claim that the proposed method for the computation of  $R_f$  421  
significantly reduces the errors in the fault location; this fact is 422  
relevant in hydrogenerators with high number of poles, since it 423  
reliably enables the location of the pole where the fault occurs. 424  
This way, the extraction of the whole rotor can be avoided, thus 425  
substantially reducing repair costs. 426

In [21], the authors introduce an approach for interturn short- 427  
circuit diagnosis in five-phase PMSMs. The approach relies on 428  
the spectral analysis of the modulus of a space vector  $\vec{D}$ . This 429  
vector is obtained as a combination of two space vectors that 430  
are calculated from the measured phase voltages but using two 431  
different reference frames, named  $\alpha\beta$  and  $\alpha2\beta2$ . It is justified 432  
that an interturn fault in one of the stator phases produces an 433  
increase in the  $DC$  and  $2fs$  components in the spectrum of 434  
the modulus of the space vector  $\vec{D}$  ( $fs$  : supply frequency 435  
fundamental harmonic). It is shown from simulations and tests 436

437 that this signature is very sensible, reaching amplitude incre-  
438 ments in the fault-related harmonics higher than 15 dB for  
439 a fault affecting up to 3% of the turns of a phase; and it is  
440 also clearly different from the signatures produced by other  
441 kind of faults (as static or dynamic eccentricity and partial  
442 demagnetization), thus enabling a robust and reliable diagnosis  
443 of interturn short-circuit faults.

444 The work presented in [22], as in the previous paper, deals  
445 with interturn short-circuit detection in PMSMs. In this case,  
446 the work is focused on three-phase PMSMs working under  
447 high variable load and speed conditions, as it happens in  
448 aircraft applications. This work proposes an approach based on  
449 parameter identification. The authors introduce a PMSM model  
450 based on the  $dq$  reference frame, where the short-circuited turns  
451 ratios of each phase ( $n_{s/cA}, n_{s/cB}, n_{s/cC}$ ) are the parameters  
452 to be identified. The estimation of these parameters is carried  
453 out using the EKF, which is justified to be a suitable tool that  
454 enables to perform accurate estimations in real time, even under  
455 continuous and substantial changes in the operation conditions.  
456 Finally, the fault indicators are defined as the average value  
457 of the estimated short-circuited turns ratios calculated over a  
458 sliding window with a length equal to half period of the main  
459 component. The approach is extensively validated by simula-  
460 tion and laboratory tests; it is demonstrated to be robust against  
461 frequency variations, load variations, power factor variations,  
462 load unbalances, and harmonic content variations.

463 Reference [23] is the only paper in this Special Section  
464 dealing with axial flux PMSMs. In this paper, the authors  
465 introduce a method for diagnosing static eccentricities in axial  
466 flux PMSMs. The method requires the installation of three  
467 search coils, mounted on three stator teeth shifted  $120^\circ$ . First,  
468 a parameter named static eccentricity factor (SEF) is defined  
469 in order to characterize the fault severity in such type of  
470 machines; then, a simple algorithm is theoretically justified  
471 that enables calculation of the SEF, and also the position of  
472 minimum airgap in a faulty machine, using the measured back  
473 electromotive forces in the search coils. It is interesting that  
474 the computed SEF depends neither on the rotor speed nor on  
475 the load. The approach is extensively validated via simulations,  
476 using a 3-D finite-element software, as well as thorough labo-  
477 ratory tests.

478

## VI. ELECTRICAL DRIVES

479 In [24], a new fault detection and isolation technique is pre-  
480 sented with the aim of making the traditional vector-controlled  
481 IM drive fault tolerant against current and speed sensor failure.  
482 The underlying idea is that the controller keeps estimating  
483 the different currents and the speed and, in case of a fault, it  
484 switches to the correct estimated value. On the one hand, the  
485 proposed technique extracts eight estimates of currents in the  
486  $\alpha - \beta$  reference frame (the authors obtain four estimates using  
487 the reverse transformation from  $d-q$  to  $\alpha - \beta$  and the other  
488 four using the forward transformation from  $a-b-c$  to  $\alpha - \beta$ ).  
489 In this context, the concept of vector rotation is introduced to  
490 decide the correct estimated value of current corresponding to a  
491 fault. On the other hand, the speed is estimated by modifying  
492 one of the available model reference adaptive system-based

formulations (X-based MRAS). Both simulations, as well as 493  
494 experiments carried out with a laboratory prototype, demon- 494  
495 strate that the system is capable of detecting a fault and recon- 495  
496 figure itself in a seamless manner. In this regard, the authors 496  
497 thoroughly evaluate the performance of the proposed algorithm 497  
498 under different faulty conditions of the considered sensors. 498  
499 The results prove that proposed technique works well even in 499  
500 the case of multiple sensor failures and does not require any 500  
501 additional sensor. The developed fault-tolerant controller can 501  
502 be particularly useful for applications such as electric vehicles 502  
503 to avoid complete shutdown of the system, in case of sensor 503  
504 failure. 504

In [25], the detection of incipient faults in coupling inductors 505  
506 used in three-phase adjustable-speed drives with direct power 506  
507 control-based active front-end rectifiers is considered. More 507  
508 specifically, the authors develop a new strategy for early fault 508  
509 detection in coupling inductors, which enables a fast identi- 509  
510 fication of the defective phase while providing an accurate 510  
511 estimation of the inductance value of the coupling inductors that 511  
512 enhances the performance of the direct power control method. 512  
513 The underlying idea is that coupling inductor faults (e.g., an 513  
514 interturn short circuit) lead to a variation in the value of the 514  
515 coupling inductance. Hence, the goal is to detect the fault by 515  
516 tracking estimations of the coupling inductances associated 516  
517 with a fault in each phase. A detailed description of the full 517  
518 estimation procedure is given in this paper. Both simulation 518  
519 and experimental tests demonstrate the validity of the proposed 519  
520 method. As stated in this paper, the detection of the fault 520  
521 enables the suspension of the service if this is required to 521  
522 avoid a major breakdown. In addition, the identification of the 522  
523 affected phase enables the replacement of only the defective 523  
524 inductor if three single-phase chokes are used or helps with 524  
525 the repair of the nonhealthy winding if a three-phase reactor is 525  
526 used. Among the claimed advantages of the proposed method 526  
527 are the simplicity, speed, and effectiveness. On the other hand, 527  
528 the main constraint relies on the manufacturing tolerance of 528  
529 the inductors, which makes their actual values differ from 529  
530 each other including when there are not any faults. This latter 530  
531 issue, however, does not affect the robustness of the presented 531  
532 strategy. 532

In [26], an observer-based fault detection method is designed 533  
534 for the rotor position sensor of PMSM drives in an elec- 534  
535 tromechanical brake (EMB). To this end, the authors develop 535  
536 a position estimation algorithm with a full-order Luenberger 536  
537 observer for the rotor flux linkage. However, there are some 537  
538 deviations between the observer and the real process caused by 538  
539 model uncertainties and parameter variations. To overcome this 539  
540 drawback, the authors add a crucial feature in their detection 540  
541 method that relies on an adaptive threshold; this is determined 541  
542 by analyzing position estimation errors of the observer. The 542  
543 adaptive threshold enables, among other things, avoidance of 543  
544 missing or false alarms. The experimental results using the 544  
545 EMB test bench prove the effectiveness and robustness of the 545  
546 designed method that can even detect a small amount of phase 546  
547 shift fault within a wide operation range, not only at steady state 547  
548 but also under transient operation. Moreover, the fault-tolerance 548  
549 capability of the proposed method is achieved by introducing a 549  
550 compensation algorithm for the phase shift. The experimental 550

551 results show that this compensation algorithm is useful for  
 552 tolerating the phase shift fault. For other types of rotor position  
 553 sensor faults, the authors propose potential solutions that can  
 554 overcome low-speed limitation issues, such as the incorporation  
 555 with a high-frequency injection-based method. This latter ap-  
 556 proach can be somehow complementary to that proposed in the  
 557 work, since each of them shows special suitability for different  
 558 speed ranges.

