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Additional Information

# 1 An ultra-low pressure pneumatic jamming impact device to non- 2 destructively assess cherimoya firmness

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10 **Abstract:** The quality of cherimoya fruit is reduced by the rapid deterioration of firmness during  
11 ripening. Different methods have been developed for the measurement of firmness. The objective of this  
12 study was to use a developed impact prototype for the non-destructive assessment and prediction of  
13 cherimoya fruit firmness. The prototype has an ultra-low pressure pneumatic jamming rod used to copy  
14 the irregular fruit shape. A sample of 200 cherimoyas from Málaga (Spain) ‘Fino de Jete’ were tested  
15 during 4 days. Every day all the fruits were non-destructively tested and a set of 15 were destructively  
16 tested. On the fourth day all the remaining fruits were also destructively tested. The prototype was  
17 capable of copying the irregularities of the fruit and non-destructively assessing the decrease in  
18 cherimoya firmness during ripening without causing damage. A high correlation was found between  
19 destructive firmness and non-destructive variables from the prototype. A PLS model was developed to  
20 relate destructive firmness from day 4 to non-destructive variables and diameter from day 3, with a  $R^2$  of  
21 75.6 and a RMSECV of 0.9885. A calibration set confirmed the prediction with a  $R^2$  of 80.2 and a  
22 RMSEP of 0.0561. Firmness decay could be non-destructively predicted 24 hours in advance using the  
23 variables extracted from the prototype device signal.

24 **Keywords:** fruit quality; prediction; prototype; deceleration signal; non-damaging.  
25  
26

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## 27 1. Introduction

28 Cherimoya (*Annona cherimola*) production for fresh-market consumption is reduced by the rapid  
29 deterioration of the fruit during postharvest handling (Alique & Zamorano, 2000). The fruit ripens  
30 quickly, the pulp softens and the peel darkens, being difficult to handle without producing damage  
31 (Franco-Mora et al., 2015). One of the deterioration characteristics is softening of the fruit. The  
32 measurement of fruit firmness is a suitable method to monitor fruit softening during postharvest handling  
33 (Valero, Crisosto, Slaughter, 2007).

34 Advanced sensing technologies have been developed to non-destructively assess the quality of fresh fruits  
35 and vegetables such as: computer vision (Opara & Pathare, 2014), spectroscopy (Wang, Peng, Xie, Bao,  
36 He, 2015), X-rays, hyperspectral techniques (Lorente et al., 2012), magnetic resonance techniques,  
37 mechanical contact (Chen & Opara, 2013), chemical sensing, wireless sensor networks and radio-  
38 frequency identification sensors (Ruiz-Altisent et al., 2010; Arendse, Fawole, Magwaza, Opara, 2018).  
39 However, most of these techniques are not extensively used in commercial postharvest handling due to  
40 their high cost, technical limitations, grower resistance and supply chain restrictions. However, the  
41 successful application of NIR spectroscopy to assess fruit quality has been limited to fruits with  
42 homogeneous pulp and thin rind (De Oliveira, Bureau, Peira-Netto, 2014).

43 Different mechanical non-destructive techniques have been developed in order to assess fruit firmness  
44 instead of using the traditional destructive test. Fruit response to force (the mechanical thumb method, the  
45 Sinclair firmness tester and the laser air-puff), impact force response (the instrumented hammer impact  
46 device and load cells) or other devices based on impact forces, rebound technique, acoustic responses to  
47 vibrations and impacts, have been used to assess fruit firmness without damaging the fruit (García-  
48 Ramos, Valero, Hommer, Ortiz-Cañavate, Ruiz-Altisent, 2005; Khalifa, Komarizadeh, Tousei, 2011).  
49 However, most of them are used in the laboratory, and new methods which increase accuracy and  
50 velocity and decrease cost are still required.

51 Cherimoya is a very irregular and delicate fruit, for which measuring firmness using impact methods is  
52 very difficult. Jamming systems consisting of a mass of granular material encased in an elastic membrane  
53 have been used in robotic grippers for gripping objects with complex geometries (Amend, Brown,  
54 Rodenberg, Jaeger, Lipson, 2012). A jamming system has been used for copying eggplant and mango  
55 fruit shape during the pick & place process (Blanes, Ortiz, Mellado, Beltrán, 2015; Cortés et al., 2017).  
56 One of the fingers adapts and copies the product shape when the jamming of its internal granular material  
57 changes from soft to hard.

58 The objective of the present research study was to non-destructively assess cherimoya firmness using an  
59 impact device prototype with an ultra-low pressure pneumatic jamming rod.

## 60 **2. Materials and Methods**

### 61 2.1. Vegetal Material

62 A sample of 200 cherimoyas from Málaga (Spain) of the 'Fino de Jete' variety were selected in a very  
63 unripe stage (0.1845 kg mass (SD = 0.097), 0.0649 m diameter (SD = 0.0026), 71.4 N destructive  
64 firmness (SD= 11.84) and 15.3 °Brix (SD = 0.81) soluble solid content with a refractometer. Fruits were  
65 previously stored at 8°C and during the experiment days at room conditions (22.63 °C (SD = 1.77) and 56  
66 % relative humidity (SD = 9.06)).

### 67 2.2. Method

68 All the fruits were non-destructively tested every day for 4 d and a set of 15 randomly selected  
69 cherimoyas destructively tested (destructive firmness and soluble solid content). After being measured by  
70 the non-destructive prototype, the 15 selected fruits were destructively measured by a penetration test (5  
71 mm deformation, 10 mm rod diameter and 0.001 m s<sup>-1</sup> speed) using a universal test machine (Ibertest,  
72 Madrid, Spain) [15]. Three destructive firmness measurements were done per fruit, one at the same point  
73 and two more at the equatorial surface. Soluble solids content (SSC, °Brix) was determined with a digital  
74 refractometer (PR-101 ATAGO, Norfolk, VA). Mass and diameter were also measured and the equatorial  
75 diameter determined using a digital calliper (0.001 mm accuracy).

76 The ready-to-eat stage was considered when the flesh was uniformly creamy and glossy white, with a  
77 custard-like consistency, with no more than 10% browning of the skin area (Alique & Zamorano, 2000).

78 On the fourth day all the remaining fruits (155 cherimoyas) were destructively tested by penetration test  
79 after the non-destructive firmness measurement. Then, the destructive firmness (obtained by the

80 penetration test on day 4) was use as the reference firmness value to be compared to the non-destructive  
81 variables obtained from the prototype on day 4.

