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**PASSIVE AND TRANSPASSIVE BEHAVIOUR OF ALLOY 31 IN A HEAVY
BRINE LiBr SOLUTION**

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The passive and transpassive behaviour of Alloy 31, a highly-alloyed austenitic stainless steel (UNS N08031), has been investigated in a LiBr heavy brine solution (400 g/l) at 25° C using potentiostatic polarisation combined with electrochemical impedance spectroscopy and Mott-Schottky analysis. The passive film formed on Alloy 31 has been found to be *p*-type and/or *n*-type in electronic character, depending on the film formation potential. The thickness of the film formed at potentials within the passive region increases linearly with applied potential. The film formed at transpassive potentials is thinner and more conductive than the film formed within the passive region. These observations are consistent with the predictions of the Point Defect Model for passive and transpassive films on metals and alloys.

Keywords: stainless steel; passive film; transpassivity; EIS; Mott-Schottky

1. INTRODUCTION

Energy demand for refrigeration and air-conditioning systems has been increasing in recent years, due to the demand of higher comfort conditions inside buildings [1-4]. This has led to a widespread use of air conditioning systems based on compression technology, with the associated negative impact on the environment (ozone layer depletion and CO₂ emissions). Refrigeration absorption systems which use highly concentrated lithium bromide solutions as absorbent (LiBr absorbs the water vapour coming from the evaporator) are a suitable alternative to compression systems. However, lithium bromide/water absorption systems also have some drawbacks, such as the severe corrosion problems on metallic components due to the aggressiveness of bromide ions [5-12]. Therefore, highly corrosion resistant materials have been developed for the construction of LiBr absorption machines, such as Alloy 31 (UNS N08031) [13], a highly alloyed austenitic stainless steel that consists of much larger amounts of alloying elements (26.75% Cr, 31.85% Ni) in comparison with the typical 18% Cr, 10-12% Ni austenitic stainless steels.

The enhanced corrosion resistance of Alloy 31 is attributed to the formation of a thin and stable oxide film on its surface, known as passive film. Therefore, passivity is defined as the decrease in the corrosion rate of a metal or alloy resulting from the formation of a thin and tenacious protective film due to the oxidation of the metal. From an engineering point of view, passivity of metals is a phenomenon of utmost importance. The Point Defect Model (PDM) successfully accounts for the properties of the passive state [14-19]. According to the PDM, passive films contain a high concentration of point defects (vacancies and interstitials) and behave as incipient

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semiconductors. The **type**, concentration and distribution of these vacancies determine the properties of passive films and, as a consequence, the behaviour of metals and alloys against corrosion. Vacancies generate and annihilate at the interfaces, which are normally separated by no more than a few nanometers (passive film thickness). The electric field strength across the film depends on the chemical and electrical properties of the film, and is independent of applied potential and film thickness. The PDM also provides a number of diagnostic criteria that can be used to determine the principal crystallographic defects within the passive film.

The objective of this work is to examine the effect of formation potential on the passive and transpassive behaviour of Alloy 31 in a heavy brine LiBr solution (400 g/l LiBr, **which is a typical LiBr concentration inside absorption machines**) at 25 °C, using potentiostatic polarisation, EIS measurements and Mott-Schottky analysis

2. EXPERIMENTAL PROCEDURE

The material tested was the highly alloyed austenitic stainless steel Alloy 31 (UNS N08031: **Cr 26.75 (wt%), Ni 31.85 (wt%), Mn 1.50 (wt%), Si 0.10 (wt%), Mo 6.60 (wt%), Cu 1.21 (wt%), Fe 31.43 (wt%), S 0.002 (wt%), P 0.017 (wt%), C 0.005 (wt%), N 0.193 (wt%)**), provided by ThyssenKrupp VDM. The Alloy 31 electrodes were cylindrically shaped (8-mm in diameter) and covered with a polytetrafluoroethylene (PTFE) coating. The area exposed to the solution was 0.5 cm². All specimens were wet abraded from 500 to 4000 SiC grit, and finally rinsed with distilled water. The samples were tested in a 400 g/l (4.61 M) LiBr solution (pH = 6.80), prepared from LiBr **salt** (98 wt%), from PANREAC.