## 559 VII. POWER COMPONENTS AND POWER CONVERTERS

560 In [27], an adaptive threshold-based approach is also pre-  
 561 sented, but in this case it is to design an electronic failure detec-  
 562 tion system applied to the IGBT. More specifically, the method  
 563 proposed by the authors relies on the direct measurement of  
 564 behavior of the gate signal during the IGBT turn-on transient  
 565 via continuous processing using analog and digital electronics.  
 566 The main goal pursued with an early fault detection design in  
 567 the IGBT is to obtain a corrective action to prevent propagation  
 568 of the fault to the complementary device in the same affected  
 569 leg in the inverter-motor system, when a short circuit or an  
 570 overcurrent occurs. Two different faults are considered in the  
 571 work: open-circuit and short-circuit failures. The considered  
 572 stages of the developed diagnosis scheme are improved resid-  
 573 ual generation stage, ramp rate, and a symmetrical adaptable  
 574 thresholds stage. The final scheme is intended to decrease the  
 575 false alarm rate by the aforementioned failures. To achieve the  
 576 early fault detection, the proposed circuit is implemented in  
 577 the gate driver using analog electronics. As the authors point  
 578 out, the main advantage of adding detection process with adap-  
 579 tive threshold is that the false alarm rate decreases because the  
 580 system is not so vulnerable to variations in the power supply  
 581 of the IGBT gate driver circuit. On the other hand, the main  
 582 limitation is that the proposed design is not suitable for power  
 583 applications, where the switching frequency is above 20 kHz  
 584 since the introduction of an external resistance limits the IGBT  
 585 switching speed.

586 In [28], a methodology to analyze the losses in the converters  
 587 of fault-tolerant drives is presented. This work aims to evaluate  
 588 the losses in the power components of the converter (IGBT,  
 589 diodes, capacitors) during the time the fault takes place, during  
 590 the subsequent reconfiguration process and, finally, during the  
 591 operation in faulty mode; the objective is to assess whether the  
 592 drive components are able to withstand the thermal stresses that  
 593 produce transient currents during the fault and reconfiguration  
 594 period; and also assess the possible reduction in the rated power  
 595 of the converter when operating in faulty mode. The authors  
 596 perform the analysis on a single but actual topology of a fault-  
 597 tolerant inverter and develop a simple model to assess the  
 598 losses in all the components after an IGBT open-circuit fault  
 599 event, both during the fault, reconfiguration process, and faulty  
 600 operation. The model was validated experimentally by compar-  
 601 ing the sum of computed losses and the total losses measured  
 602 in the experimental rig. From the analysis, conclusions about  
 603 the maximum allowable time in faulty and reconfiguration  
 604 conditions or the maximum power after the reconfiguration are  
 605 discussed.

## ACKNOWLEDGMENT

606

The authors would like to thank the journal Editor-in-Chief, 607  
 Prof. Carlo Cecati, for having accepted their Special Session 608  
 proposal and for letting them led the process with confidence up 609  
 to its end. The authors also thank Sandra McLain, the journal 610  
 administrator, for her timely help anytime it was necessary 611  
 during both the reviewing process and the editorial conclusion. 612

GÉRARD-ANDRÉ CAPOLINO, *Guest Editor* 613  
 Department of Electrical Engineering 614  
 University of Picardie “Jules Verne” 615  
 80000 Amiens, France 616

JOSE A. ANTONINO-DAVIU, *Guest Editor* 617  
 Instituto de Ingeniería Energética 618  
 Polytechnic University of Valencia 619  
 46071 Valencia, Spain 620

MARTIN RIERA-GUASP, *Guest Editor* 621  
 Instituto de Ingeniería Energética 622  
 Polytechnic University of Valencia 623  
 46071 Valencia, Spain 624

## REFERENCES

625

- [1] A. Bellini and F. Filippetti, “Guest editorial, special section on 626  
 diagnostics—Part I,” *IEEE Trans. Ind. Electron.*, vol. 55, no. 12, 627  
 pp. 4106–4108, Dec. 2008. 628
- [2] A. Bellini and F. Filippetti, “Guest editorial, special section on 629  
 diagnostics—Part II,” *IEEE Trans. Ind. Electron.*, vol. 56, no. 11, 630  
 pp. 4532–4533, Nov. 2009. 631
- [3] G.-A. Capolino and H. Henao, “Guest editorial on diagnostics of electrical 632  
 machines, power electronics and drives,” *IEEE Trans. Ind. Electron.*, 633  
 vol. 58, no. 5, pp. 1463–1467, May 2011. 634
- [4] G.-A. Capolino and F. Filippetti, “Introduction to the special section 635  
 on advances in diagnosis for electrical machines, power electronics, 636  
 drives—Part I,” *IEEE Trans. Ind. Electron.*, vol. 60, no. 8, pp. 3396–3397, 637  
 Aug. 2013. 638
- [5] G.-A. Capolino and F. Filippetti, “Introduction to the special section 639  
 on advances in diagnosis for electrical machines, power electronics, 640  
 drives—Part II,” *IEEE Trans. Ind. Electron.*, vol. 60, no. 9, pp. 4009– 641  
 4011, Sep. 2013. 642
- [6] M. Riera-Guasp, J. A. Antonino-Daviu, and G.-A. Capolino, “Advances in 643  
 electrical machine, power electronic and drive condition monitoring and 644  
 fault detection: State of the art,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 645  
 Mar. 2015. 646
- [7] S. Choi, E. Pazouki, J. Baek, and H. R. Bahrami, “Iterative condition mon- 647  
 itoring and fault diagnosis scheme of electric motor for harsh industrial 648  
 application,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 649
- [8] A. Giantomassi, F. Ferracuti, S. Iarlori, G. Ippoliti, and S. Longhi, “Elec- 650  
 tric motor fault detection and diagnosis by kernel density estimation 651  
 and Kullback–Leibler divergence based on stator current measurements,” 652  
*IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 653
- [9] R. K. Singleton, II, E. G. Strangas, and S. Aviyente, “Extended Kalman 654  
 filtering for remaining-useful-life estimation of bearings,” *IEEE Trans.* 655  
*Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 656
- [10] J. Pons-Llinares *et al.*, “Advanced induction motor rotor fault diagno- 657  
 sis via continuous and discrete time–frequency tools,” *IEEE Trans. Ind.* 658  
*Electron.*, vol. 62, no. 3, Mar. 2015. 659
- [11] C. Yang *et al.*, “Screening of false induction motor fault alarms produced 660  
 by axial air ducts based on the space-harmonic-induced current compo- 661  
 nents,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 662
- [12] V. Climente-Alarcon, J. A. Antonino-Daviu, E. G. Strangas, and 663  
 M. Riera-Guasp, “Rotor-bar breakage mechanism and prognosis in 664  
 an induction motor,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 665  
 Mar. 2015. 666
- [13] F. Duan and R. Živanović, “Condition monitoring of an induction motor 667  
 stator windings via global optimization based on the hyperbolic cross 668  
 points,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 669