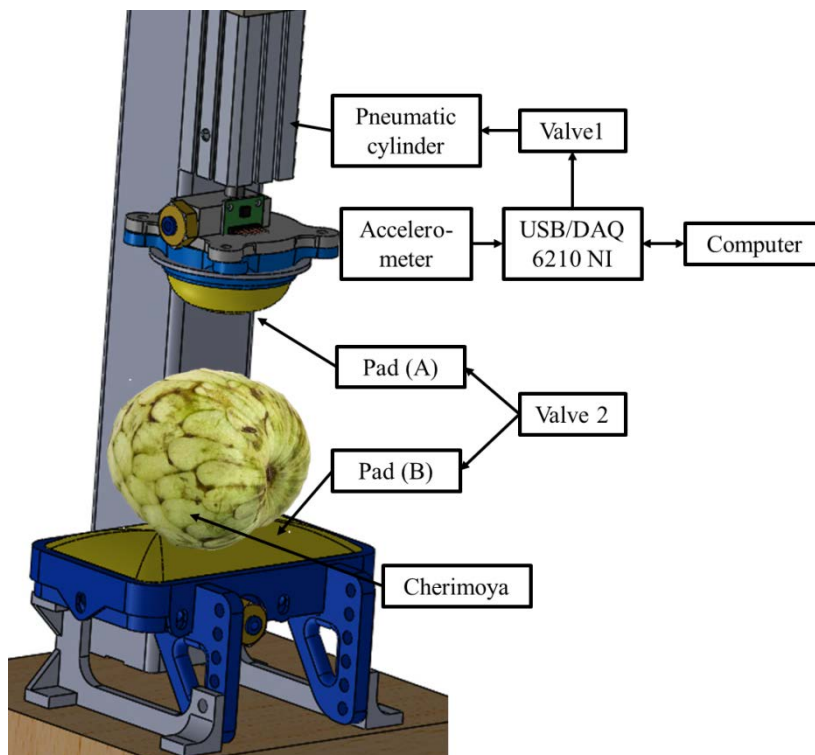
82 Besides, in order to predict firmness using the non-destructive variables, the non-destructive variables  
83 (obtained from the prototype) from day 3 were used to predict destructive firmness (obtained by the  
84 penetration test).

### 85 2.3. Prototype calibration

86 At every measuring session the prototype was calibrated with a rubber cylinder with a steel centre (63  
87 mm length, 52 mm diameter, 7.8 mm width and 62.2 N penetration resistance (5 mm deformation, 10 mm  
88 rod diameter and  $0.001 \text{ m s}^{-1}$  speed)).

### 89 2.4. Prototype device and signal processing

90 The non-destructive firmness measurements were provided by the analysis of the impacts of a pad, moved  
91 by an ultra-low friction pneumatic cylinder (SMC MQQT B16-50D), against every cherimoya, Figure 1.  
92 The pad (A) was located at the pneumatic cylinder end of rod (A) and the pad (B) was located at the  
93 cradle. Both pads had a vacuum jamming system capable of adapting to the irregularities of fruit shape. A  
94 mono-axial accelerometer (ADXL278, Analog Devices, USA; measurement range of  $\pm 50 \text{ g}$ ) was attached  
95 to the pad (A). Impacts were sampled with a USB data acquisition (DAQ) 6201 NI (National Instruments,  
96 USA).

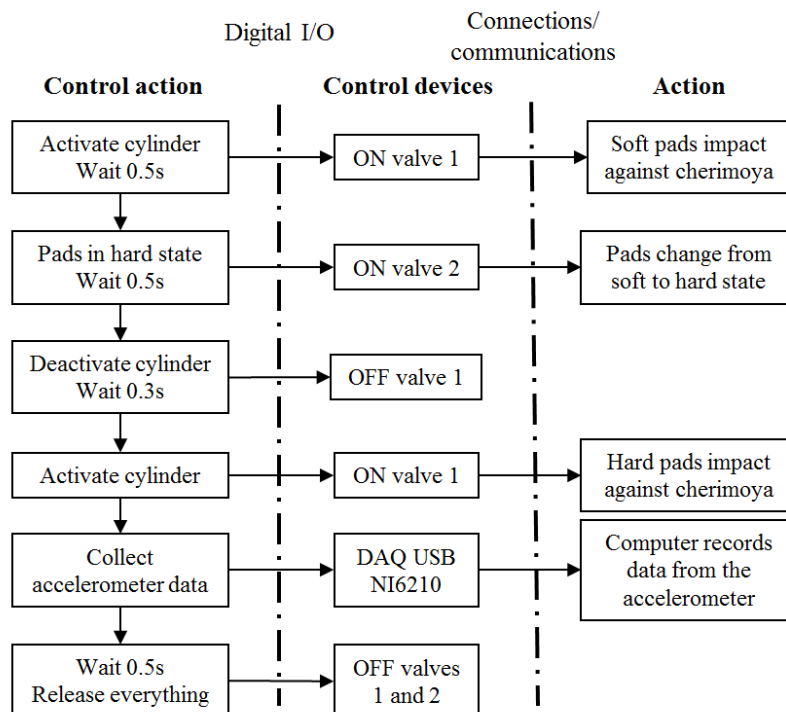


97

98 **Figure 1.** Prototype device used for the assessment of cherimoya firmness. (A) Pneumatic cylinder end of rod, (B)  
99 rubber cylinder for calibration, (C) cradle.

