# Optical Implementation of $2 \times 2$ Universal Unitary Matrix Transformations 

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#### Abstract

Unitary operations are a specific class of linear transformations that have become an essential ingredient for the realization of classical and quantum information processing. The ability of implementing any $n$-dimensional unitary signal transformation by using a reconfigurable optical hardware has recently led to the pioneering concept of programmable linear optical processor, whose basic building block (BB) must be correctly designed to guarantee that the whole system is able to perform $n \times n$ universal (i.e., arbitrary) unitary matrix transformations. Here, it is demonstrated that the present architectures of the BB do not fulfil the universal unitary property (at least) in $2 \times 2$ optical processors, limiting the number of unitary matrix transformations that may be generated. Aiming to solve this fundamental constraint, the theoretical tools required to analyze and design $2 \times 2$ universal unitary optical circuits and their corresponding BBs are presented. The consequences of this mathematical framework are explored, obtaining a simple route to implement different BB architectures, all of them guaranteeing a true universal unitary functionality in the resulting $2 \times 2$ optical processors. These findings may pave the way to revisit the design of high-dimensional unitary optical processors, unleashing the potential of programmable integrated photonics technology.


## 1. Introduction

Unitary operators are linear transformations between complex vector spaces which preserve the norm of the input vector. ${ }^{[1-4]}$ Such a kind of transformations have become a mathematical tool of paramount importance in fundamental and applied research, for instance, enabling the implementation of any linear mapping in a simple and elegant fashion, ${ }^{[1,5]}$ explaining underlying aspects of quantum mechanics (such as the unitary nature of the time evolution of a particle in a closed Hermitian quantum

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有 proposing a unique optical hardware, the so-called programmable linear optical processor, which must be able to generate any $n$-dimensional unitary transformation (an indispensable piece to implement any multidimensional linear mapping via the singular value decomposition). ${ }^{[5,11,14-16]}$ This requires, as a necessary and sufficient condition, that the transfer function of the system $T_{n}$ is an $n \times n$ arbitrary (or universal) unitary matrix, that is, the $\mathrm{U}(n)$ Lie group (an algebraic group composed by all the $n \times n$ unitary matrices along with the matrix multiplication operation ${ }^{[2,3]}$ ) must be completely described by $T_{n}$ when varying the value of its entries (encoded by parameters) in the complex plane. ${ }^{[2-4,17]}$ Along this line, since the proposed architectures of $T_{n}$ are constructed by combining basic building blocks (BBs), which perform $2 \times 2$ unitary transformations, ${ }^{[15,16,18-21]}$ it is of capital importance a correct design and implementation of this system (also termed in the literature as unit cell, ${ }^{[19,22,23]}$ programmable photonic analog block ${ }^{[14,24]}$ or reconfigurable beamsplitter ${ }^{[25]}$ ) to guarantee the universal unitary property in $T_{n}$ for any $n \geq 2$ (however, note that the BB does not have to perform universal unitary transformations by itself ${ }^{[20,21,25]}$ ).
In this work, it is shown that the existing architectures of the $\mathrm{BB}^{[16,19-23,25-34]}$ lead to optical processors which do not satisfy the unitary universality (at least) for the case $n=2$. To overcome this


Figure 1. $2 \times 2$ universal unitary optical processor. Two (classical or quantum) optical wave packets $A_{1}$ and $A_{2}$ at the input waveguides may be linearly transformed into any pair of optical wave packets $B_{1}$ and $B_{2}$ at the output waveguides with the same global energy as that of the input via the relation $\left(B_{1}, B_{2}\right)^{\top}=T_{2}\left(A_{1}, A_{2}\right)^{\top}$, with the system transfer function $T_{2}$ being an arbitrary matrix of $U(2)$ (the yellow lines represent the matrix nature of the transformation). Since the system input $\mathbf{e}_{A}=A_{1} \hat{\mathbf{e}}_{1, \perp}+A_{2} \hat{\mathbf{e}}_{2, \perp}$ and the system output $\mathbf{e}_{B}=B_{1} \hat{\mathbf{e}}_{1, \perp}+B_{2} \hat{\mathbf{e}}_{2, \perp}$ can always be illustrated as two different points on the surface of the Bloch sphere, $T_{2}$ must be able to induce any (no observable) global phase shifting $\delta$ along with a rotation of an angle $\alpha$ around an arbitrary unit vector $\hat{\mathbf{n}}$ which allows us to move from $\mathbf{e}_{A}$ to $\mathbf{e}_{B}$, i.e., $T_{2} \equiv e^{j \delta} R_{\hat{n}}(\alpha)$. Given that the arbitrary nature of $\hat{\mathbf{n}}$ hampers the direct implementation of $R_{\hat{\mathrm{n}}}(\alpha)$ (red arrow) using mainstream integrated optical devices (PSs, DCs and MMIs), we take advantage of the Euler rotation theorem (Equation (2)) to describe $R_{\hat{\mathrm{n}}}(\alpha)$ as a concatenation of three rotations around two specific unit vectors $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2} \in \mathbb{R}^{3}$ (a particular example is depicted taking $\hat{\mathbf{r}}_{1}=\hat{\mathbf{z}}$ and $\hat{\mathbf{r}}_{2}=\hat{\mathbf{y}}$, see blue arrows).
fundamental restriction, we dig into the foundations of the $\mathrm{U}(2)$ group to analyze and design compact $2 \times 2$ universal unitary optical circuits and their corresponding BBs. To further unfold the potential of our results, we also uncover the minimal circuit architecture of the BB , defined as the BB implementation requiring the lowest number of basic devices.