- 670 [14] P. Nussbaumer, M. A. Vogelsberger, and T. M. Wolbank, "Induction  
671 machine insulation health state monitoring based on online switch-  
672 ing transient exploitation," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3,  
673 Mar. 2015.
- 674 [15] L. Frosini, C. Harlişca, and L. Szabó, "Induction machine bearing faults  
675 detection by means of statistical processing of the stray flux measure-  
676 ment," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015.
- 677 [16] V. C. M. N. Leite *et al.*, "Detection of localized bearing faults in induction  
678 machines by spectral kurtosis and envelope analysis of stator current,"  
679 *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015.
- 680 [17] S. Hedayati Kia, H. Henao, and G.-A. Capolino, "Gear tooth sur-  
681 face damage fault detection using induction machine stator current  
682 space vector analysis," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3,  
683 Mar. 2015.
- 684 [18] E. Fournier *et al.*, "Current-based detection of mechanical unbalance in  
685 an induction machine using spectral kurtosis with reference," *IEEE Trans.*  
686 *Ind. Electron.*, vol. 62, no. 3, Mar. 2015.
- 687 [19] S. Nadarajan, S. K. Panda, B. Bhangu, and A. Kumar Gupta, "Hybrid  
688 model for wound-rotor synchronous generator to detect and diagnose turn-  
689 to-turn short-circuit fault in stator windings," *IEEE Trans. Ind. Electron.*,  
690 vol. 62, no. 3, Mar. 2015.
- 691 [20] F. R. Blázquez, M. Aranda, E. Rebollo, F. Blázquez, and C. A. Platero,  
692 "New fault-resistance estimation algorithm for rotor-winding ground-fault  
693 online location in synchronous machines with static excitation," *IEEE*  
694 *Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015.
- 695 [21] F. Immovilli, C. Bianchini, E. Lorenzani, A. Bellini, and E. Fornasiero,  
696 "Evaluation of combined reference frame transformation for interturn  
fault detection in permanent-magnet multiphase machines," *IEEE Trans.* 697  
*Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 698
- [22] B. Aubert, J. Régner, S. Caux, and D. Alejo, "Kalman-filter-based in- 699  
dicator for online interturn short circuits detection in permanent-magnet 700  
synchronous generators," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 701  
Mar. 2015. 702
- [23] S. M. Mirimani, A. Vahedi, F. Marignetti, and R. Di Stefano, "An online 703  
method for static eccentricity fault detection in axial flux machines," *IEEE* 704  
*Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 705
- [24] C. Chakraborty and V. Verma, "Speed and current sensor fault detection 706  
and isolation technique for induction motor drive using axes transforma- 707  
tion," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 708
- [25] J. G. Normiella *et al.*, "Coupling inductor fault detection and estimation 709  
in three-phase adjustable-speed drives with direct power control-based 710  
active front-end rectifiers," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 711  
Mar. 2015. 712
- [26] C. Choi, K. Lee, and W. Lee, "Observer-based phase-shift fault detection 713  
using adaptive threshold for rotor position sensor of permanent-magnet 714  
synchronous machine drives in electromechanical brake," *IEEE Trans.* 715  
*Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 716
- [27] M. A. Rodríguez-Blanco *et al.*, "Fault detection for IGBT using adap- 717  
tive thresholds during the turn-on transient," *IEEE Trans. Ind. Electron.*, 718  
vol. 62, no. 3, Mar. 2015. 719
- [28] A. Stabile, J. O. Estima, C. Boccaletti, and A. J. Marques Cardoso, 720  
"Converter power loss analysis in a fault-tolerant permanent-magnet 721  
synchronous motor drive," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 722  
Mar. 2015. 723



**Gérard-André Capolino** (A'77–M'82–SM'89–F'02) was born in Marseille, France. He 724  
received the B.Sc. degree in electrical engineering from the Ecole Centrale de Marseille, 725  
Marseille, in 1974, the M.Sc. degree from the Ecole Supérieure d'Electricité, Paris, 726  
France, in 1975, the Ph.D. degree from the Aix-Marseille University, Marseille, in 1978, 727  
and the D.Sc. degree from the Institut Polytechnique de Grenoble, Grenoble, France, 728  
in 1987. 729

In 1994, he joined the University of Picardie "Jules Verne," Amiens, France, where he 730  
is currently a Chair Professor of electrical engineering. 731

Dr. Capolino is an Associate Editor of the IEEE TRANSACTIONS ON POWER ELEC- 732  
TRONICS, IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS, and IEEE ACCESS. He 733  
is also the acting Chair for the Steering Committee of the International Conference on 734  
Electrical Machines (ICEM). He was the recipient of the 2008 IEEE-IES Dr.-Ing. Eugene 735  
Mittelmann Achievement Award, the 2010 ICEM Arthur Ellison Achievement Award, and 736  
the 2011 IEEE-PELS Diagnostics Achievement Award. 737



**Jose A. Antonino-Daviu** (M'06–SM'12) received the M.Sc. and Ph.D. degrees in 738  
electrical engineering from the Universitat Politècnica de València, Valencia, Spain, in 739  
2000 and 2006, respectively. 740

He worked in the private sector, having been involved in several international projects. 741  
Currently, he is an Associate Professor with the School of Industrial Engineering, 742  
Universitat Politècnica de València. His primary research interests include condition 743  
monitoring of electric machines, wavelet theory and its application to fault diagnosis, 744  
and design and optimization of electrical installations and systems. 745



746  
747  
748  
749  
750  
751  
752



**Martin Riera-Guasp** (M'94–SM'12) received the M.Sc. degree in industrial engineering and the Ph.D. degree in electrical engineering from the Universitat Politècnica de València, Valencia, Spain, in 1981 and 1987, respectively.

Currently, he is an Associate Professor with the Department of Electrical Engineering, Universitat Politècnica de València. His research interests include condition monitoring of electrical machines, applications of signal analysis techniques to electrical engineering, and efficiency in electric power applications.

## AUTHOR QUERIES

AUTHOR PLEASE ANSWER ALL QUERIES

AQ1 = Please check if provided definition for DSP is correct. Otherwise, please make the necessary corrections.

AQ2 = Please check if provided definition for MCSA is correct. Otherwise, please make the necessary corrections.

END OF ALL QUERIES

IEEE  
Proof

# Modern Diagnostics Techniques for Electrical Machines, Power Electronics, and Drives

## I. INTRODUCTION

FOR THE last ten years, at least three different Special Sections dealing with diagnostics in power electrical engineering have been published in the IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS [1]–[5]. All of them had their specificities, but the last ones, starting in 2011, were more connected to relevant events organized on the topic. In fact, these events have been clearly the only international forums fully dedicated to diagnostics techniques in power electrical engineering. For this particular issue, it has been decided to separate the different submissions into six parts:

- state of the art;
- general methods;
- induction machines (IMs);
- synchronous machines;
- electrical drives;
- power components and power converters.

The second section includes only one state-of-the-art paper, which is dedicated to actual techniques implemented in both industry and research laboratories. The third section includes three papers on diagnostic techniques not specifically aimed at a particular type of machine. The fourth section includes three papers devoted to diagnostics of rotor faults, two dedicated to stator insulation issues, and four papers dealing with mechanical faults diagnosis in IMs. The fifth section includes papers focusing on different types of synchronous machines. The first two papers deal with wound-rotor synchronous machines, the following three papers are dedicated to permanent-magnet radial flux machines, and the last one deals with permanent-magnet axial flux machines. Regarding the types of faults analyzed, there are three papers devoted to the diagnosis of interturn short circuits in the stator windings, i.e., one dedicated to the detection and location of field-winding-to-ground faults and a paper devoted to the diagnosis of static eccentricities. In the sixth section, two papers investigate issues related to faults in drive sensors, and one is devoted to fault detections in the coupling inductors. The last section includes two papers devoted to diagnosis of faults and losses analysis in switching components of power converters.

## II. STATE OF THE ART

In [6], the authors have screened the most recent papers published on the topic to draw the real “state of the art” on condition monitoring and fault detection of rotating electrical

machines, drives, and power electronics. As expected, since it is the most investigated electrical machine from the very beginning, a large part of the development has been dedicated to IMs. It is well known that most of the methods developed for IMs can be simply used directly or adapted for other types of rotating electrical machines or even for linear actuators or generators.

A large part of this paper is dedicated to IM fault detection since it has been the historical field of investigation for the last 30 years or so. In this way, rotor faults have been under focus mainly for squirrel-cage IMs with convenient signal processing techniques to tackle the fact that many faults cannot be detected easily when the machine load is light. The second largest part dealing with the IM fault detection is related to stator winding, including the insulation degradation and further early stage short circuits. It has been shown that the insulation degradation detection is the best way to prevent short circuits, but it is the most difficult to be implemented online. Moreover, early stage short circuits are easier to detect particularly by the use of a stray flux sensor, which is simple, cheap, and noninvasive for large-power IMs. Other methods to detect early stage short circuits are based on the impedance asymmetry on the stator side. In this last case, the sensors are based on both stator voltages and stator currents measurements. Then, the decision process for early stage short-circuit detection can be based on advanced artificial intelligence techniques, which are well known in this specific area. Finally, in the case of IMs, methods for mechanical failures detection have been investigated. Faults such as eccentricities, bearings, and gearboxes have been under focus. On the other hand, a brief analysis of the ongoing research in the field of multiphase IMs has been pointed out.