100

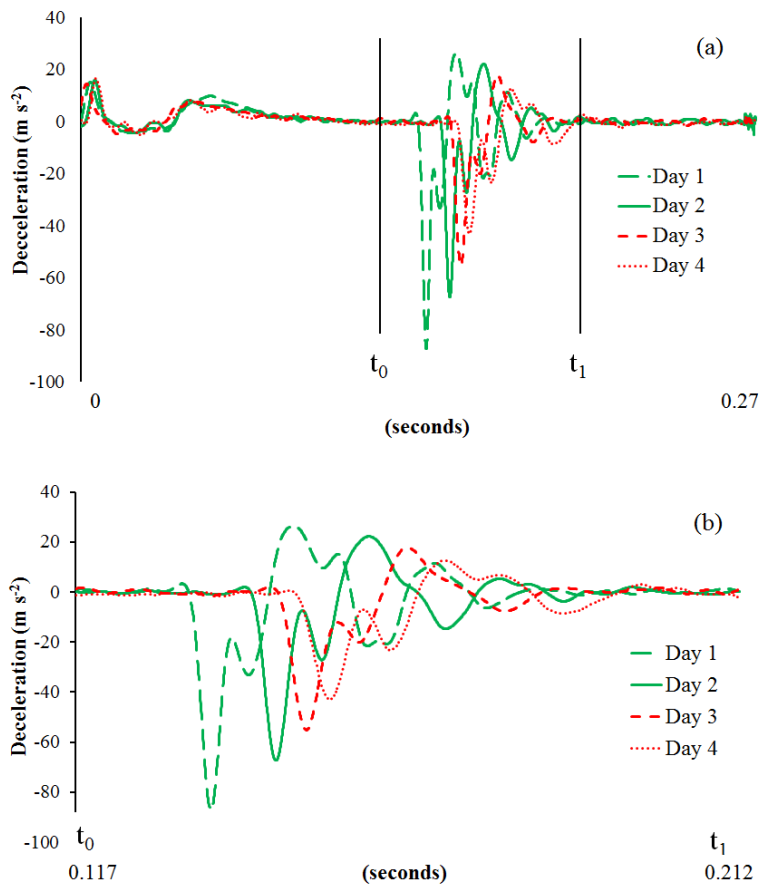
101 Two programs were used during the process. The first program, LabVIEW11.0 (National Instruments,  
 102 USA), controlled the pads and the pneumatic cylinder. Valve 1 (SY3120, SMC, Japan) was activated  
 103 during 0.5 seconds. Two adjustable flowmeter control valves (SMC Ref. AS2201F-01-04S) were used to  
 104 adjust the speed of the pneumatic cylinder. Pad (A), in soft state, went down and impacted against  
 105 cherimoya. Valve 2 (SY3120, SMC, Japan) was activated during 0.5 s and pads (A) and (B) changed  
 106 from soft to hard state. The air inside pads (A) and (B) was extracted by means of a vacuum generator  
 107 (Coval Ref GVP20N14), and inside, its particles collapsed. This process was called jamming transition.  
 108 The pads adapted to the cherimoya shape and kept hard while vacuum process continued. Valve 1 was  
 109 deactivated during 0.3 s and pad (A) was raised. Valve 1 was activated during 0.5 s and, at the same time,  
 110 a trigger signal was sent to the DAQ. Pad (A) dropped and impacted against cherimoya. Deceleration data  
 111 were sampled during 0.27 s at 30 kHz while a computer recorded the signal. The whole process is  
 112 illustrated in Fig. 2.



113

114 **Figure2.** Diagram of the control action, devices involved and actions until collecting accelerometer.

115 The second program, LabVIEW11.0 (National Instruments, USA), processed deceleration data. Firstly,  
 116 data were low-pass filtered at 1500Hz. Figure 3 (a) shows the deceleration when the same cherimoya was  
 117 analysed with this device in different days. Figure 3 (b) shows the signal when pad (A) impacted against  
 118 cherimoya. This part of the signal was used for extracting three variables. First variable (VE) processed  
 119 the signal with a Fast Fourier Transform methodology, using the option “measurement magnitude root  
 120 main square” with Hanning window, to obtain the frequency distribution energy. Variable (VE) was the  
 121 area of spectral energy of this curve. Second variable (SLP) was average of slope of the deceleration  
 122 during the first contact of deceleration curve. Third variable (MAX) was the maximum value achieved for  
 123 this deceleration curve. Detailed process of this methodology is explained in (Blanes et al. 2016).



124

125 **Figure3.** An example of the method for processing deceleration signals. (a) Original collected signals for  
 126 decelerations of one cherimoya in 4 different days and with different ripeness state, (b) cut signal between  $t_0$  and  $t_1$   
 127 that collects the impact of pad (A) against the cherimoya.

128

### 129 2.5. Statistical analysis

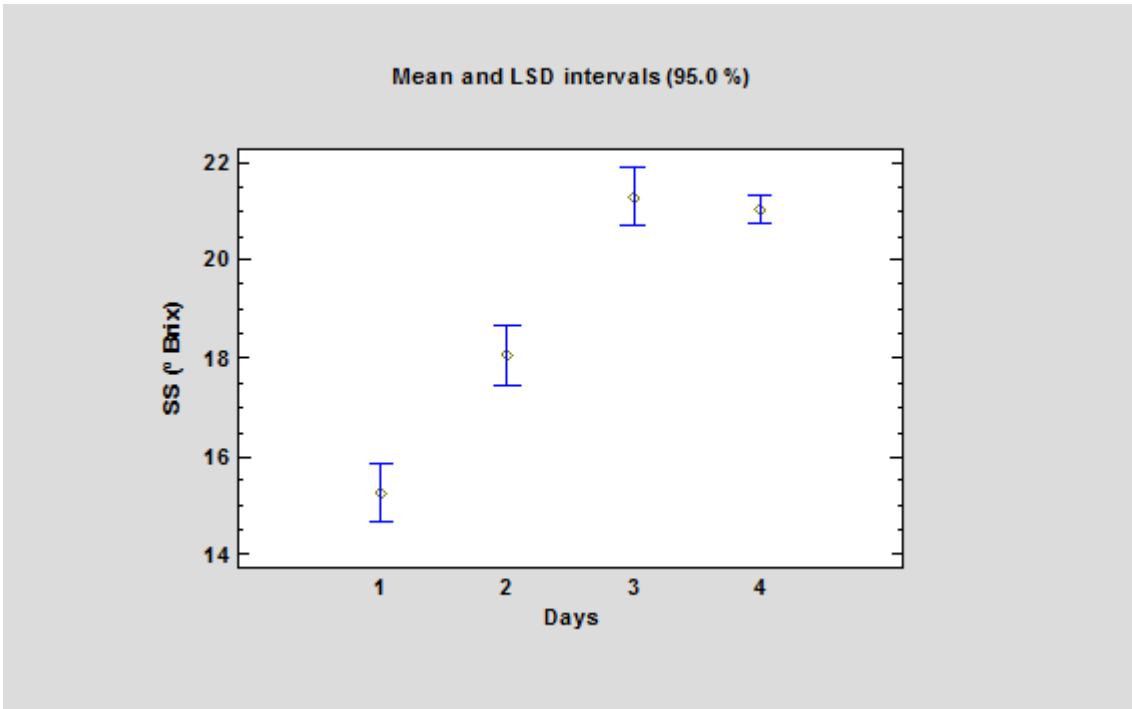
130 A partial least square (PLS) regression model was built for the prediction of destructive firmness  
 131 according to the three non-destructive variables extracted from the prototype. Cross validation was  
 132 carried out with an internal set using “leave out every 2nd”. Root mean square error for cross validation  
 133 (RMSECV) was obtained by comparing the predicted firmness with the experimental values. RMSECV  
 134 was plotted against LVs to set the optimal number of LVs.