## 2. Preliminary Concepts: $\mathbf{2 \times 2}$ Universal Unitary Matrix Transformations

As illustrated in Figure 1, a $2 \times 2$ universal unitary optical processor is a system which linearly transforms two (classical or quantum) optical wave packets $A_{1}$ and $A_{2}$ at the system input into any pair of optical wave packets $B_{1}$ and $B_{2}$ at the system output with the same global energy as that of the input via the matrix relation $\left(B_{1}, B_{2}\right)^{\mathrm{T}}=T_{2}\left(A_{1}, A_{2}\right)^{\mathrm{T}}$, with the system transfer function $T_{2}$ being an arbitrary matrix of $\mathrm{U}(2)$ (the superscript T accounts for the matrix transposition).

In complete analogy with a path-encoded quantum bit where the standard states $|0\rangle$ and $|1\rangle$ may be respectively identified with the unit vectors $\hat{\mathbf{e}}_{1, \perp}$ and $\hat{\mathbf{e}}_{2, \perp}$ of Figure 1 (which account for the transverse direction of the electric field strength propagated by the upper and lower waveguides), the system input
$\mathbf{e}_{A}=A_{1} \hat{\mathbf{e}}_{1, \perp}+A_{2} \hat{\mathbf{e}}_{2, \perp}$ and the system output $\mathbf{e}_{B}=B_{1} \hat{\mathbf{e}}_{1, \perp}+B_{2} \hat{\mathbf{e}}_{2, \perp}$ can always be illustrated as two different points on the surface of the Bloch sphere (also known as Poincaré sphere in classical polarization optics, although here there is no connection between the Cartesian axes of the Bloch sphere and the state-ofpolarization of light. The wave packets are always located in $\hat{\mathbf{e}}_{1, \perp}$ and $\hat{\mathbf{e}}_{2, \perp}$ ).

Consequently, $T_{2}$ is an arbitrary matrix of $\mathrm{U}(2)$ if and only if $T_{2}$ can perform a complete description of the surface of the Bloch sphere and may induce any global phase shifting in $A_{1,2}$ (no observable in the Bloch sphere). Mathematically, this necessary and sufficient condition can be written as ${ }^{[7,35]}$

$$
T_{2}=\mathrm{e}^{\mathrm{j} \delta} R_{\hat{\mathrm{n}}}(\alpha)=\mathrm{e}^{\mathrm{j} \delta}\left(\begin{array}{c}
\cos \frac{\alpha}{2}-j n_{z} \sin \frac{\alpha}{2}-\left(n_{y}+j n_{x}\right) \sin \frac{\alpha}{2}  \tag{1}\\
\left(n_{y}-j n_{x}\right) \sin \frac{\alpha}{2}
\end{array} \cos \frac{\alpha}{2}+j n_{z} \sin \frac{\alpha}{2} .,\right.
$$

where $\delta \in[0,2 \pi)$ is the global phase shifting and $R_{\hat{\mathrm{n}}}(\alpha)$ is a matrix that allows us to move between two arbitrary points of the Bloch sphere (from $\mathbf{e}_{A}$ to $\mathbf{e}_{B}$ ) by performing a rotation of an angle $\alpha \in$ $[0,2 \pi]$ around an arbitrary unit vector $\hat{\mathbf{n}}=n_{x} \hat{\mathbf{x}}+n_{y} \hat{\mathbf{y}}+n_{z} \hat{\mathbf{z}}$, with $n_{x, y, z} \in[-1,1]$. In line with the dimension of $\mathrm{U}(2)(\operatorname{dim} \mathrm{U}(2)=$ 4), ${ }^{[3]} T_{2}$ is a parametric unitary matrix encompassing


Figure 2. Building blocks (BBs) proposed in the PIP literature. a) BB architecture reported in refs. ${ }^{[26-31]}$ and corresponding $S U(2)$ processor. ${ }^{[30]}$ b) ${ }^{[3 B}$ architecture reported in refs. ${ }^{[16,19-23,25,32-34]}$ and resulting $S U(2)$ processor. ${ }^{[25,34]}$ The rotations of the Bloch sphere that cannot be generated by each $S U(2)$ processor are inset at the right of the figures.

4 independent real parameters (degrees of freedom): $\delta, \alpha$ and two components of $\hat{\mathbf{n}}$ (the three components cannot be independent parameters since $\hat{\mathbf{n}}$ must satisfy the normalization condition $|\hat{\mathbf{n}}|^{2}=n_{x}^{2}+n_{y}^{2}+n_{z}^{2}=1$ ).