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2 The electrochemical measurements were carried out with an Autolab PGSTAT302N
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4 potentiostat. An Ag/AgCl (3M KCl) electrode served as the reference electrode and a
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6 platinum wire served as the counter electrode. Before the potentiostatic passivation
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8 tests, the surface of the samples was initially pretreated cathodically at $-1 V_{Ag/AgCl}$ for 30
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10 min. Afterwards, the working electrode was polarised at different film formation
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12 potentials within the passive region (from $-0.3 V_{Ag/AgCl}$ to $0.1 V_{Ag/AgCl}$) and within the
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14 transpassive region (from $0.15 V_{Ag/AgCl}$ to $0.4 V_{Ag/AgCl}$) of Alloy 31 for 1 hour to form a
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16 steady-state film. Polarisation curves of Alloy 31 in the 400 g/l LiBr solution were
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18 presented elsewhere [20]. In these curves, passive and transpassive regions can be
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20 observed.
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29 EIS experiments were conducted over a frequency range from 100 kHz to 10 mHz with
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31 a 10 mV (peak to peak) signal amplitude. Mott–Schottky plots were subsequently
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33 obtained by sweeping the potential from the film formation value in the negative
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35 direction with potential steps of 50 mV, at a frequency of 5 kHz with an amplitude
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37 signal of 10 mV. A high scanning rate was used to avoid electroreduction of the passive
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39 film and changes in film thickness during the measurements. At a sufficiently high
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41 scanning rate, the defect structure within the passive film is “frozen-in”, which avoids
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43 the defect density from being affected by potential [21-23].
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52 **3. RESULTS AND DISCUSSION**

53 **Potentiostatic passivation tests**

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Potentiostatic passivation tests were conducted at several formation potentials within the passive (from -0.3 to 0.1 V) and transpassive (from 0.15 to 0.4 V) regions of Alloy 31 [20]. As an illustration, **Figure 1** shows the current density transients recorded during the potentiostatic passivation tests at -0.3, -0.1 and 0.1 V (within the passive region) and at 0.4 V (within the transpassive region). Regardless of the applied potential, the current density of Alloy 31 decreases exponentially with time as the film grows on the electrode surface, and eventually reaches a very low steady-state value (i_{ss}) of the order of 0.1-0.3 $\mu\text{A}/\text{cm}^2$ after 1 hour of film formation. In the inserts in **Figure 1** it can be observed that current density values increase as the applied potential increases, especially at the potential located in the transpassive region. In previous studies [20], a current density peak was observed in the polarisation curves of Alloy 31 in heavy brine LiBr solutions, before the sharp increase in current density due to the onset of pitting corrosion (**Figure 2**). This peak has been related to the transpassive dissolution of Cr-containing species. Thus, the higher values of current density obtained at 0.4 V can be related to the transformation of Cr oxides and hydroxides to form chemical species in a valence state higher than that in the primary passive film. It is important to remark that at these potentials within the transpassive region, which are lower than the pitting potential [20], the electrode examination revealed no damage on its surface, indicating that the passive film was not destroyed.

The PDM predicts that the steady-state passive current density, i_{ss} , contains three components corresponding to the generation and movement of cation interstitials, cation vacancies and oxygen vacancies through the film [19, 24]. According to this model, $\ln i_{ss}$ will vary linearly with film formation potential, E_f , provided that cation interstitials, cation vacancies or oxygen vacancies dominate ionic charge transfer

1 through the film. A plot of $\ln i_{ss}$ vs E_f is shown in **Figure 3**. Two different zones can be
 2 observed in this diagram, corresponding to the passive region (Region I) and to the
 3 transpassive region (Region II). In both regions, a linear dependence of $\ln i_{ss}$ on the film
 4 formation potential is observed, with the current density increasing with increasing
 5 potential, although the slope of the line in Region II (1.423 V^{-1}) is higher than that in
 6 Region I (0.803 V^{-1}). The dependence of $\ln i_{ss}$ on the formation potential provides a
 7 diagnostic criterion that can be used to identify the dominant charge carriers in the film
 8 under steady-state conditions and to indicate the kinetic nature of the processes that
 9 generate and annihilate these defects at the interfaces [17]. According to this criterion, a
 10 linear $\ln i_{ss}$ vs. E_f dependence with positive slope, as is the case in **Figure 3**, indicates
 11 that there is a preponderance of cation vacancies over cation interstitials and oxygen
 12 vacancies in the passive film, that is, the majority of the current is carried by cation
 13 vacancies. This preponderance is more evident at potentials in the transpassive region
 14 (Region II), since additional cation vacancies are produced in this region by the ejection
 15 of cations from the passive film into the electrolyte, involving a change in the oxidation
 16 state of the ion. In the case of chromium-containing alloys (such as Alloy 31), the cation
 17 ejection from the passive film takes place via the following reaction [24-26]:



44 Notice that the Kroger-Vink notation is used in eq. (2) to describe the various species in
 45 the system, with Cr_{Cr} and $\text{V}_{\text{Cr}}^{3'}$ indicating a Cr(III) cation in a normal site on the cation
 46 sub-lattice and a cation vacancy on the same sub-lattice of the passive film,
 47 respectively. Reaction (2) leads to enhanced cation transmission through the passive
 48 film, and hence to a higher current density [24]. As mentioned above, the reaction in eq.

(2) does not involve the destruction of the passive film, since it occurs at potentials lower than the pitting potential, E_p , before the onset of stable pitting corrosion [20].

For cation vacancy conducting films, the PDM predicts that the $\ln i_{SS}$ vs E_f relationship within the passive range has the form:

$$i_{SS} = \delta F k_{cat}^0 \exp(\alpha_{cat} \alpha \delta \gamma E_f) \exp(\alpha_{cat} \beta \delta \gamma pH) \quad (3)$$

where δ is the charge of the cation ejected from the passive film (3 in the case of Cr^{3+}), F is Faraday's constant (96485.34 C mol⁻¹), k_{cat}^0 and α_{cat} are the standard rate coefficient and the transfer coefficient, respectively, for the cation ejection reaction at the passive film/electrolyte interface ($Cr_{Cr} \rightarrow Cr^{3+} + V_{Cr}^{3'}$), α is the polarizability of the passive film/electrolyte interface (the dependence of the potential drop across the passive film/electrolyte interface, $\phi_{f/e}$, on the applied potential, E_f), $\gamma = F/RT$ and β is the dependence of the potential drop across the film/electrolyte interface, $\phi_{f/e}$, on pH.

According to eq. (3), a plot of $\ln i_{SS}$ vs. E_f in the passive region should be linear with a slope of $\alpha_{cat} \alpha \delta \gamma$. With $\alpha = 0.7$ [24-26], $\delta = 3$ and $\gamma = 39.32 \text{ V}^{-1}$, the transfer coefficient for the cation ejection reaction at the passive film/electrolyte interface, α_{cat} , can be calculated from the slope (0.803 V^{-1}) in the passive region (Region I), yielding $\alpha_{cat} = 0.01$. Low transfer coefficient values have usually been found for passive films on iron and Fe-Cr alloys [25, 27, 28]. Since the transfer coefficient is a measure of the location of the transition state relative to the stable states, the rather small value of α_{cat} indicates that charge separation is not highly developed in the transition state for the cation ejection reaction at the passive film/electrolyte interface, that is, the transition state only occurs at a small displacement of the cation from its normal site within a cation vacancy

1 in the passive film surface [29, 30]. From the intercept at 0.0 V_{SHE} of the straight line in
2 Region I ($\ln \delta F k_{cat}^0 + \alpha_{cat} \beta \delta \gamma pH$), the value of k_{cat}^0 can be calculated. With pH = 6.80
3 and $\beta = -0.005$ V [24-26], the standard rate coefficient for the cation ejection reaction at
4 the film/electrolyte interface gives a value of $k_{cat}^0 = 2.95 \cdot 10^{-13}$ mol s⁻¹ cm⁻².
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10 **EIS measurements**