135 The model was tested to predict firmness with a random calibration set of 35 fruits. The root mean square  
 136 error of the prediction and the  $R^2$  of the prediction were calculated. RMSEP was then expressed as  
 137 RMSEP% corresponding to the percentage of error of prediction calculated with RMSEP divided by the  
 138 mean values of fruit firmness from the validation set.

## 139 3. Results

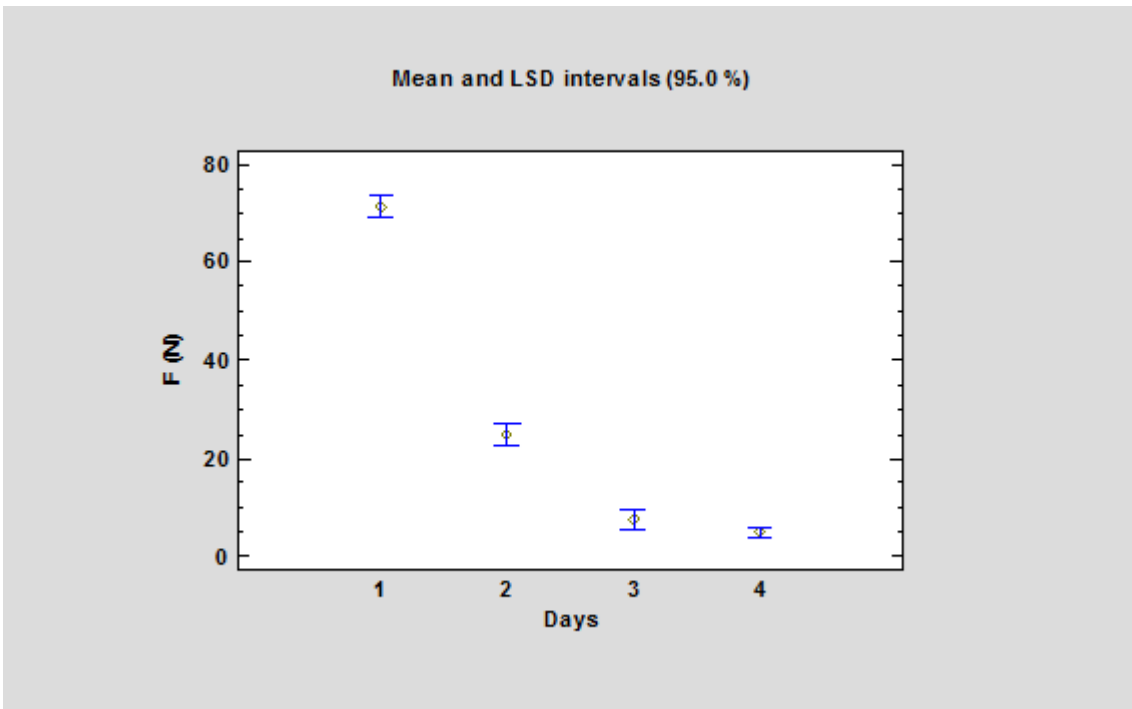
### 140 3.1. Ripeness development

141 Ripeness development during the four days was properly measured by the destructive variables: soluble  
 142 solid content (Fig. 4) and destructive firmness (Fig. 5).



143

144 **Figure 4.** Soluble solid content development (mean and LSD intervals) during the four test days.



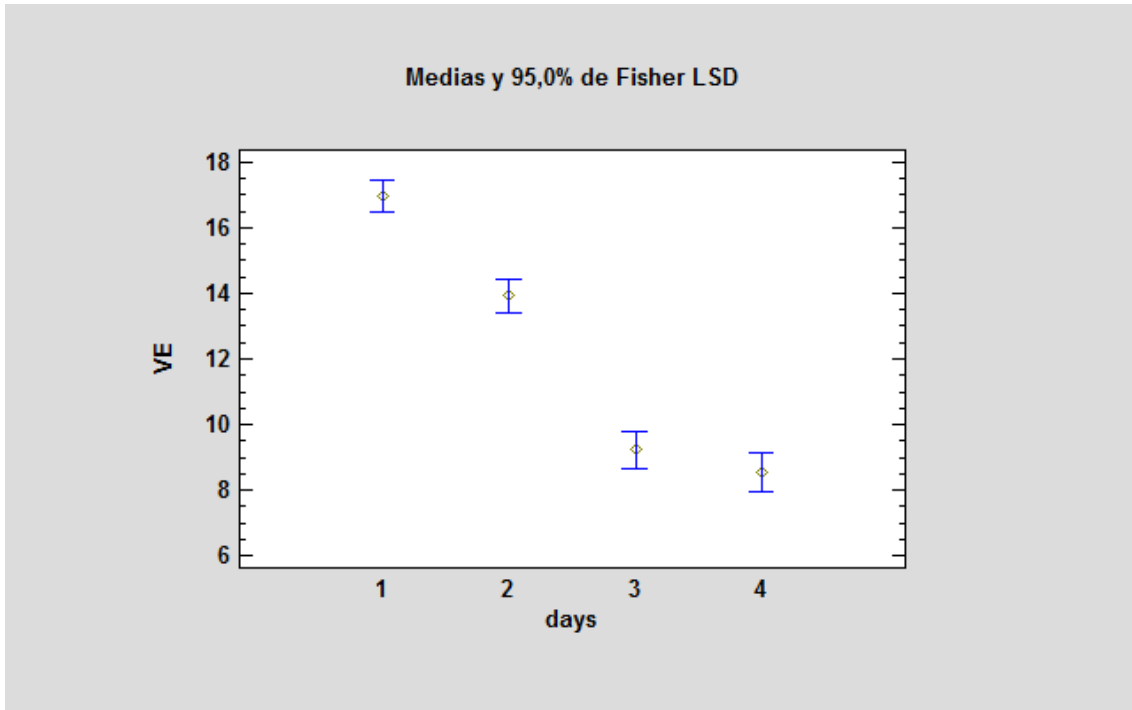
145

146 **Figure 5.** Destructive firmness (force, N) development (mean and LSD intervals) during the four test days.