Unfortunately, the arbitrary nature of $\hat{\mathbf{n}}$ hampers the direct implementation of $T_{2}$ using mainstream integrated optical devices (PSs, DCs, and MMIs). This technological difficulty can be circumvented by taking advantage of the Euler rotation theorem, which states that $R_{\hat{\mathrm{n}}}(\alpha)$ can be factorized as a concatenation of three rotations around two specific unit vectors $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2} \in \mathbb{R}^{3}$ which must be linearly independent or, equivalently, nonparallel (note that the orthogonality is a particular case of such condition) ${ }^{(7,35,36]}$
$R_{\hat{\mathrm{n}}}(\alpha)=R_{\mathrm{r}_{1}}\left(\alpha_{3}\right) R_{\mathrm{f}_{2}}\left(\alpha_{2}\right) R_{\mathrm{r}_{1}}\left(\alpha_{1}\right)$.

Now, the four independent real parameters of $T_{2}$ are encoded in $\delta$ and the angles $\alpha_{1,2,3} \in[0,2 \pi]$. As shown below, selecting adequate values in $\hat{\mathbf{r}}_{1}$ and $\hat{\mathbf{r}}_{2}$, we will be able to implement $T_{2}$ using PSs, DCs and MMIs (the implementation of each degree of freedom may require more than one basic device).

In the next sections, we will restrict the analysis of the unitary universality to $S U(2)$, a Lie subgroup of $U(2)$ exclusively including the $2 \times 2$ unitary matrices with determinant equal to 1. ${ }^{[2,3]}$ Remarkably, this will allow us to: i) simplify the discussion of the $2 \times 2$ optical processors reported in previous works to demonstrate that the unitary universality is not hold, ${ }^{[16,19-23,25-34]}$ and ii) uncover compact architectures of universal $U(2)$ processors in Section 4. Specifically, the restriction to $\operatorname{SU}(2)$ can be done by excluding the term $\mathrm{e}^{j \delta}$ in $T_{2}$. In such circumstances, $T_{2}=R_{\mathbf{r}_{1}}\left(\alpha_{3}\right) R_{\hat{\mathrm{r}}_{2}}\left(\alpha_{2}\right) R_{\mathrm{r}_{1}}\left(\alpha_{1}\right)$ and a set of three independent real parameters $\left\{\alpha_{1}, \alpha_{2}, \alpha_{3}\right\}$ are only required to perform a complete description of $\mathrm{SU}(2)$ (matching to the dimension of this subgroup, $\operatorname{dim} \operatorname{SU}(2)=3) .{ }^{[3]}$ For completeness, in Section S1 (Supporting Information) we include alternative strategies to analyze the universal unitary property in a parametric matrix of $\mathrm{SU}(2)$.

On the other hand, bearing in mind that the optical circuits associated to two different $\mathrm{SU}(2)$ systems (e.g., $T_{2}^{(i)}=$ $R_{\hat{\mathrm{r}}_{1}}\left(\alpha_{3}\right) R_{\hat{\mathrm{r}}_{2}}\left(\alpha_{2}\right) R_{\hat{\mathrm{r}}_{1}}\left(\alpha_{1}\right)$ and $\left.T_{2}^{(i i)}=R_{\hat{\mathrm{r}}_{1}}\left(\alpha_{6}\right) R_{\hat{\mathrm{r}}_{2}}\left(\alpha_{5}\right) R_{\hat{\mathrm{r}}_{1}}\left(\alpha_{4}\right)\right)$ can be cascaded by describing the transformations $R_{\mathrm{r}_{1}}\left(\alpha_{4}\right)$ and $R_{\mathrm{r}_{1}}\left(\alpha_{3}\right)$ using a single rotation matrix $R_{\mathrm{r}_{1}}\left(\alpha_{4}+\alpha_{3}\right)$ in the matrix multiplication $T_{2}^{(i)} T_{2}^{(i)}$ (while the other four rotations remain invariant), the BB of a universal $\operatorname{SU}(2)$ processor can be defined via the following transfer function
$T_{\mathrm{B}}:=R_{\mathrm{t}_{2}}\left(\alpha_{2}\right) R_{\mathrm{r}_{1}}\left(\alpha_{1}\right)$.

In this way, the final $R_{\mathrm{r}_{1}}$ transformation of Equation (2) may be employed to connect the BBs of adjacent $\mathrm{SU}(2)$ systems, providing simultaneously the input and output rotations required by their corresponding $T_{2}$ matrices (the same definition of $T_{\mathrm{B}}$ can also be extrapolated to a more general scenario where the BBs are connected in a mesh configuration to construct $n \times n$ optical processors with $n>2$, as discussed in Section 5).