The same approach has been presented for permanent-magnet synchronous machines (PMSMs) or even synchronous generators (SGs) but with a shorter description since the main features of the IMs fault detection can be applied in the same way for PMSMs. However, the detection of demagnetization has been added as an important point specific to these machines. As in the case of IMs, a brief analysis of the ongoing research in the field of multiphase PMSMs has also been developed.

The last part of this paper has been dedicated to fault detection in power converters and power components as a part of diagnostic techniques associated with power electronics. For the power converters, specific techniques have been developed in order to speed up the detection process in order to avoid components breakage. These techniques have been successfully applied to inverters, matrix converters, and even to dc–dc converters. The problem of fault detection in dc link capacitors has also been analyzed. For the power components, things are much more difficult since they have fast switching capabilities and the



95 fault detection has to be as fast as possible. Therefore, the fault  
 96 detection techniques have been applied to both insulated-gate  
 97 bipolar transistors (IGBTs) and MOSFETs in order to protect  
 98 them from irreversible failures. In the same way, the very last  
 99 part of this paper is dedicated to fault-tolerant drives for which  
 100 multilevel and multiphase topologies have been developed in  
 101 the last ten years.

102

### III. GENERAL METHODS

103 In [7], a robust electric motor fault decision-making algo-  
 104 rithm, particularly suited for harsh industrial environments, is  
 105 presented. The proposed technique is based on the simultaneous  
 106 utilization of multiple fault signature patterns, noise signal fre-  
 107 quency patterns, and fundamental harmonics current frequency  
 108 patterns in a whole motor current signal for diagnosis purposes.  
 109 As the authors pointed out, the identified pattern is proven to be  
 110 robust to the signal distortion and inherent monitor noise during  
 111 motor dynamic operation. In this paper, it is mathematically and  
 112 experimentally proven that the proposed diagnosis algorithm  
 113 provides highly accurate monitoring performance while mini-  
 114 mizing both false detection and missing detection rates under  
 115 high noise and nonlinear machine operating conditions. The  
 116 experimental results are obtained with a DSP-based IM drive  
 117 system, where motor control and fault diagnosis are performed  
 118 in real time. The faulty conditions considered in the work are  
 119 broken rotor bars and eccentricities. The authors include some  
 120 comments regarding its possible constraints related to industrial  
 121 applicability of the proposed technique, stating that since the  
 122 proposed method assumes prior knowledge of harmonics in  
 123 a motor current spectrum, small additional memory might be  
 124 required to implement the proposed method. In addition, a suf-  
 125 ficient frequency bandwidth of data acquisition and motor con-  
 126 trol is required, particularly for high-frequency signal detection.  
 127 In [8], a new online diagnosis of three-phase IM stator  
 128 faults using a signal-based method is proposed. The proposed  
 129 technique starts with a data preprocessing stage, in which prin-  
 130 cipal component analysis (PCA) is applied to current signals.  
 131 PCA enables the reduction of the three-phase currents space  
 132 to a two-dimensional space. Afterward, features are extracted  
 133 from PCA-transformed data using the kernel density estimation  
 134 (KDE) improved by fast Gaussian transform along with a point  
 135 reduction method. The automatic fault identification is achieved  
 136 by means of Kullback–Leibler divergence (KLD), which is used  
 137 as an index to identify the dissimilarity between two probability  
 138 distributions. The final goal is to ensure that the developed  
 139 technique can be used for online monitoring; this is possible due  
 140 to the remarkable computational cost reduction obtained with  
 141 the aforementioned enhancement techniques, in comparison  
 142 with the standard KDE. In this regard, before presenting their  
 143 developed algorithm, the authors perform a thorough descrip-  
 144 tion and analysis of the considered techniques, namely, PCA,  
 145 KDE, improved KDE by fast Gaussian transform, and point  
 146 reduction and KLD. This paper also includes experimental  
 147 results obtained with two different IMs and under three different  
 148 fault conditions: cracked rotor, out-of-tolerance geometry rotor,  
 149 and backlash. The tests are carried out at different load and  
 150 voltage levels to prove the proposed method effectiveness. The

authors emphasize that it is totally signal based since no IM 151  
 parameters are required. 152

In [9], a stochastic modeling-based prognosis approach 153  
 [extended Kalman filter (EKF)] is proposed for tracking the 154  
 remaining useful life (RUL) of bearings under different oper- 155  
 ating conditions. The proposed data-driven methodology relies 156  
 on both time and time–frequency domain features of vibration 157  
 signals obtained from the PROGNOSTIA platform. In this 158  
 regard, the authors reach original conclusions on the better suit- 159  
 ability of different features for different operating conditions 160  
 depending on the length of the test data set. For instance, the 161  
 authors show that the entropy feature is successful at detecting 162  
 the early stages of degradation, whereas the variance feature 163  
 is not very informative until the final failure stage. As the 164  
 authors point out, shorter test data sets provide less information 165  
 for RUL estimation yielding higher error rates, which is in 166  
 concordance with the conclusions of other works based on the 167  
 same data set. Once features have been extracted, an analytical 168  
 function, which best approximates the evolution of the fault, 169  
 is determined and used to learn the parameters of the EKF. In 170  
 this regard, the work gives a detailed description of the RUL 171  
 estimation based on EKF, and unlike other investigations, also 172  
 provides a procedure to estimate the confidence interval along 173  
 with the RUL estimates. The algorithm is finally applied to 174  
 bearing vibration data obtained from the mentioned platform, 175  
 illustrating the convergence of the algorithm, as well as its be- 176  
 havior under different conditions. The work includes a compar- 177  
 ison of EKF versus the regular KF showing better performance 178  
 of the proposed approach for all operating conditions. 179

### IV. IMs

180

In [10], a detailed comparison between the two main groups 181  
 of transforms that are employed for IMs rotor assessment based 182  
 on transient analysis (continuous versus discrete transforms) 183  
 is presented. In this paper, the discrete wavelet transform and 184  
 the short-time Fourier transform are taken as representatives 185  
 of each respective group. The work begins with an overall 186  
 revision of the diagnosis based on transient analysis and the 187  
 inherent benefits that such methodology brings in comparison 188  
 to the conventional motor current signature analysis (MCSA) 189  
 approach. The authors remark on its usefulness in cases where 190  
 the MCSA may lead to incorrect diagnostic conclusions. A 191  
 detailed description of the operation of each group of trans- 192  
 forms is presented making special emphasis on aspects as 193  
 fault severity quantification or computational burden. In this 194  
 regard, the authors emphasize the following advantages of 195  
 the continuous tools versus their discrete counterparts: clearer 196  
 extraction of the low-frequency fault components evolutions, 197  
 possibility of tracking the high-order harmonics evolutions, 198  
 and easier fault discrimination. Afterward, the authors show 199  
 the results of applying each transform to data obtained with 200  
 real IMs. These results do not only consider trivial fault sit- 201  
 uations, where the conventional MCSA also works well, but 202  
 also some of the controversial cases, where the application 203  
 of the conventional methods often leads to false diagnostics, 204  
 namely, outer bar breakages in double cage IMs, IMs with rotor 205  
 axial duct influence, as well as combined faults. The authors 206

AQ2

207 present a detailed discussion of the performance of each group  
208 of transforms based on their results concerning aspects such as  
209 quantification or computational time. In their conclusions, they  
210 ratify the aforementioned advantages of the continuous tools,  
211 and they also tear down the false myth concerning the higher  
212 computational burden of continuous transforms.