147

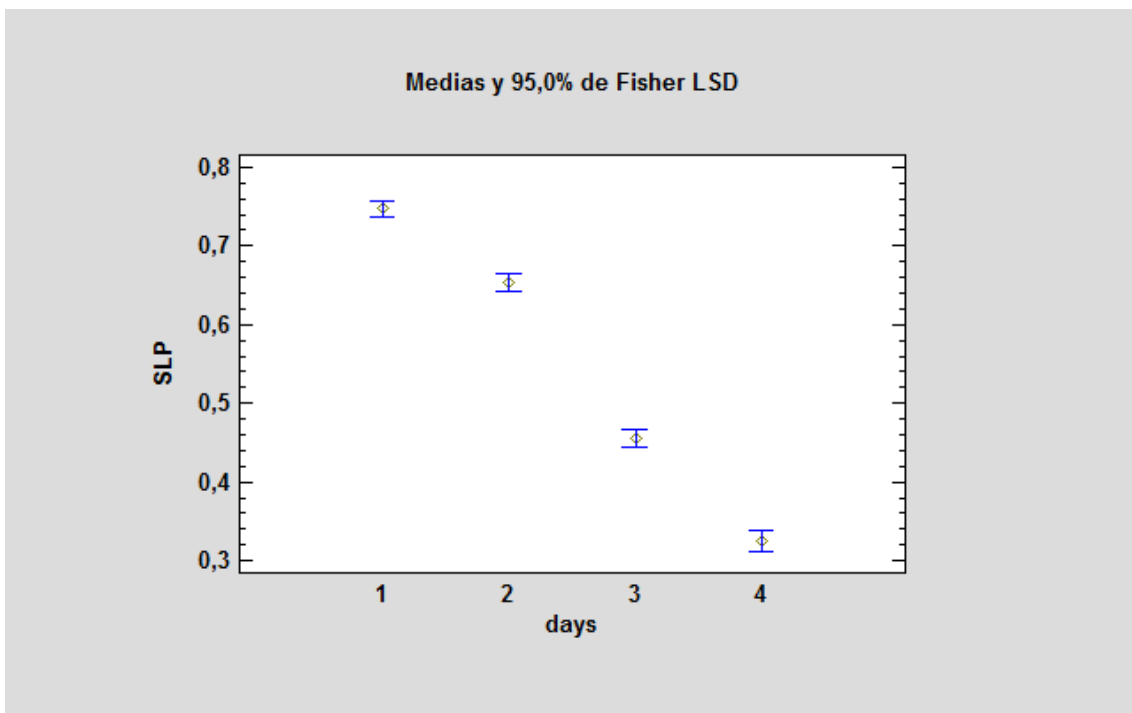
148 Cherimoya fruit is characterised by a high perishability (3-6 d at 20 °C), Alique and Zamorano (2000). As  
 149 registered before by Manriquez, Muñoz-Robredo, Gudenschwager, Robledo and Defilippi (2014) pulp  
 150 firmness was very high at harvest. However, a rapid softening was observed coinciding with an increase  
 151 in ethylene production and the increase in soluble solid content. The ready-to-eat stage was reached after

152 3 or 4 days of storage at 20 °C. In the same way, the non-destructive variables extracted from the  
153 prototype registered the ripening development parallel to the destructive firmness decrease (Figs. 6, 7 and  
154 8). While soluble solid content was not significantly different from day 3 to day 4 (Fig. 4), the destructive  
155 firmness was significantly higher from day 3 to day 4. In the same way, the non-destructive parameters  
156 extracted from the accelerometers curve were significantly higher from day 3 to day 4.



157

158 **Figure 6.** Non-destructive variable obtained from the prototype deceleration curve VE (mean and LSD intervals)  
159 during the four test days.

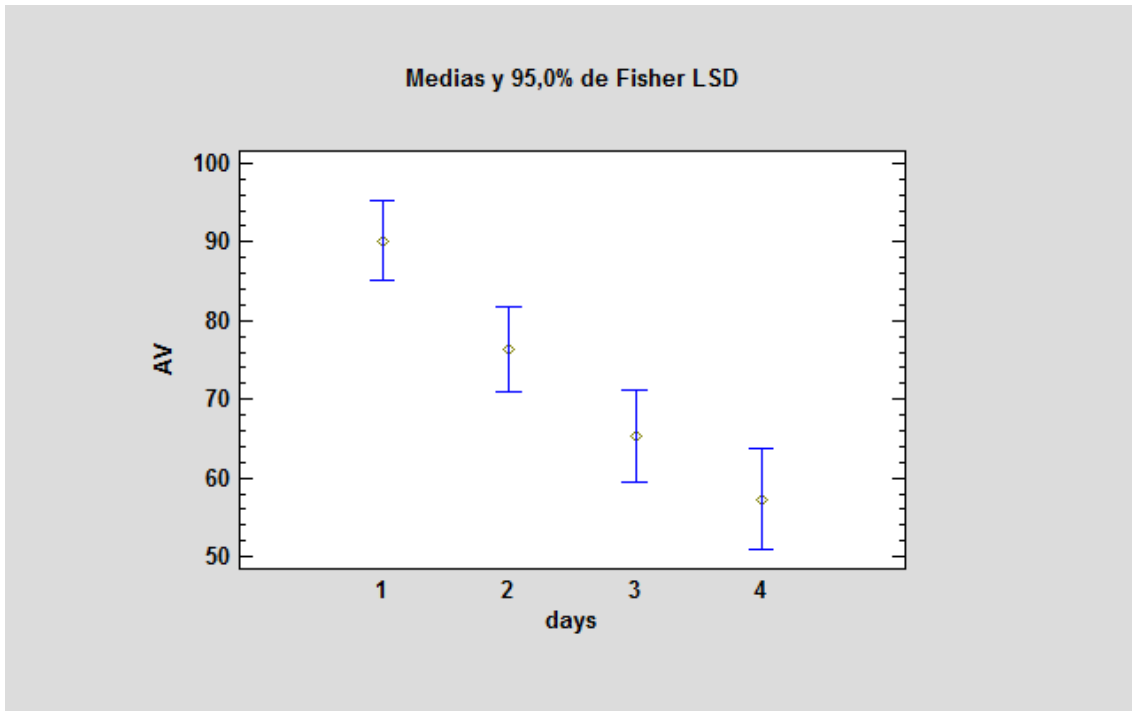


160



161 **Figure 7.** Non-destructive variable obtained from the prototype deceleration curve SLP (mean and LSD intervals)  
162 during the four test days.