## 3. Existing Proposals of the Building Block

Basically, two popular optical architectures of the BB have been proposed in the state of the art, sketched in Figure 2. ${ }^{[16,19-23,25-34]}$ Both structures are composed by fixed couplers (MMIs or symmetric DCs) and PSs. Each coupler implements a perfect 50:50 beamsplitter and each PS encodes a tunable real parameter of the BB transfer function. Considering only forward propagation (from left to right) and assuming negligible wave reflection, the following unitary matrices $(\phi, \theta \in[0,2 \pi])$
$T_{\mathrm{B} a}=\mathrm{je}^{\mathrm{j}\left(\frac{\phi+\theta}{2}\right)}\left(\begin{array}{cc}-\sin \left(\frac{\phi-\theta}{2}\right) & \cos \left(\frac{\phi-\theta}{2}\right) \\ \cos \left(\frac{\phi-\theta}{2}\right) & \sin \left(\frac{\phi-\theta}{2}\right)\end{array}\right)$,
$T_{\mathrm{B} b}=\mathrm{je}^{\mathrm{j} \frac{\theta}{2}}\left(\begin{array}{c}\mathrm{e}^{\mathrm{j} \phi} \sin \frac{\theta}{2} \mathrm{e}^{\mathrm{j} \phi} \cos \frac{\theta}{2} \\ \cos \frac{\theta}{2}\end{array}-\sin \frac{\theta}{2} . ~\right.$,
are the transfer functions of the BBs shown in Figure 2a,b, respectively (see Section S2 in the Supporting Information).

The simplest unitary optical processor that may be built from each BB with the aim of performing universal SU(2) transformations is also depicted in Figure 2. In the former case (Figure 2a), the $\mathrm{SU}(2)$ processor is implemented by its own BB without resorting to other additional elements, as reported in ref. ${ }^{[30]}$ In the latter case (Figure 2b), one PS must be added at the input of the BB to implement universal $\operatorname{SU}(2)$ operations, as explicitly indicated in ref. ${ }^{[25,34]}$ (although in ref. ${ }^{[16]}$ it is suggested that the additional PS must be included at the output of the BB, note that the same $S U(2)$ processor is finally found because of its $B B$ is the reversal version of the BB illustrated in Figure 2b). Accordingly, the corresponding transfer functions $T_{2 a(b)}$ of the above $\mathrm{SU}(2)$ systems are found to be $T_{2 a}=T_{\mathrm{B} a}$ and $T_{2 b}=\mathrm{e}^{\mathrm{j} \gamma / 2} T_{\mathrm{Bb}} R_{\hat{\Sigma}}( \pm \gamma)$, with $\gamma \in[0,2 \pi]$ and the sign $-(+)$ when the additional PS encoding the $\gamma$ parameter is integrated in the upper (lower) path, see Figure $2 b$ and Section S2 in the Supporting Information. In the following, let us analyze if $T_{2 a}$ and $T_{2 b}$ are arbitrary matrices of the $\mathrm{SU}(2)$ group.

It is straightforward to demonstrate that $T_{2 a}$ is not an arbitrary matrix of $\mathrm{SU}(2)$ because the number of real parameters in $T_{2 a}$ is 2 , lower than the number of independent real parameters required by the dimension of $\operatorname{SU}(2)$. This reason directly precludes the universal unitary property in the optical circuit shown in Figure 2a. Using the Euler rotation theorem, we can find specific rotations of the Bloch sphere that cannot be generated with $T_{2 a}$. For instance, performing the factorization $T_{2 a}=$ $\mathrm{e}^{\mathrm{j}(\phi+\theta) / 2} R_{\hat{\mathbf{x}}}(-\pi / 2) R_{\hat{\mathbf{z}}}(\phi-\theta) R_{\hat{\chi}}(-\pi / 2)$, we observe that the rotations around the $x$-axis of the Bloch sphere are fixed to a specific angle ( $-\pi / 2 \mathrm{rad}$ ) and, consequently, we may infer that there exist $R_{\widehat{\chi}}$ transformations that cannot be generated, e.g., $R_{\widehat{\chi}}(2 \pi)=-I$, where $I$ is the identity matrix.

Contrariwise, $T_{2 b}$ is parametrized with the number of degrees of freedom $(\{\gamma, \theta, \phi\})$ required by the dimension of $\mathrm{SU}(2)$. However, note that this is a necessary, but not a sufficient condition to guarantee the unitary universality because of such degrees of freedom must independently account for three arbitrary rotations of the Bloch sphere obeying the relation given by Equation (2). Along this line, the following noteworthy features of $T_{2 b}$ should be taken into consideration when the PS encoding the $\gamma$ parameter is added at the upper input of the BB:

1) Since $\operatorname{det}\left(T_{2 b}\right)=\mathrm{e}^{\mathrm{j}(\phi+\theta+\gamma)} \neq 1, T_{2 b} \notin \mathrm{SU}(2)$. Therefore, we must impose the additional condition $\phi+\theta+\gamma=2 \pi m$ ( $m \in$ $\mathbb{Z}$ ) on the set of parameters $\{\gamma, \theta, \phi\}$ to generate $\mathrm{SU}(2)$ transformations. As a consequence, the number of degrees of freedom in $T_{2 b}$ is reduced from 3 to 2 , lower than the ones required by the group dimension. Here, we find the first proof which indicates that $T_{2 b}$ is not an arbitrary matrix of $\mathrm{SU}(2)$. Likewise, it should be noted that an external synchronization is required to guarantee that the PSs associated to $\gamma, \theta$ and $\phi$ fulfill the aforementioned condition.
2) Taking $\gamma=2 \pi m-\theta-\phi$, then it follows that $T_{2 b}=$ $R_{\hat{z}}(-\phi-\pi) R_{\hat{y}}(\theta-\pi) R_{\hat{z}}(\phi+\theta)$, with $\alpha_{3} \equiv-\phi-\pi, \alpha_{2} \equiv \theta-\pi$ and $\alpha_{1} \equiv \phi+\theta$ being the rotation angles (see Section S2
in the Supporting Information). Since $\alpha_{1}=\alpha_{2}-\alpha_{3}, T_{2 b}$ does not encode three independent rotation angles, as required by the Euler rotation theorem. This implies that $T_{2 b}$ cannot completely describe the $\mathrm{SU}(2)$ group. Specifically, $T_{2 b}$ cannot generate an arbitrary rotation around the $z$-axis of the Bloch sphere. In a universal $\mathrm{SU}(2)$ matrix of the form $R_{\hat{\mathbf{z}}}\left(\alpha_{3}\right) R_{\hat{\mathrm{y}}}\left(\alpha_{2}\right) R_{\hat{\mathbf{z}}}\left(\alpha_{1}\right)$, with three independent arbitrary rotation angles, we will be able to generate any rotation around the $z$-axis by taking $\alpha_{2}=0$ given that $R_{\hat{\mathbf{z}}}\left(\alpha_{3}\right) R_{\hat{y}}(0) R_{\mathbf{z}}\left(\alpha_{1}\right)=R_{\hat{z}}\left(\alpha_{3}\right) R_{\mathbf{z}}\left(\alpha_{1}\right)=R_{\mathbf{z}}\left(\alpha_{3}+\alpha_{1}\right)$. In this way, varying the values of $\alpha_{1}$ and $\alpha_{3}$, we will generate infinite different $R_{\hat{z}}$ transformations. Nonetheless, setting $\alpha_{2}=0(\theta=\pi)$ in $T_{2 b}$, we obtain a single $R_{\mathbf{2}}$ transformation: $T_{2 b}=R_{\hat{z}}(-\phi-\pi) R_{\hat{z}}(\pi+\phi)=R_{\mathbf{z}}(0)=I$. Hence, there exist rotations around the $z$-axis that cannot be described by $T_{2 b}$, e.g., $R_{2}(2 \pi)=-I$. The same results can equivalently be validated by means of two different ways: i) verifying that $T_{2 b}$ cannot be restated as a rotation matrix of the Bloch sphere $R_{\hat{\mathrm{n}}}(\alpha)$ around an arbitrary unit vector $\hat{\mathbf{n}} \in \mathbb{R}^{3}$, (ii) demonstrating that the corresponding Lie algebra $\mathfrak{H u}(2)$ is not completely generated when applying the logarithmic mapping to $T_{2 b}$, see Section S2 (Supporting Information) for more details.

Alternatively, as commented above, the PS associated to $\gamma$ may be integrated in the lower input of the BB. This scenario gives rise to similar conclusions to those of the above system. In such circumstances, we must also impose the same mathematical condition on the set of parameters of $T_{2 b}$ to induce $\mathrm{SU}(2)$ transformations $(\phi+\theta+\gamma=2 \pi m, m \in \mathbb{Z})$, reducing the number of degrees of freedom from 3 to 2 and, therefore, being inviable to generate specific $\operatorname{SU}(2)$ transformations, in particular, arbitrary rotations around the $\gamma$-axis (see Section S2 in the Supporting Information).

So far, we have extensively discussed the main architectures of the BB reported in previous works, demonstrating that they lead to $S U(2)$ processors where the unitary universality is not hold. In the next subsection, we will provide a simple route to overcome this fundamental constraint.

## 4. Universal SU(2) Optical Processor and Building Block

Taking a closer look at Equations (2) and (3), two interesting remarks can be inferred. First, note that an infinite number of different $2 \times 2$ universal unitary processors and BBs may be constructed by taking different rotation vectors $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2}$. Each dupla ( $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2}$ ) will lead to an explicit architecture of the universal unitary processor and the BB, which will differ from other possible schemes in the number and the kind of integrated basic devices. Second, observe that there is a one-to-one correspondence between $T_{2}$ and $T_{\mathrm{B}}$ once the rotation vectors are selected. Hence, the design of the BB suffices to specify the optical circuit of the universal $U(2)$ (or $S U(2)$ ) processor based on the same rotation vectors.