213 In [11], the authors analyze a diagnostic problem related to  
214 IMs with special magnetic structures. More specifically, this  
215 paper deals with the false broken rotor bar alarms that have been  
216 reported in cage IMs with a number of rotor axial ducts equal to  
217 the number of poles. In such cases, even in healthy conditions,  
218 two sidebands appear around the fundamental component; their  
219 frequencies are equal to those produced by a broken bar. This  
220 problem is documented through the analysis of three high-  
221 voltage IMs working in actual industrial applications that were  
222 misdiagnosed. The authors analyze the theoretical origin of this  
223 issue and conclude that the confusing sidebands are produced  
224 by the periodical variations of reluctance that the fundamen-  
225 tal flux wave undergoes during its relative rotation along the  
226 cross section of the rotor. Once the physical phenomenon is  
227 explained, the authors propose a diagnosis method based on the  
228 current sidebands originated by the fifth and seventh space har-  
229 monics of the flux wave. The authors state that these high-order  
230 harmonics hardly penetrate the rotor core and, consequently,  
231 are not affected by the rotor axial air ducts. This hypothesis is  
232 experimentally verified using specifically built prototypes.

233 In [12], the results of a fatigue test that is intended to  
234 reproduce, in the most natural way possible, the exposed rotor  
235 bar breakage process in an IM. For this purpose, a 1.5-kW  
236 two-pole squirrel-cage IM is monitored along 82 265 identical  
237 working cycles, each one comprising a heavy start-up, a pe-  
238 riod of stationary operation at rated load and, finally, a plug  
239 stopping. To accelerate the breakage process, one of the rotor  
240 rings was mechanized in order to weaken the junction between  
241 the end-ring and the bars. In addition, an incipient breakage  
242 was forced in one of the rotor bars. Afterward, the working  
243 cycle was repeated until the bar naturally cracked. Taking as  
244 bases the results of these tests, the authors carry out three  
245 different analyses. First, they compare the performances of sev-  
246 eral fault indicators described in the literature for tracking the  
247 fault components evolutions; transient and steady-state-based  
248 parameters are considered in this study. Second, an explanation  
249 of the breakage mechanism is given, based on a series of  
250 pictures of the breakage region, which were taken during the  
251 breakage development. Third, a physical model of the failure  
252 is introduced and, based on this model, the authors propose  
253 an algorithm for state estimation and prognosis analysis of the  
254 bars health.

255 In [13], a diagnostic method based on parameter estimation,  
256 which is applied to the detection of interturn short circuits in  
257 IMs, is proposed. The detection algorithm is based on three  
258 blocks that are cyclically executed: The first block is a coupled  
259 circuits model of the IM, able to simulate faults in the stator  
260 windings; in this model, the faults are characterized by three  
261 parameters ( $\mu f$ : fault location;  $\mu s$ : severity of the fault; LL:  
262 load level). The second block is an objective function whose  
263 value depends on the errors between the measured currents  
264 and the currents calculated by the model. The third block is a

global optimization algorithm, called hyperbolic cross points  
algorithm. It efficiently seeks the combination of parameter  
values, which minimize the objective function under the tested  
operation conditions. The authors claim that the proposed al-  
gorithm reliably locates, with a reduced number of iterations,  
the global minimum of the objective function, avoiding errors  
due to local minima. The state of the IM, i.e., the severity and  
location of the fault, is characterized by the set of parameters  
that lead to the global minimum of the objective function. The  
authors validate the method by simulations and laboratory tests,  
showing that it can detect a fault affecting 8% of the turns of a  
phase with a processing time of 106 s.

276  
277 In [14], a method for monitoring the insulation health of  
IMs is proposed. As the authors highlight, the objective of  
this work is not to detect sudden insulation faults but to ob-  
serve a trend of the insulation state indicator over time. The  
method is applicable to IMs fed by voltage-source inverters. It  
relies on an offline test, which consists of applying a voltage  
step, obtained by switching the inverter, to the tested phase.  
The subsequent reaction current is recorded and employed to  
evaluate the winding condition. This current is based on high-  
frequency oscillations, which vanish after a few microseconds.  
It is shown that the current evolution depends on the parasitic  
turn-to-turn and winding-to-ground capacitances that change  
during the aging process of the insulation. The authors propose  
two insulation state indicators, which are intended for phase  
evaluation (ISI) and global winding evaluation (SISI). These  
parameters are computed comparing the current spectra and  
reference spectra, obtained in healthy condition. The method  
is validated on two quite different IMs, rated 280 V, 5.5 kW and  
1428 kW, 2183 V, respectively.

295  
296 In [15], a new technique based on stray flux measurement is  
proposed for bearing fault detection in IMs. The method relies  
on the statistical processing of the measurements of this quan-  
tity in different positions around the IM. The usefulness of the  
proposed method is mainly justified based on the simplicity and  
the flexibility of the custom flux probe with its amplification  
and filtering stage. The authors first present a detailed literature  
survey about the use of stray flux measurement in the IMs fault  
diagnosis area, emphasizing the advantages of such approach  
in comparison with other techniques. Afterward, their proposed  
method is described; it requires at least ten data acquisitions of  
the stray flux, performed under identical conditions, both for  
the healthy machine (considered as reference) and the same  
machine having diverse bearing faults. The authors prove the  
validity of the method in a real IM, considering three different  
types of bearing failure (crack in the outer race, hole in the  
outer race, and deformation of the seal) under different load  
conditions. In addition, different positions for the flux mea-  
surement with their custom probe are considered, as well as a  
comparison with a commercial probe, leading to a total number  
of 32 analyzed cases. Their subsequent discussions lead to  
interesting conclusions as to the suitability of the method even  
to detect damages in the bearing seal, the good performance  
of their probe for higher loads or the general higher effectivity  
of the custom probe versus the commercial one for stray flux  
measurements, among others. The only requisite of the method  
is that it needs an initial data set as "healthy reference" for

323 comparisons to the successive measurements during the IM  
324 lifetime.

325 In [16], a methodology for diagnosing localized defects in  
326 the outer race of IM bearings is introduced. The method relies  
327 on the spectral analysis of the squared envelope of the stator  
328 current in an optimized frequency band, characterized by a  
329 central frequency  $f_c$  and a bandwidth  $Bw$ , which contains the  
330 nonstationary components with frequencies related to fault. The  
331 optimum frequency interval is selected using the kurtogram of  
332 the current as a decision tool: it simply consists of selecting the  
333 central frequency/bandwidth combination that maximizes the  
334 spectral Kurtosis in the kurtogram. Advanced algorithms such  
335 as the fast kurtogram or the wavelet kurtogram are used in this  
336 work to compute the kurtogram in a computationally efficient  
337 way. The method is validated by means of laboratory tests,  
338 using two bearings with forced faults, consisting of holes with  
339 different diameters. Under these strong defect conditions, this  
340 technique enables a clear detection of the fault components,  
341 although as the authors state, the method needs to be validated  
342 with small and real defects.

343 In [17], the authors have presented the gear tooth damage  
344 fault detection using the IM as a sensor but measuring its stator  
345 currents. The basic principle is to use the torque oscillations  
346 as a means to bring to the IM currents the image of what is  
347 happening in the mechanical part related to the machine shaft.  
348 Therefore, the electromagnetic torque has been developed as  
349 a mean part plus an oscillation part for both healthy and faulty  
350 cases and characteristic frequencies of the oscillating parts  
351 have been identified. A simplified model of the mechanical part  
352 has been developed to compute these characteristic frequencies  
353 from a theoretical point of view and to relate them to the IM  
354 currents. In order to detect the different frequencies related to  
355 the mechanical failure, a fault profile reconstruction has been  
356 defined and a fault index has been proposed. The proposed  
357 methodology has been applied to a simple test rig with a  
358 three-phase IM connected by its shaft to a pinion and a wheel  
359 with very small surface wear damage on one tooth for each  
360 part. Both simulation and experimental results have confirmed  
361 the validity of this new technique of mechanical fault detection.