163



164

165 **Figure 8.** Non-destructive variable obtained from the prototype deceleration curve MAX (mean and LSD intervals)  
166 during the four test days.

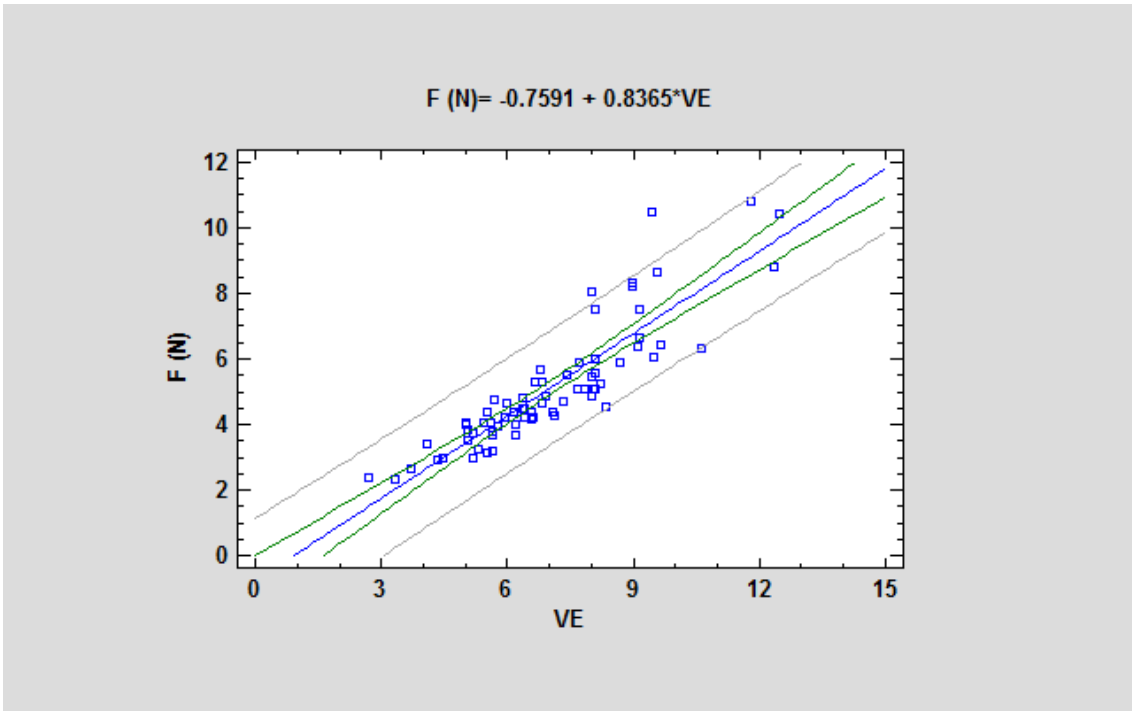
167

### 168 3.2. Fruit damage

169 No damage was produced by the prototype impacting the fruit until the day 4. On day 4, some overripe  
170 cherimoyas were damaged.

### 171 3.3. Correlation between destructive firmness and non-destructive variables

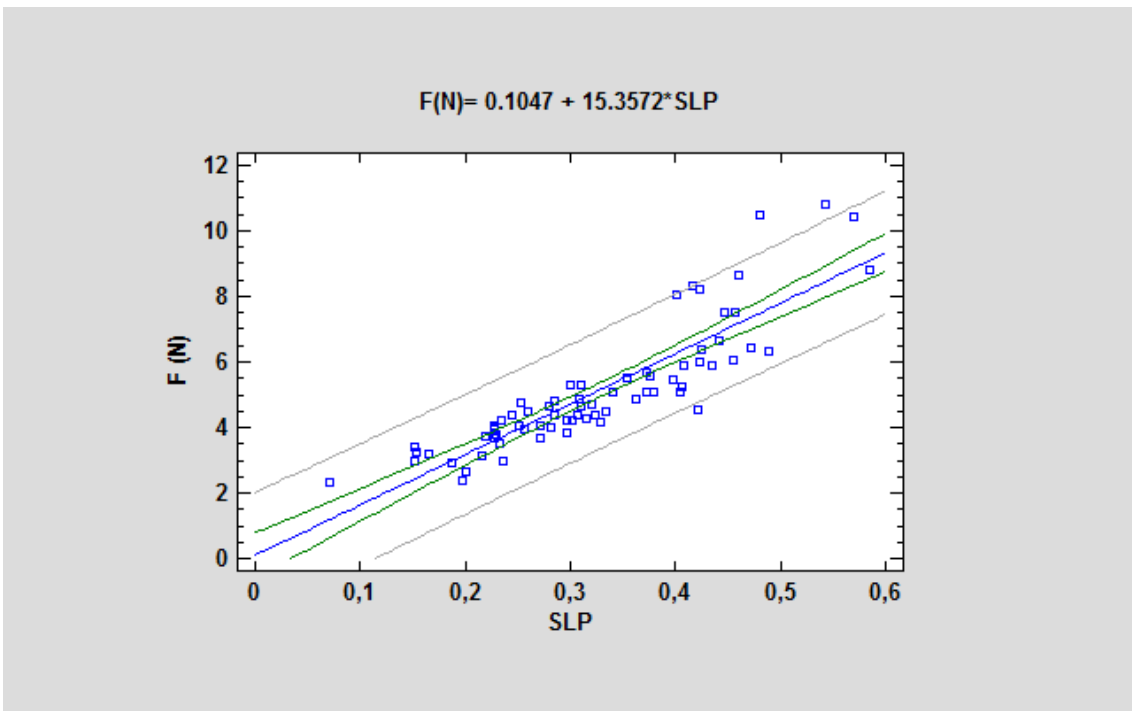
172 On comparing the destructive firmness and the non-destructive variables extracted from the prototype  
173 from the fourth day, they showed a clearly linear correlation, with a correlation coefficient of 0.91 ( $p <$   
174 0.05) to VE, 0.90 ( $p <$  0.05) to SLP and 0.90 ( $p <$  0.05) to MAX (Figs. 9, 10 and 11 respectively). These  
175 results are confirming that the studied non-destructive parameters extracted from the prototype are  
176 capable to monitor ripeness in a similar way to the destructive parameters.