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12 Electrochemical impedance spectra were measured at different formation potentials in
13 the passive and transpassive regions. By way of illustration, Nyquist and Bode-phase
14 plots are shown in **Figure 4** at -0.3, -0.1, 0.1 and 0.4 V. In all cases, EIS diagrams
15 exhibit a typical passive state shape characterised by high impedance values with phase
16 angle values close to 90 degrees, suggesting that a highly stable film formed on all the
17 electrodes [31-34]. There are no differences between the EIS spectra at the potentials
18 within the passive region (-0.3, -0.1 and 0.1 V). However, at 0.4 V, the EIS spectrum
19 shows that impedance in the transpassive region is significantly lower than in the
20 passive region. Besides, the values for the phase angle are slightly lower at 0.4 V.
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22 Assuming that the high impedance values obtained in the passive region are due to the
23 passive film, the reduction in impedance within the transpassive region is consistent
24 with a loss of protectiveness against corrosion. In fact, transpassive dissolution of the
25 alloying elements such as Cr results in their depletion in the passive film, which is
26 closely related to the passive film breakdown [35].
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51 The stability of the system is crucial for the validity of EIS measurements. Kramers–
52 Kronig (K–K) transforms can be used as an independent validity check of the
53 impedance data (that is, compliance of the system with the constraints of the Linear
54 Systems Theory (LST)). Kramers–Kronig transforms have been applied to the
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1 experimental impedance data by transforming the real axis into the imaginary axis and
 2 the imaginary axis into the real axis and then comparing the transformed quantities to
 3 their respective experimental data. Typical Kramers–Kronig transforms of the
 4 impedance data obtained at -0.1 V are displayed in **Figure 5**. It can be seen that the K-K
 5 transforms are similar, especially at low frequencies, following the same **trend** as the
 6 experimental values. K–K transforms demonstrate that the system (Alloy 31/LiBr)
 7 remains stable during the measurement time. This condition is necessary for the analysis
 8 of the data in terms of electrical analogues.

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 21 The equivalent electric circuit used to interpret EIS spectra of anodically formed passive
 22 films is shown in **Figure 6**. In this equivalent circuit, R_S represents the electrolyte
 23 resistance, R_I and CPE_I correspond to the charge transfer resistance and the capacitance
 24 of the passive film/electrolyte interface, respectively, and Z_W is a Warburg component,
 25 which has been used to interpret the transport of vacancies within the passive film, in
 26 the frame of the Point Defect Model [14, 16, 36-38]. The Warburg impedance is
 27 represented by means of an Open-Boundary Finite Length Diffusion element (OFLD)
 28 [37, 39-46], which models dimensional diffusion through a layer of finite thickness with
 29 absorbing boundary condition. The equation of the OFLD element is [39-46]:

$$Z_w (OFLD) = \frac{R_w \tanh(B\sqrt{j\omega})}{B\sqrt{j\omega}} \quad (4)$$

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 53 where $B = \delta/(D)^{1/2}$, D is the diffusion coefficient of vacancies, δ is the diffusion layer
 54 thickness and R_w is the Warburg resistance.
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1 A constant-phase element (CPE) representing a shift from the ideal capacitor has been
2 used instead of the capacitance itself. The impedance of a constant-phase element is
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$$Q = Z_{CPE} = [C(j\omega)^n]^{-1} \quad (5)$$

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15 where n , defined as a CPE power, is an adjustable parameter that lies between -1 and 1.
16 For $n = 1$ the CPE describes an ideal capacitor, and for $n = 0$ the CPE is an ideal
17 resistor. When $n = 0.5$ the CPE represents Warburg impedance with diffusional
18 character and for $0.5 < n < 1$ the CPE describes a frequency dispersion of time constants
19 due to local heterogeneities in the dielectric material. A pure inductance yields $n = -1$.
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29 The CPE used in the equivalent electric circuit of **Figure 6** has been converted into a
30 pure capacitance (C) through equation [28, 31, 47]:
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$$C = Q^{1/n} (R_s^{-1} + R_1^{-1})^{(n-1)/n} \quad (6)$$

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42 where $Q = Z_{CPE}$ (eq. (5)).
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51 The parameters of the equivalent circuit of **Figure 6** obtained from the fitting procedure
52 are shown in **Table 1**. In the passive region, the charge transfer resistance, R_1 , varies
53 with film formation potential, increasing significantly within the passive range. This
54 **shows a slower rate of** reactions taking place at the passive film/electrolyte interface,
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indicating that the passive films formed at higher passive potentials are more protective than those formed at lower passive potentials. The interfacial capacitance, C_I , is almost constant in this region. The values of the exponent n_I are between 0.93-0.94 in the passive region, indicating a considerable homogeneity of the passive film surface. The Warburg resistance, R_W , is non-sensitive to film formation potential within the passive region, because defect transport is primarily due to migration under the influence of the electric field and the field strength is postulated (in the PDM) to be independent of the applied potential [29, 48].