362 In [18], a method called spectral kurtosis with reference is  
363 employed to design a system's healthy reference. This approach  
364 is afterward evaluated for mechanical unbalance detection in  
365 IMs using the stator currents instantaneous frequency. As the  
366 authors explain, the definition of a healthy reference enables  
367 the computation of normalized fault indicators whose values  
368 are independent of the system characteristics. This means a  
369 significant advantage when diagnosing systems with different  
370 power, coupling, inertia, and load. In this paper, the authors re-  
371 view the concept of kurtosis and demonstrate its ability to detect  
372 outliers within a reference distribution. They introduce a new  
373 kurtosis-based indicator,  $SK_R$ , which includes a new reference  
374 set, and they prove its ability to generate a system's healthy  
375 reference and to detect any drift from it. The authors evaluate  
376 this indicator using synthetic signals and also experimentally  
377 verify its efficiency when applied to the current instantaneous  
378 frequency for the detection of low levels of mechanical unbal-  
379 ance. Their results prove the  $SK_R$  detection capacity with a  
380 single fault threshold for a wide range of load conditions and

ratify the usefulness of creating a system's healthy reference for 381  
the robust detection of weak mechanical unbalances, avoiding 382  
false alarms for different operating conditions and showing a 383  
great robustness against load variations. 384

## V. SYNCHRONOUS MACHINES 385

In [19], an SG model that enables the simulation of stator 386  
interturn short circuits is presented. The novelty of this work is 387  
that it develops a hybrid model, in which the Winding Function 388  
Approach (WFA) is combined with the  $dq0$  transform. As the 389  
authors remark, the proposed model takes advantage of the 390  
suitability of WFA for detailed and simple representation of 391  
the faults and, at the same time, enables the calculation simplic- 392  
ity that is provided by the  $dq0$  representation. Consequently, a 393  
very precise model that is suitable to run online is achieved. In 394  
addition, this model accounts for the effect of local saturation of 395  
the magnetic circuit due to the fault currents. Local saturation 396  
and saliency are taken into consideration through a modified 397  
airgap function, which facilitates the accurate computation of 398  
the inductance of the shorted turns. The model is extensively 399  
validated by laboratory tests and compared with a model based 400  
on the  $dq0$  transform. The authors conclude that the proposed 401  
model provides more accurate results than the  $dq0$  model 402  
although its performance with incipient faults needs to be 403  
improved. 404

The work presented in [20] deals with the accurate local- 405  
ization of field-winding to ground faults in SGs. First, the 406  
authors analyze in detail a previously developed method for 407  
the online detection of excitation-system faults to ground that 408  
is valid for generators with static excitation. The method allows 409  
discriminating if the fault takes place in the ac side or in the dc 410  
side of the excitation system. In the event of faults in the dc 411  
the method approximately forecasts the location of the fault in 412  
the excitation winding. However, this procedure depends on the 413  
value of the fault resistance  $R_f$ , which has to be estimated; this 414  
fact leading to a wide margin of indetermination. The main 415  
contribution of this work is a new algorithm that, from the 416  
measured quantities, accurately calculates the value of the fault 417  
resistance  $R_f$ . The method is validated through laboratory tests 418  
and also on a 106-MW SG operating under real conditions in 419  
a hydroelectric power plant. From the test results, the authors 420  
claim that the proposed method for the computation of  $R_f$  421  
significantly reduces the errors in the fault location; this fact is 422  
relevant in hydrogenerators with high number of poles, since it 423  
reliably enables the location of the pole where the fault occurs. 424  
This way, the extraction of the whole rotor can be avoided, thus 425  
substantially reducing repair costs. 426

In [21], the authors introduce an approach for interturn short- 427  
circuit diagnosis in five-phase PMSMs. The approach relies on 428  
the spectral analysis of the modulus of a space vector  $\vec{D}$ . This 429  
vector is obtained as a combination of two space vectors that 430  
are calculated from the measured phase voltages but using two 431  
different reference frames, named  $\alpha\beta$  and  $\alpha2\beta2$ . It is justified 432  
that an interturn fault in one of the stator phases produces an 433  
increase in the  $DC$  and  $2fs$  components in the spectrum of 434  
the modulus of the space vector  $\vec{D}$  ( $fs$  : supply frequency 435  
fundamental harmonic). It is shown from simulations and tests 436



437 that this signature is very sensible, reaching amplitude incre-  
438 ments in the fault-related harmonics higher than 15 dB for  
439 a fault affecting up to 3% of the turns of a phase; and it is  
440 also clearly different from the signatures produced by other  
441 kind of faults (as static or dynamic eccentricity and partial  
442 demagnetization), thus enabling a robust and reliable diagnosis  
443 of interturn short-circuit faults.

444 The work presented in [22], as in the previous paper, deals  
445 with interturn short-circuit detection in PMSMs. In this case,  
446 the work is focused on three-phase PMSMs working under  
447 high variable load and speed conditions, as it happens in  
448 aircraft applications. This work proposes an approach based on  
449 parameter identification. The authors introduce a PMSM model  
450 based on the  $dq$  reference frame, where the short-circuited turns  
451 ratios of each phase ( $n_{s/cA}, n_{s/cB}, n_{s/cC}$ ) are the parameters  
452 to be identified. The estimation of these parameters is carried  
453 out using the EKF, which is justified to be a suitable tool that  
454 enables to perform accurate estimations in real time, even under  
455 continuous and substantial changes in the operation conditions.  
456 Finally, the fault indicators are defined as the average value  
457 of the estimated short-circuited turns ratios calculated over a  
458 sliding window with a length equal to half period of the main  
459 component. The approach is extensively validated by simula-  
460 tion and laboratory tests; it is demonstrated to be robust against  
461 frequency variations, load variations, power factor variations,  
462 load unbalances, and harmonic content variations.

463 Reference [23] is the only paper in this Special Section  
464 dealing with axial flux PMSMs. In this paper, the authors  
465 introduce a method for diagnosing static eccentricities in axial  
466 flux PMSMs. The method requires the installation of three  
467 search coils, mounted on three stator teeth shifted  $120^\circ$ . First,  
468 a parameter named static eccentricity factor (SEF) is defined  
469 in order to characterize the fault severity in such type of  
470 machines; then, a simple algorithm is theoretically justified  
471 that enables calculation of the SEF, and also the position of  
472 minimum airgap in a faulty machine, using the measured back  
473 electromotive forces in the search coils. It is interesting that  
474 the computed SEF depends neither on the rotor speed nor on  
475 the load. The approach is extensively validated via simulations,  
476 using a 3-D finite-element software, as well as thorough labo-  
477 ratory tests.

## 478 VI. ELECTRICAL DRIVES

479 In [24], a new fault detection and isolation technique is pre-  
480 sented with the aim of making the traditional vector-controlled  
481 IM drive fault tolerant against current and speed sensor failure.  
482 The underlying idea is that the controller keeps estimating  
483 the different currents and the speed and, in case of a fault, it  
484 switches to the correct estimated value. On the one hand, the  
485 proposed technique extracts eight estimates of currents in the  
486  $\alpha - \beta$  reference frame (the authors obtain four estimates using  
487 the reverse transformation from  $d-q$  to  $\alpha - \beta$  and the other  
488 four using the forward transformation from  $a-b-c$  to  $\alpha - \beta$ ).  
489 In this context, the concept of vector rotation is introduced to  
490 decide the correct estimated value of current corresponding to a  
491 fault. On the other hand, the speed is estimated by modifying  
492 one of the available model reference adaptive system-based

formulations (X-based MRAS). Both simulations, as well as 493  
494 experiments carried out with a laboratory prototype, demon- 494  
495 strate that the system is capable of detecting a fault and recon- 495  
496 figure itself in a seamless manner. In this regard, the authors 496  
497 thoroughly evaluate the performance of the proposed algorithm 497  
498 under different faulty conditions of the considered sensors. 498  
499 The results prove that proposed technique works well even in 499  
500 the case of multiple sensor failures and does not require any 500  
501 additional sensor. The developed fault-tolerant controller can 501  
502 be particularly useful for applications such as electric vehicles 502  
503 to avoid complete shutdown of the system, in case of sensor 503  
504 failure. 504