177

178 **Figure 9.** Linear relation between the destructive firmness (F, N) and the non-destructive firmness measured as VE  
 179 from the prototype, using the data tested on day 4.

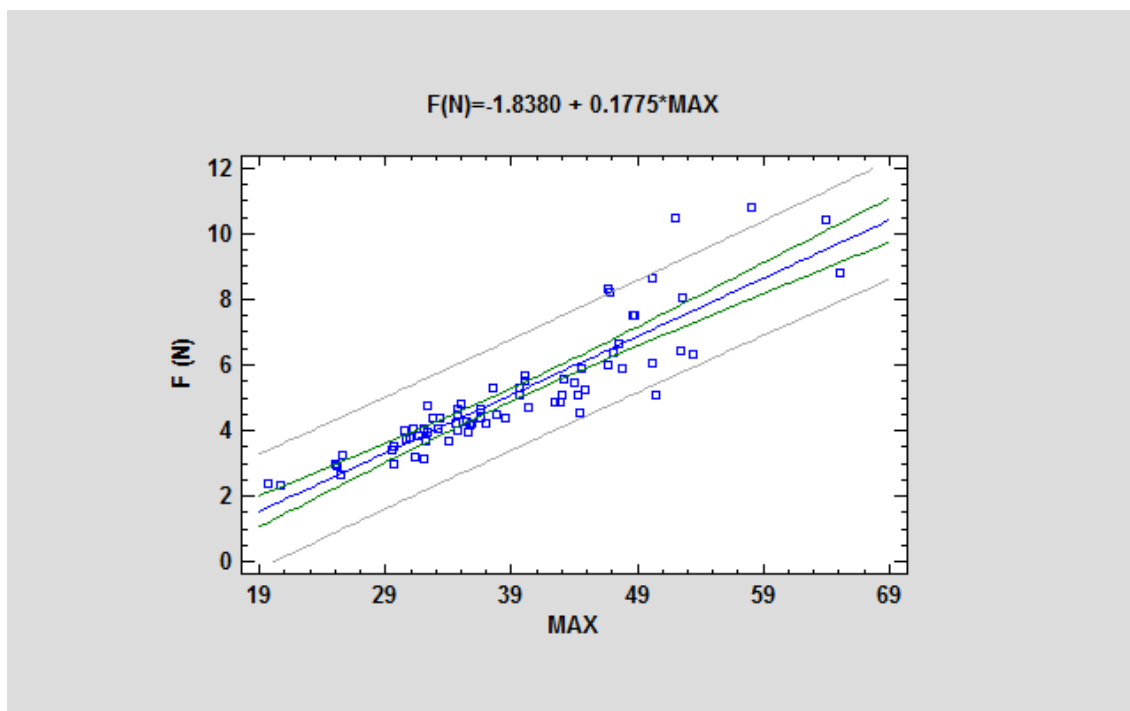
180



181

182 **Figure 10.** Linear relation between the destructive firmness (F, N) and the non-destructive firmness measured as SLP  
 183 from the prototype, using the data tested on day 4.

184



185

186 **Figure 11.** Linear relation between the destructive firmness (F, N) and the non-destructive firmness measured as  
 187 MAX from the prototype, using the data tested on day 4.

188

189 3.4. Firmness prediction of the fourth day with the non-destructive data from third day

190 In order to predict firmness decay on day 4 (measured as destructive firmness, F(N)) using the non-  
 191 destructive measurements from day 3 (VE, SLP and MAX) and the fruit diameter, a partial least square  
 192 model was developed. Table 1 shows the analysis of variance of the partial least square model explaining  
 193 final firmness decay based on the non-destructive variables from day 3 and the fruit diameter. The  
 194 resulting model is a significant predictor for the destructive firmness based on non-destructive variables.

195 Cross validation was then carried out. Four components were used, with a  $R^2$  of 75.6 and a root mean  
 196 square error for cross validation (RMSECV) of 0.99.

197 **Table 1.** ANOVA analysis of the effect of the non-destructive variables from day 3 (SLP, MAX and VE) on the  
 198 destructive firmness from day 4 (F(N)) from the PLS model.

Source	Sum of Square	df	Mean Square	F-value	P-value
Model	191.745	4	47.9363	51.0038	0.0
Residues	62.0306	66	0.939858		
Total (corr.)	253.776	70			

199 A calibration set was used to test the prediction, with a  $R^2$  of 80.2, a root mean square of the prediction  
 200 (RMSEP) of 0.0561 and a RMSEP percentage of 1.71, Table 2. The high value of the  $R^2$  and the low  
 201 values of the root mean square of the cross validation and the root mean square of the prediction indicated  
 202 the goodness of the model. The number of components (Factor, LV - 4) that were needed to be extracted  
 203 was selected according to the model comparison plot.

204 **Table 2.** Results of performance of firmness model for non-destructive firmness assessment of cherimoya fruits.

Factor	RMSECV	RMSEP	RMSEP (%)	$R^2$ (%)
--------	--------	-------	-----------	-----------