In the transpassive region, R_I decreases and C_I increases slightly at 0.4 V, which suggest worse protective properties of the films formed at high potentials. Furthermore, the Warburg impedance, R_W , is potential dependent, decreasing significantly as formation potential becomes more positive. The decrease of R_W could be explained by the progressive transformation of the compact passive film into a porous transpassive film [29], which forms by the oxidative ejection of Cr(III) from the passive film to form Cr(VI), according to eq. (2); the values of the exponent n_I , which are lower in the transpassive region than in the passive region, support the formation of a porous film.

Capacitance results

The electrochemical capacitance of the passive film/electrolyte interface was measured as a function of the applied potential to assess the semiconducting properties of the passive films formed on Alloy 31. Since the space charge region developed in the passive film and the Helmholtz layer can be considered as two capacitors in series, the measured capacitance of the film/electrolyte interface can be written as [49, 50]:

$$\frac{1}{C} = \frac{1}{C_{SC}} + \frac{1}{C_H} \quad (7)$$

where C_{SC} is the capacitance of the space charge layer and C_H the capacitance of the Helmholtz layer.

It is important to remark that capacitance is frequency dependant [51-56]. Several causes for the frequency dispersion have been proposed: (i) a non-uniform distribution of point defects through the passive film [52, 55, 57]; (ii) the contribution of surface states to the capacitance response (adsorption of anions, e.g. chlorides, or other species) [52, 55]; (iii) the ionic part of the space charge layer, which gives a contribution only at low frequencies due to the low ionic mobility, particularly in heavily doped materials where the space charge region is very thin (passive films generally satisfy these requirements) [52, 54, 58]; (iv) dielectric relaxation phenomena which occur throughout the space charge layer and the Helmholtz layer [50, 52, 53, 55]; (v) an amorphous and strongly disordered semiconductor nature of passive films, characterised by a high density of localised states between the valence and the conduction band and whose charging leads to a strong frequency dependent capacitance behaviour [51, 52, 57, 58]; (vi) presence of deep donor states [52, 53, 58].

Figure 7 shows the capacitance-potential curves obtained at -0.1 V and at different frequencies. It can be observed that there is a strong frequency dependence at low frequencies (capacitance curves shift to higher values with decreasing frequencies), but the capacitance becomes almost independent of frequency at approximately 5 kHz. Therefore, a value of 5 kHz has been used in this work to eliminate capacitance dependence on frequency.

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2 **Figure 8** shows the capacitance-potential relationship at a frequency of 5 kHz of the
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4 **passive film formed** at -0.1 V (passive region) and at 0.4 V (transpassive region). These
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6 curves are representative of the results obtained at the different applied potentials in
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8 both passive and transpassive regions.
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14 In the case of the film formed at 0.4 V, the capacitance falls continuously from 0.4 to -
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16 0.4 V. The initial higher capacitance value can be attributed to either the strong
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18 dependence of the current density on potential in the transpassive region (see **Figure 3**)
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20 or the development of an inversion layer in the passive film so it becomes conductive
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22 [51, 52]. In the potential range from -0.4 V to -1.3 V, both diagrams have a similar
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24 shape. Below -0.4 V, the capacitance values start rising as a consequence of the
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26 reduction of the space charge layer thickness, reaching a maximum value of 20-22 μF
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28 cm^{-2} at a potential around -0.85 V. In this narrow potential region (the flat-band
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30 potential, E_{FB}) the contribution of the space charge layer to the measured capacitance is
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32 limited and the Helmholtz layer dominates the capacitance response. At potentials more
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34 negative than -0.85 V the capacitance values decrease as the space charge layer thickens
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36 again.
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46 It is usually assumed that the Helmholtz layer capacitance is so large compared with the
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48 space charge layer capacitance that the total capacitance measured can be treated as the
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50 space charge layer capacitance and the potential drop caused by the applied potential
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52 occurs entirely within the space charge region. However, several studies [49, 59] have
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54 shown that a significant part of the potential difference at the semiconductor/electrolyte
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56 interface extends to the Helmholtz layer in the solution. Therefore, C_H should not be
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neglected, particularly in highly doped semiconductors, such as passive films [49, 50].