In order to uncover a compact implementation of the BB, we will use the following design criteria: i) we must select rotation vectors which give rise to an optical circuit of the rotation matri$\operatorname{ces} R_{\hat{\mathrm{r}}_{1}}\left(\alpha_{1}\right)$ and $R_{\mathrm{r}_{2}}\left(\alpha_{2}\right)$ encompassing the lowest number of basic


Figure 3. Optical circuits of the basic rotation matrices of the Bloch sphere. a) Architecture of $R_{\hat{\mathrm{x}}}(\alpha)$ based on a tunable synchronous DC (the PSs integrated in its arms must induce the same effective index modulation in the fundamental mode of each waveguide). b) Architecture of $R_{\hat{\mathbf{z}}}(\alpha)$ using two PSs integrated in parallel uncoupled waveguides. c) Architecture of $R_{\hat{y}}(\alpha)$ built from the concatenation of the $R_{\hat{\mathbf{x}}}$ and $R_{\hat{\mathbf{z}}}$ transformations using the two possibilities provided by the Euler rotation theorem (Equation (2)).
devices ( $N$ ), ii) these basic devices must perform unitary signal operations and must be highly compactable and scalable in integrated photonics using current technology. The resulting scheme of the BB fulfilling the above criteria will be referred to as the minimal circuit architecture (MCA).

Basic optical devices satisfying the second criterion are PSs, DCs and MMIs, whose transfer matrices may induce rotations around the Cartesian axes of the Bloch sphere, as detailed below. Accordingly, the natural option to design the BB-MCA is $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2} \in$ $\{\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}}\}$.

Therefore, before delving into the specific structure of the BBMCA, we should first discuss the optical implementation of the basic rotation matrices $R_{\hat{\chi}}(\alpha), R_{\hat{y}}(\alpha)$ and $R_{\hat{\imath}}(\alpha)$, defined as ${ }^{[7,36]}$

$$
\begin{align*}
& R_{\hat{\chi}}(\alpha):=\left(\begin{array}{cc}
\cos \frac{\alpha}{2} & -j \sin \frac{\alpha}{2} \\
-j \sin \frac{\alpha}{2} & \cos \frac{\alpha}{2}
\end{array}\right), R_{\hat{y}}(\alpha):=\left(\begin{array}{cc}
\cos \frac{\alpha}{2} & -\sin \frac{\alpha}{2} \\
\sin \frac{\alpha}{2} & \cos \frac{\alpha}{2}
\end{array}\right), \\
& R_{\hat{z}}(\alpha):=\left(\begin{array}{cc}
e^{-j \frac{\alpha}{2}} & 0 \\
0 & e^{j \frac{\alpha}{2}}
\end{array}\right) . \tag{6}
\end{align*}
$$

The matrix $R_{\hat{\chi}}(\alpha)$ can be implemented by using a tunable synchronous DC, with PSs integrated in its arms which allow us to change the mode-coupling coefficient $\kappa$ of the DC inducing the same effective index modulation in the fundamental mode of each waveguide. The rotation angle $\alpha$ may be controlled via $\kappa(\alpha=2 \kappa L$, where $L$ is the length of the PSs, see Chapter 2 of ref. ${ }^{[14]}$ for a more technical discussion about the tunable DC). Hence, the number of basic devices required to implement $R_{\hat{x}}(\alpha)$ is $N_{\hat{x}}=3$ (1 DC and 2 PSs, see Figure 3a). Furthermore,
the matrix $R_{\hat{\mathbf{z}}}(\alpha)$ is the transfer function of a system composed by two parallel uncoupled waveguides, each of which integrates a PS inducing a phase shifting of $\pm \alpha / 2$ rad in the optical signals. Thus, $R_{\hat{\mathbf{z}}}(\alpha)$ requires $N_{\hat{\mathbf{z}}}=2$ basic devices (2 PSs, see Figure 3b). Finally, $R_{\hat{y}}(\alpha)$ can be built by concatenating the $R_{\hat{x}}$ and $R_{\hat{z}}$ transformations using Equation (2) in two distinct ways: $R_{\mathrm{y}}(\alpha)=$ $R_{\hat{\chi}}(\pi / 2) R_{\hat{z}}(-\alpha) R_{\hat{\chi}}(-\pi / 2)$ and $R_{\hat{y}}(\alpha)=R_{\hat{z}}(\pi / 2) R_{\hat{\chi}}(\alpha) R_{\hat{z}}(-\pi / 2)$. The former can be implemented by means of two 50:50 beamsplitters to induce the $R_{\hat{x}}( \pm \pi / 2)$ transformations (using MMIs or symmetric DCs) and 2 PSs to generate the $R_{\mathrm{z}}(-\alpha)$ matrix $\left(N_{\hat{y}}=2+2=4\right)$. The latter requires 4 PSs to perform the $R_{\hat{z}}( \pm \pi / 2)$ transformations along with the optical circuit shown in Figure 3a to produce the $R_{\hat{x}}(\alpha)$ matrix ( $N_{\hat{y}}=4+N_{\hat{x}}=7$ ). As seen in Figure 3c, the former factorization encompasses a lower $N_{\hat{y}}$ but the latter leads to the most compact architecture of $R_{\hat{y}}(\alpha)$ because of only a single coupler is required.