(LV)				
4	0.99	0.0561	1.71	80.2

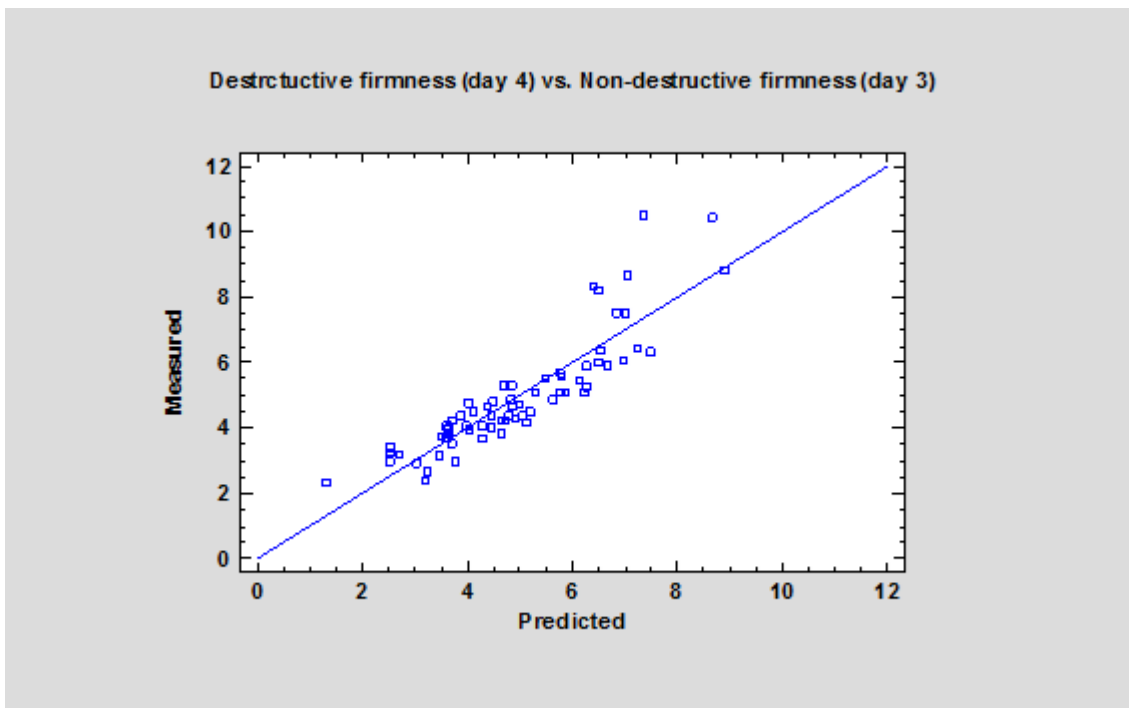
205 With the non-standardized coefficients from Table 3 the fitted equation can be built to predict the  
 206 predicted values. According to the standardized coefficients the non-destructive variables building the  
 207 model could be categorized according to their effect in the model, first the non-destructive variable  
 208 related to the maximum value of the deceleration curve from day 3 (MAX3), second the non-destructive  
 209 variable related to the slope of the deceleration curve from day 3 (SLP3), third the non-destructive  
 210 variable related to the average deceleration value from day 3 (VE3) and fourth the diameter of the fruit.

211 **Table 3.** Coefficients from the PLS model from the variables of the fitted model (diameter and the non-destructive  
 212 variables extracted from the prototype from day 3).

Coefficients from the PLS model		
	Standardised	Non-standardised
<b>Constant</b>	0	-16,73320
<b>Diameter</b>	-0,10559	-0,04969
<b>MAX3</b>	1,13693	0,43235
<b>SLP3</b>	-0,50998	-11,83370
<b>VE3</b>	0,21229	0,25411

213

214 Figure 12 shows the measured values (destructive firmness on day 4) and the firmness predicted values  
 215 extracted from the PLS model using the non-destructive variables from the prototype on day 3 and the  
 216 fruit diameter, with a 0.9 correlation coefficient ( $p < 0.05$ ).



217

218 **Figure 12.** Measured values (destructive firmness on day 4) and firmness predicted values (from the PLS  
 219 model).

220

221 According to the model, destructive firmness from day 4 could be predicted based on the non-destructive  
222 parameters extracted from the prototype from day 3. However, it is necessary to incorporate the diameter  
223 values in the model. This parameter is necessary because the non-destructive impact measurements are  
224 affected by the size of the fruit. In any case, the firmness decay measured on day 4 could be predicted 24  
225 h before using non-destructive measurements.

226 Cherimoya fruit ripens very fast, it softens and the peel darkens in the last ripeness stages. This final  
227 darkening and firmness decay could be predicted 24 h before it occurs when there are still not clear  
228 external effects.

#### 229 **4. Discussion**

230 The cherimoya fruit has high perishability and is very susceptible to fruit damage. Fruit are harvested  
231 according to subjective criteria, when they change colour and have reduced touching resistance. The  
232 tender skin and the short shelf life, makes the fruit very susceptible to physical damage during handling,  
233 transport and marketing, restricting its commercialisation (Cordeiro & Gouveia, 2013). Cherimoya fruit  
234 also ripens quickly, it softens and the peel darkens, being difficult to handle without producing damage  
235 (Franco-Mora et al., 2015). When the firmness decay and the darkening of the skin are clear it is already  
236 too late to detect firmness.

237 Dynamic hardness or stiffness measurement methods could offer useful tools in fruit ripening monitoring,  
238 but they have limitations in applicability (Feljöldi et al., 2016). Traditional impact devices are not  
239 prepared to handle delicate fruit when it is soft. The developed ultra-low pressure impact prototype has  
240 shown itself to be able to non-destructively assess firmness, even when the fruit is already soft, without  
241 damaging it.

242 In the traditional impact devices, a spherical head rod is used and the Hertz contact theory applied for the  
243 evaluation of the impact signal. This methodology is accurate when the fruit is also spherical. However,  
244 when measuring irregular shape fruits, as cherimoya, ensuring a uniform contact behaviour is difficult.  
245 The vacuum-jamming rod is capable of assuring a clean contact between the impact pad and the fruit,  
246 reducing the noise of the signal.

247 The ultra-low pressure pneumatic cylinder pad reduces fruit damage while measuring firmness of very  
248 soft fruit and the jamming rod and cradle system are capable of adapting to the irregular shape of the fruit  
249 and increases accuracy when measuring irregular fruit. Final darkening and firmness decay could be  
250 predicted before it occurs. Based on this prototype a new easy to calibrate and use, non-expensive device  
251 could be developed and used on-line for postharvest sorting applications.

#### 252 **5. Conclusions**

253 An impact prototype device with an ultra-low pressure pneumatic jamming rod has been developed. The  
254 device is capable of adapting to the irregularities of the fruit shape and non-destructively assessing the  
255 decrease in cherimoya firmness during ripening without causing damage.

256 The measured destructive firmness and the non-destructive variables extracted from the prototype showed  
257 a clearly linear correlation, higher than 0.8 in all the cases.

258 A PLS model was developed to relate destructive firmness from day 4 to the prototype non-destructive  
259 variables and diameter from day 3, with a  $R^2$  of 75.6 and a RMSECV of 0.9885. A calibration set  
260 confirmed the prediction with a  $R^2$  of 80.2 and a RMSEP of 0.0561.

261 Firmness decay and darkening (measured as destructive firmness) could be non-destructively predicted 24  
262 h in advance using the variables extracted from the prototype device signal. Based on this prototype, a  
263 new, easy to calibrate and use, non-expensive device could be developed for use in on-line postharvest  
264 sorting applications.

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