In [25], the detection of incipient faults in coupling inductors 505  
506 used in three-phase adjustable-speed drives with direct power 506  
507 control-based active front-end rectifiers is considered. More 507  
508 specifically, the authors develop a new strategy for early fault 508  
509 detection in coupling inductors, which enables a fast identi- 509  
510 fication of the defective phase while providing an accurate 510  
511 estimation of the inductance value of the coupling inductors that 511  
512 enhances the performance of the direct power control method. 512  
513 The underlying idea is that coupling inductor faults (e.g., an 513  
514 interturn short circuit) lead to a variation in the value of the 514  
515 coupling inductance. Hence, the goal is to detect the fault by 515  
516 tracking estimations of the coupling inductances associated 516  
517 with a fault in each phase. A detailed description of the full 517  
518 estimation procedure is given in this paper. Both simulation 518  
519 and experimental tests demonstrate the validity of the proposed 519  
520 method. As stated in this paper, the detection of the fault 520  
521 enables the suspension of the service if this is required to 521  
522 avoid a major breakdown. In addition, the identification of the 522  
523 affected phase enables the replacement of only the defective 523  
524 inductor if three single-phase chokes are used or helps with 524  
525 the repair of the nonhealthy winding if a three-phase reactor is 525  
526 used. Among the claimed advantages of the proposed method 526  
527 are the simplicity, speed, and effectiveness. On the other hand, 527  
528 the main constraint relies on the manufacturing tolerance of 528  
529 the inductors, which makes their actual values differ from 529  
530 each other including when there are not any faults. This latter 530  
531 issue, however, does not affect the robustness of the presented 531  
532 strategy. 532

In [26], an observer-based fault detection method is designed 533  
534 for the rotor position sensor of PMSM drives in an elec- 534  
535 tromechanical brake (EMB). To this end, the authors develop 535  
536 a position estimation algorithm with a full-order Luenberger 536  
537 observer for the rotor flux linkage. However, there are some 537  
538 deviations between the observer and the real process caused by 538  
539 model uncertainties and parameter variations. To overcome this 539  
540 drawback, the authors add a crucial feature in their detection 540  
541 method that relies on an adaptive threshold; this is determined 541  
542 by analyzing position estimation errors of the observer. The 542  
543 adaptive threshold enables, among other things, avoidance of 543  
544 missing or false alarms. The experimental results using the 544  
545 EMB test bench prove the effectiveness and robustness of the 545  
546 designed method that can even detect a small amount of phase 546  
547 shift fault within a wide operation range, not only at steady state 547  
548 but also under transient operation. Moreover, the fault-tolerance 548  
549 capability of the proposed method is achieved by introducing a 549  
550 compensation algorithm for the phase shift. The experimental 550

551 results show that this compensation algorithm is useful for  
 552 tolerating the phase shift fault. For other types of rotor position  
 553 sensor faults, the authors propose potential solutions that can  
 554 overcome low-speed limitation issues, such as the incorporation  
 555 with a high-frequency injection-based method. This latter ap-  
 556 proach can be somehow complementary to that proposed in the  
 557 work, since each of them shows special suitability for different  
 558 speed ranges.

## 559 VII. POWER COMPONENTS AND POWER CONVERTERS

560 In [27], an adaptive threshold-based approach is also pre-  
 561 sented, but in this case it is to design an electronic failure detec-  
 562 tion system applied to the IGBT. More specifically, the method  
 563 proposed by the authors relies on the direct measurement of  
 564 behavior of the gate signal during the IGBT turn-on transient  
 565 via continuous processing using analog and digital electronics.  
 566 The main goal pursued with an early fault detection design in  
 567 the IGBT is to obtain a corrective action to prevent propagation  
 568 of the fault to the complementary device in the same affected  
 569 leg in the inverter-motor system, when a short circuit or an  
 570 overcurrent occurs. Two different faults are considered in the  
 571 work: open-circuit and short-circuit failures. The considered  
 572 stages of the developed diagnosis scheme are improved resid-  
 573 ual generation stage, ramp rate, and a symmetrical adaptable  
 574 thresholds stage. The final scheme is intended to decrease the  
 575 false alarm rate by the aforementioned failures. To achieve the  
 576 early fault detection, the proposed circuit is implemented in  
 577 the gate driver using analog electronics. As the authors point  
 578 out, the main advantage of adding detection process with adap-  
 579 tive threshold is that the false alarm rate decreases because the  
 580 system is not so vulnerable to variations in the power supply  
 581 of the IGBT gate driver circuit. On the other hand, the main  
 582 limitation is that the proposed design is not suitable for power  
 583 applications, where the switching frequency is above 20 kHz  
 584 since the introduction of an external resistance limits the IGBT  
 585 switching speed.

586 In [28], a methodology to analyze the losses in the converters  
 587 of fault-tolerant drives is presented. This work aims to evaluate  
 588 the losses in the power components of the converter (IGBT,  
 589 diodes, capacitors) during the time the fault takes place, during  
 590 the subsequent reconfiguration process and, finally, during the  
 591 operation in faulty mode; the objective is to assess whether the  
 592 drive components are able to withstand the thermal stresses that  
 593 produce transient currents during the fault and reconfiguration  
 594 period; and also assess the possible reduction in the rated power  
 595 of the converter when operating in faulty mode. The authors  
 596 perform the analysis on a single but actual topology of a fault-  
 597 tolerant inverter and develop a simple model to assess the  
 598 losses in all the components after an IGBT open-circuit fault  
 599 event, both during the fault, reconfiguration process, and faulty  
 600 operation. The model was validated experimentally by compar-  
 601 ing the sum of computed losses and the total losses measured  
 602 in the experimental rig. From the analysis, conclusions about  
 603 the maximum allowable time in faulty and reconfiguration  
 604 conditions or the maximum power after the reconfiguration are  
 605 discussed.

## ACKNOWLEDGMENT

606

The authors would like to thank the journal Editor-in-Chief, 607  
 Prof. Carlo Cecati, for having accepted their Special Session 608  
 proposal and for letting them led the process with confidence up 609  
 to its end. The authors also thank Sandra McLain, the journal 610  
 administrator, for her timely help anytime it was necessary 611  
 during both the reviewing process and the editorial conclusion. 612

GÉRARD-ANDRÉ CAPOLINO, *Guest Editor* 613  
 Department of Electrical Engineering 614  
 University of Picardie “Jules Verne” 615  
 80000 Amiens, France 616

JOSE A. ANTONINO-DAVIU, *Guest Editor* 617  
 Instituto de Ingeniería Energética 618  
 Polytechnic University of Valencia 619  
 46071 Valencia, Spain 620

MARTIN RIERA-GUASP, *Guest Editor* 621  
 Instituto de Ingeniería Energética 622  
 Polytechnic University of Valencia 623  
 46071 Valencia, Spain 624