Once we have discussed the optical implementation of the basic rotation matrices, let us retrieve the initial goal of this subsection: the design of the BB-MCA. In line with the first design criterion indicated above, we must select rotation vectors $\hat{\mathbf{r}}_{1}, \hat{\mathbf{r}}_{2} \in\{\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}}\}$ which give rise to a BB architecture integrating the lowest number of basic devices ( $N=N_{\hat{\mathrm{r}}_{1}}+N_{\hat{\mathrm{r}}_{2}}$ ). Therefore, it is straightforward to infer that the most compact design of the BB requires to select $\hat{\mathbf{r}}_{1}=\hat{\mathbf{z}}$ and $\hat{\mathbf{r}}_{2}=\hat{\mathbf{x}}$, with $N=N_{\hat{\mathbf{z}}}+N_{\hat{\mathbf{x}}}=5$. Figure 4a depicts the optical circuit of the BB-MCA, whose transfer function is given by the matrix:
$T_{\mathrm{B}}=R_{\hat{\chi}}\left(\alpha_{2}\right) R_{\hat{\mathrm{z}}}\left(\alpha_{1}\right)=\left(\begin{array}{cc}\mathrm{e}^{-\mathrm{j} \frac{\alpha_{1}}{2}} \cos \frac{\alpha_{2}}{2} & -j \mathrm{e}^{\mathrm{j} \frac{\alpha_{1}}{2}} \sin \frac{\alpha_{2}}{2} \\ -j \mathrm{e}^{-\mathrm{j} \frac{\alpha_{1}}{2}} \sin \frac{\alpha_{2}}{2} & \mathrm{e}^{\mathrm{j} \frac{\alpha_{1}}{2}} \cos \frac{\alpha_{2}}{2}\end{array}\right)$.


Figure 4. BB-MCA and universal $\mathrm{SU}(2)$ and $\mathrm{U}(2)$ optical processors. a) Scheme of the BB-MCA and resulting universal $\operatorname{SU}(2)$ processor. b) Universal $U(2)$ processor built from the $S U(2)$ system depicted in (a). The PSs encoding $\delta$ can equivalently be integrated along with the PSs which perform the $R_{\hat{\mathbf{z}}}\left(\alpha_{3}\right)$ transformation at the output of the BB-MCA. c) BB architecture based on $50: 50$ beamsplitters (implemented via symmetric DCs or MMIs), constructed by using the optical circuit of $R_{\hat{y}}(\alpha)$ shown in the top of Figure $3 c$ to perform the second rotation required by Equation (3).

The architecture of the universal $\mathrm{SU}(2)$ processor is completed by adding the optical circuit associated to the rotation matrix $R_{\hat{2}}\left(\alpha_{3}\right)$ at the output of the BB (Figure 4a). As a result, we obtain a $2 \times 2$ system with transfer function $T_{2}=R_{\mathrm{z}}\left(\alpha_{3}\right) T_{\mathrm{B}}=$ $R_{\hat{\mathbf{z}}}\left(\alpha_{3}\right) R_{\hat{\mathbf{x}}}\left(\alpha_{2}\right) R_{\hat{\mathbf{z}}}\left(\alpha_{1}\right)$ being able to perform any $\mathrm{SU}(2)$ transformation. Here, in contrast to the scheme of Figure 2b, it is not required an external synchronization between the PSs to perform $\operatorname{SU}(2)$ transformations given that $\operatorname{det}\left(T_{2}\right)=1, \forall \alpha_{1,2,3} \in[0,2 \pi]$. The same optical circuit can be employed to perform universal $\mathrm{U}(2)$ transformations by including two additional PSs at the outputs (or inputs) in order to implement a global phase shifting $\mathrm{e}^{\mathrm{j} \delta}$. Along this line, it should be noted that $\delta$ can optionally be encoded along with $\alpha_{3}$ (or $\alpha_{1}$ ) in the corresponding PSs, see Figure 4 b . However, in such a case, a mutual synchronization (e.g., via software ${ }^{[37,38]}$ ) is essential between these PSs to be able of tuning $\alpha_{3}$ (or $\alpha_{1}$ ) and $\delta$ independently.

As commented above, additional BB candidates may be explored by selecting different rotation vectors in Equation (3). As an illustrative example, in Figure 4 c it is shown a BB based on fixed couplers (50:50 beamsplitters implemented via MMIs or symmetric DCs), whose transfer function is directly obtained by replacing $R_{\hat{\mathbf{x}}}\left(\alpha_{2}\right)$ with $R_{\hat{y}}\left(\alpha_{2}\right)$ in Equation (7). Nevertheless, the manufacturing of this BB will approximately require the double
footprint than that of the BB depicted in Figure 4a because of a twice number of couplers must be integrated in this BB architecture.

## 5. Conclusion

Overall, these results demonstrate that the programmable linear optical processors built from the existing architectures of the BB do not furnish a $2 \times 2$ universal unitary functionality and, in order to circumvent this fundamental limitation, we blaze a trail for designing BB schemes that guarantee the unitary universality in $2 \times 2$ optical processors. The theoretical framework presented here is a first research step to: i) establish the fundamentals of analog optical gates and, ${ }^{[11,14]}$ ii) build a systematic approach for the design of integrated photonic signal processing devices and subsystems that can be directly translated into commercial development kits. With the obvious differences, we expect that the future availability of such an approach can render similar benefits as those ripped by the science and technology of electronic integrated circuit design through the exploitation of the principles of Boole's algebra.