In this case, the passive film/electrolyte interface can be described by the Mott-Schottky expressions [49, 50, 52]:

$$\frac{1}{C^2} = \frac{1}{C_H^2} + \frac{2}{\varepsilon\varepsilon_0 e N_D} \left(E - E_{FB} - \frac{kT}{e} \right) \quad \mathbf{n\text{-type}} \quad (8a)$$

$$\frac{1}{C^2} = \frac{1}{C_H^2} - \frac{2}{\varepsilon\varepsilon_0 e N_A} \left(E - E_{FB} - \frac{kT}{e} \right) \quad \mathbf{p\text{-type}} \quad (8b)$$

where ε is the dielectric constant of the passive film (a value of 15.6 has been assumed for the chromium and iron oxides formed on austenitic stainless steels [52]), ε_0 is the vacuum permittivity ($8.85 \cdot 10^{-14}$ F/cm), e is the electron charge ($1.60 \cdot 10^{-19}$ C), N_D and N_A are respectively the donor and acceptor densities, E_{FB} is the flat-band potential k is the Boltzmann constant ($1.38 \cdot 10^{-23}$ J/K) and T is the absolute temperature.

Figure 9 shows the plot of C^{-2} vs. potential, E , for the films formed on Alloy 31 at different potentials within the passive and transpassive regions. Mott-Schottky plots reveal the existence of two or three regions, depending on the film formation potential, where a Mott-Schottky type behaviour can be observed (straight lines at low and high potentials). At potentials below -0.85 V (the flat-band potential, E_{FB}), straight lines with negative slopes can be observed. These lines are more evident as the film formation potential increases, and are representative of the behaviour of a p -type semiconductor, whose predominant acceptor species in stainless steels are chromium vacancies, $V_{Cr}^{3'}$. At potentials above -0.85 V, another linear region appears, with positive slopes, which

1 illustrate the electrochemical behaviour of an *n*-type semiconductor, whose predominant
2 donor species are oxygen vacancies, $V_O^{\bullet\bullet}$, and/or cation interstitials, Cr_i^{X+} .
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7 At the formation potentials of 0.1 and 0.2 V, a change in the positive slope can be
8 observed, indicating *n*-type semiconductivity with two kinds of donors (**Figure 9**). The
9 existence of two donor levels has already been suggested for passive films on stainless
10 steels [60-63]. In the present study, the deep donors that characterise the second linear
11 region with positive slope at higher potentials are highly related to the formation of Cr^{6+}
12 ions due to transpassivity of Cr species, as other authors have observed [60, 61, 64]. At
13 formation potentials higher than 0.2 V there is a progressive change in the sign of the
14 linear region slope at high potentials, going from positive to negative values. This fact
15 indicates a modification in the electronic properties of the passive film in the
16 transpassive region, from *n*-type to *p*-type semiconductivity, and is related to an
17 increase in the conductivity of the film due to the solid state oxidation of Cr(III) to
18 Cr(VI) [65, 66]. The change in the semiconducting behaviour can be explained by the
19 generation of cation vacancies (which are electronic acceptors and *p*-type dopants) at
20 the film/solution interface through reaction (2) [26].
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44 According to Hakiki [50] the electronic structure of the passive films formed on
45 stainless steels can be described by a bilayer model composed of a *n*-type outer region
46 of iron oxide (Fe_2O_3) and hydroxide near the solutions, and a *p*-type inner region of
47 chromium oxide (Cr_2O_3) near the metal. Tsuchiya [67] have also used a bilayer model
48 to describe the semiconducting behaviour of passive films formed on Fe-Cr alloys in
49 sulphuric acid solutions, assuming that these passive films were composed of an outer
50 *n*-type hydroxide layer $Cr(OH)_3$ and an inner *p*-type oxide layer of Cr_2O_3 . However, the
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bilayer structure of passive films formed on stainless steels has been demonstrated to be more complex [68-75]. The *n*-type outer region would be enriched in Fe³⁺ species, such as Fe₂O₃, FeO(OH) and Fe(OH)₃, as well as Cr(OH)₃ and CrO(OH). The *p*-type inner region would consist of an anhydrous mixed Fe-Cr oxide, most probably with a spinel structure, e.g. FeCr₂O₄ (chromite) [69]. This spinel should be enriched in Cr, with the octahedral sites preferentially occupied by Cr(III) and Fe(II) [68, 71], or even Fe(III) [69], so its structure should be represented in a more accurate formula as Fe(II)[Cr(III)_xFe(III)_(1-x)]₂O₄, where 0 < x ≤ 1 [69]. Nickel may also replace iron and chromium in the spinel [68].