## REFERENCES

625

- [1] A. Bellini and F. Filippetti, “Guest editorial, special section on 626  
 diagnostics—Part I,” *IEEE Trans. Ind. Electron.*, vol. 55, no. 12, 627  
 pp. 4106–4108, Dec. 2008. 628
- [2] A. Bellini and F. Filippetti, “Guest editorial, special section on 629  
 diagnostics—Part II,” *IEEE Trans. Ind. Electron.*, vol. 56, no. 11, 630  
 pp. 4532–4533, Nov. 2009. 631
- [3] G.-A. Capolino and H. Henao, “Guest editorial on diagnostics of electrical 632  
 machines, power electronics and drives,” *IEEE Trans. Ind. Electron.*, 633  
 vol. 58, no. 5, pp. 1463–1467, May 2011. 634
- [4] G.-A. Capolino and F. Filippetti, “Introduction to the special section 635  
 on advances in diagnosis for electrical machines, power electronics, 636  
 drives—Part I,” *IEEE Trans. Ind. Electron.*, vol. 60, no. 8, pp. 3396–3397, 637  
 Aug. 2013. 638
- [5] G.-A. Capolino and F. Filippetti, “Introduction to the special section 639  
 on advances in diagnosis for electrical machines, power electronics, 640  
 drives—Part II,” *IEEE Trans. Ind. Electron.*, vol. 60, no. 9, pp. 4009– 641  
 4011, Sep. 2013. 642
- [6] M. Riera-Guasp, J. A. Antonino-Daviu, and G.-A. Capolino, “Advances in 643  
 electrical machine, power electronic and drive condition monitoring and 644  
 fault detection: State of the art,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 645  
 Mar. 2015. 646
- [7] S. Choi, E. Pazouki, J. Baek, and H. R. Bahrami, “Iterative condition mon- 647  
 itoring and fault diagnosis scheme of electric motor for harsh industrial 648  
 application,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 649
- [8] A. Giantomassi, F. Ferracuti, S. Iarlori, G. Ippoliti, and S. Longhi, “Elec- 650  
 tric motor fault detection and diagnosis by kernel density estimation 651  
 and Kullback–Leibler divergence based on stator current measurements,” 652  
*IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 653
- [9] R. K. Singleton, II, E. G. Strangas, and S. Aviyente, “Extended Kalman 654  
 filtering for remaining-useful-life estimation of bearings,” *IEEE Trans.* 655  
*Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 656
- [10] J. Pons-Llinares *et al.*, “Advanced induction motor rotor fault diagno- 657  
 sis via continuous and discrete time–frequency tools,” *IEEE Trans. Ind.* 658  
*Electron.*, vol. 62, no. 3, Mar. 2015. 659
- [11] C. Yang *et al.*, “Screening of false induction motor fault alarms produced 660  
 by axial air ducts based on the space-harmonic-induced current compo- 661  
 nents,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 662
- [12] V. Climente-Alarcon, J. A. Antonino-Daviu, E. G. Strangas, and 663  
 M. Riera-Guasp, “Rotor-bar breakage mechanism and prognosis in 664  
 an induction motor,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, 665  
 Mar. 2015. 666
- [13] F. Duan and R. Živanović, “Condition monitoring of an induction motor 667  
 stator windings via global optimization based on the hyperbolic cross 668  
 points,” *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 669

- 670 [14] P. Nussbaumer, M. A. Vogelsberger, and T. M. Wolbank, "Induction machine insulation health state monitoring based on online switching transient exploitation," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 697
- 671
- 672
- 673
- 674 [15] L. Frosini, C. Harlişca, and L. Szabó, "Induction machine bearing faults detection by means of statistical processing of the stray flux measurement," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 698
- 675
- 676
- 677 [16] V. C. M. N. Leite *et al.*, "Detection of localized bearing faults in induction machines by spectral kurtosis and envelope analysis of stator current," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 699
- 678
- 679
- 680 [17] S. Hedayati Kia, H. Henao, and G.-A. Capolino, "Gear tooth surface damage fault detection using induction machine stator current space vector analysis," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 700
- 681
- 682
- 683
- 684 [18] E. Fournier *et al.*, "Current-based detection of mechanical unbalance in an induction machine using spectral kurtosis with reference," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 701
- 685
- 686
- 687 [19] S. Nadarajan, S. K. Panda, B. Bhangu, and A. Kumar Gupta, "Hybrid model for wound-rotor synchronous generator to detect and diagnose turn-to-turn short-circuit fault in stator windings," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 702
- 688
- 689
- 690
- 691 [20] F. R. Blázquez, M. Aranda, E. Rebollo, F. Blázquez, and C. A. Platero, "New fault-resistance estimation algorithm for rotor-winding ground-fault online location in synchronous machines with static excitation," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 703
- 692
- 693
- 694
- 695 [21] F. Immovilli, C. Bianchini, E. Lorenzani, A. Bellini, and E. Fornasiero, "Evaluation of combined reference frame transformation for interturn fault detection in permanent-magnet multiphase machines," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 704
- 696
- [22] B. Aubert, J. Régner, S. Caux, and D. Alejo, "Kalman-filter-based indicator for online interturn short circuits detection in permanent-magnet synchronous generators," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 705
- [23] S. M. Mirimani, A. Vahedi, F. Marignetti, and R. Di Stefano, "An online method for static eccentricity fault detection in axial flux machines," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 706
- [24] C. Chakraborty and V. Verma, "Speed and current sensor fault detection and isolation technique for induction motor drive using axes transformation," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 707
- [25] J. G. Normiella *et al.*, "Coupling inductor fault detection and estimation in three-phase adjustable-speed drives with direct power control-based active front-end rectifiers," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 708
- [26] C. Choi, K. Lee, and W. Lee, "Observer-based phase-shift fault detection using adaptive threshold for rotor position sensor of permanent-magnet synchronous machine drives in electromechanical brake," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 709
- [27] M. A. Rodríguez-Blanco *et al.*, "Fault detection for IGBT using adaptive thresholds during the turn-on transient," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 710
- [28] A. Stabile, J. O. Estima, C. Boccaletti, and A. J. Marques Cardoso, "Converter power loss analysis in a fault-tolerant permanent-magnet synchronous motor drive," *IEEE Trans. Ind. Electron.*, vol. 62, no. 3, Mar. 2015. 711



**Gérard-André Capolino** (A'77–M'82–SM'89–F'02) was born in Marseille, France. He received the B.Sc. degree in electrical engineering from the Ecole Centrale de Marseille, Marseille, in 1974, the M.Sc. degree from the Ecole Supérieure d'Electricité, Paris, France, in 1975, the Ph.D. degree from the Aix-Marseille University, Marseille, in 1978, and the D.Sc. degree from the Institut Polytechnique de Grenoble, Grenoble, France, in 1987. 724

In 1994, he joined the University of Picardie "Jules Verne," Amiens, France, where he is currently a Chair Professor of electrical engineering. 725

Dr. Capolino is an Associate Editor of the IEEE TRANSACTIONS ON POWER ELECTRONICS, IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS, and IEEE ACCESS. He is also the acting Chair for the Steering Committee of the International Conference on Electrical Machines (ICEM). He was the recipient of the 2008 IEEE-IES Dr.-Ing. Eugene Mittelmann Achievement Award, the 2010 ICEM Arthur Ellison Achievement Award, and the 2011 IEEE-PELS Diagnostics Achievement Award. 726

727



**Jose A. Antonino-Daviu** (M'06–SM'12) received the M.Sc. and Ph.D. degrees in electrical engineering from the Universitat Politècnica de València, Valencia, Spain, in 2000 and 2006, respectively. 738

He worked in the private sector, having been involved in several international projects. Currently, he is an Associate Professor with the School of Industrial Engineering, Universitat Politècnica de València. His primary research interests include condition monitoring of electric machines, wavelet theory and its application to fault diagnosis, and design and optimization of electrical installations and systems. 739

740

741

742

743

744

745



746  
747  
748  
749  
750  
751  
752



**Martin Riera-Guasp** (M'94–SM'12) received the M.Sc. degree in industrial engineering and the Ph.D. degree in electrical engineering from the Universitat Politècnica de València, Valencia, Spain, in 1981 and 1987, respectively.

Currently, he is an Associate Professor with the Department of Electrical Engineering, Universitat Politècnica de València. His research interests include condition monitoring of electrical machines, applications of signal analysis techniques to electrical engineering, and efficiency in electric power applications.

IEEE  
Proof

## AUTHOR QUERIES

AUTHOR PLEASE ANSWER ALL QUERIES

AQ1 = Please check if provided definition for DSP is correct. Otherwise, please make the necessary corrections.

AQ2 = Please check if provided definition for MCSA is correct. Otherwise, please make the necessary corrections.

END OF ALL QUERIES

IEEE  
Proof