By virtue of the Euler rotation theorem, it is shown that the optical architectures of the BB proposed in previous works (Figure 2) lead to $2 \times 2$ optical processors that cannot describe three independent rotations around two nonparallel axes of the Bloch sphere and, as a result, such schemes cannot induce arbitrary $\mathrm{SU}(2)$ transformations. In contrast, in our proposal (Figure 4), three independent rotations around two Cartesian axes of the Bloch sphere are correctly encoded by the transfer function of the optical circuits, an arbitrary matrix of $\operatorname{SU}(2)$, guaranteeing the complete description of this Lie group while leveraging the existing mainstream integrated optical components. Moreover, it is worth mentioning that the kind and the number of basic devices required to implement a specific architecture of the $B B$ can be accommodated by using different rotation vectors in Equation (3). Table 1 summarizes the most suitable and compact BB schemes that can be implemented by using PSs and couplers (MMIs, symmetric DCs or tunable synchronous DCs). In the same line, other basic devices such as tunable asynchronous DCs (inducing rotations around a reconfigurable arbitrary unit vector $\hat{\mathbf{n}}$ of the Bloch sphere ${ }^{[14]}$ ) and optical resonators (that may perform the same functionality as that of couplers and $\mathrm{PSs}^{[39]}$ ) might be explored to construct novel structures of the BB. In any case, a BB architecture must be built from basic devices with negligible insertion losses or, otherwise, the unitary nature of the transformations will not be preserved, leading to energy-inefficient optical processors requiring amplification stages.

On the other hand, it is natural to wonder about the possibility of designing a more compact BB than the architecture proposed in Figure 4a by using a different unitary factorization from the Euler rotation theorem. Diverse $2 \times 2$ unitary factorization techniques can be found in the mathematical literature, ${ }^{[40-44]}$ but all of them lead to optical schemes of the BB integrating a higher number of basic devices than in our proposal (see Section S3 in the Supporting Information).

Finally, note that these results may establish a starting point to revisit the $n \times n$ unitary universality for the case $n>2$ in current programmable linear optical processors (based on well-known optical architectures of high-dimensional unitary

Table 1. Suitable BB architectures proposed in this work and number of integrated basic devices. The design of the basic rotation matrices (Equation (6)) is also included for clarity in the results. A $2 \times 2$ universal unitary optical system may be built from these BBs by adding a $R_{\hat{\mathbf{z}}}\left(\alpha_{3}\right)$ transformation at their outputs.

| System | Transfer matrix | Number of couplers | Number of phase shifters | Total number of basic devices |
| :---: | :---: | :---: | :---: | :---: |
| Basic rotation (Figure 3a) | $R_{\hat{\mathbf{x}}}(\alpha)$ | 1 | 2 | 3 |
| Basic rotation <br> (Figure 3b) | $R_{\hat{\mathbf{z}}}(\alpha)$ | 0 | 2 | 2 |
| Basic rotation <br> (Figure 3c, top) | $R_{\hat{\mathbf{y}}}(\alpha)=R_{\hat{\mathbf{x}}}\left(\frac{\pi}{2}\right) R_{\hat{\mathbf{z}}}(-\alpha) R_{\hat{\mathbf{x}}}\left(-\frac{\pi}{2}\right)$ | 2 | 2 | 4 |
| Basic rotation <br> (Figure 3c, bottom) | $R_{\hat{\mathbf{y}}}(\alpha)=R_{\hat{\mathbf{z}}}\left(\frac{\pi}{2}\right) R_{\hat{\mathbf{x}}}(\alpha) R_{\hat{\mathbf{z}}}\left(-\frac{\pi}{2}\right)$ | 1 | 6 | 7 |
| BB-MCA <br> (Figure 4a) | $T_{\mathrm{B}}=R_{\hat{\mathbf{x}}}\left(\alpha_{2}\right) R_{\hat{\mathbf{z}}}\left(\alpha_{1}\right)$ | 1 | 4 | 5 |
| BB <br> (Figure 4c) | $T_{\mathrm{B}}=R_{\hat{\mathbf{y}}}\left(\alpha_{2}\right) R_{\hat{\mathbf{z}}}\left(\alpha_{1}\right)$ | 2 | 4 | 6 |

matrix transformations, where the BBs are connected in a mesh configuration ${ }^{[15,16]}$ ) by combining the concept of multidimensional rotation matrices ${ }^{[4]}$ along with different factorization algorithms of the $U(n)$ Lie group. ${ }^{[18,40-44]}$ In such a scenario, our definition of the BB (Equation (3)) also guarantees the unitary universality of the $U(2)$ processors integrated in the whole system, provided that the first rotation in $T_{\mathrm{B}}$ is performed around the $z$-axis of the Bloch sphere (note that the PSs that implement this rotation are integrated in uncoupled waveguides (Figure 3b) and, consequently, such a scheme can set the connection of a given BB with two independent BBs of the mesh and may simultaneously generate a $R_{\hat{z}}$ transformation along with a global phase shifting).

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

Data sharing is not applicable to this article as no new data were created or analyzed in this study.

## Keywords

integrated optics, programmable photonics, quantum photonics, signal processing
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