As it has been mentioned above, at -0.3 and -0.2 V the slopes of the straight lines below the E_{FB} are rather small (**Figure 9**), though these lines are more marked at higher formation potentials. It has been reported in the literature [76-79] that the concentration of Cr(III) oxide in the passive films formed on stainless steels and Cr alloys increases with increasing formation potential, in the passive region (at higher potentials, transpassive dissolution of chromium species occurs). The increase of Cr(III) oxide concentration within the passive film implies a decrease in the number of cation vacancies, $V_{Cr}^{3'}$, and consequently higher negative slopes in the *p*-type semiconductivity zone below the E_{FB} .

The $1/C^2$ vs. E plots shown in **Figure 9** exhibit a minimum in the flat-band potential region. Therefore, within the passive range, the capacitance should not be derived from a single space charge region, but from at least two regions [67]. In a metal/film/electrolyte system, space charge regions can be formed in the film either at the film/electrolyte interface or at the metal/film interface [80].

1 From Mott-Schottky diagrams, the passive system can be divided into three interfaces:
2 (I) metal/inner layer; (II) inner layer/outer layer; (III) outer layer/electrolyte. **Figure 10**
3 shows a schematic representation of the energy-band model corresponding to the
4 behaviour observed at film formation potentials within the passive region. At interfaces
5 (I) and (III), two space charge regions develop in the inner and outer layers,
6 respectively, depending on the applied potential. At potentials more positive than the
7 flat-band potential (E_{FB}), the conduction and valence bands bend upwards at the outer
8 layer/electrolyte interface (III), promoting the development of a **depleted** space charge
9 region, while there is an accumulation of holes at interface (I), which behaves as an
10 ohmic contact. On the contrary, at potentials more negative than E_{FB} , the bands bend
11 downwards and the situation previously described is reversed. Thus, at the outer
12 layer/electrolyte interface (III) an accumulation of electrons occurs, with a consequent
13 ohmic behaviour of the outer layer of the film, which converts from a semiconductor to
14 a metal-like conductor. Therefore, the capacitance measurements performed in the
15 potential region $E < E_{FB}$ reflect the semiconducting properties of the inner layer of the
16 passive film. According to this model, the passive film behaves as a $p-n$ heterojunction
17 where the space charge regions are not in contact with each other, but localised at the
18 interfaces (I) and (III).
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46 Donor and acceptor densities (N_D and N_A) can be calculated for n -type and p -type
47 semiconductors using equations (9a) and (9b), respectively. **Table 2** shows the values of
48 N_{A1} and N_{D1} calculated from the slopes of the linear zones below and above the E_{FB} in
49 **Figure 9**, respectively. **Table 2** also shows the values of N_{D2} , calculated from the
50 second linear region with positive slope at the formation potentials from 0.1 to 0.25 V,
51 and N_{A2} , calculated from the linear region with negative slope at the formation
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1 potentials from 0.3 to 0.4 V. Finally, the last column of **Table 2** gathers the total density
2 of defects in the outer layer of the passive film, calculated as $N_{D1} + N_{D2}$ or $N_{D1} + N_{A2}$,
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4 depending on the semiconducting behaviour at high potentials within the transpassive
5 region.
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11 It can be seen from **Table 2** that defects density values are of the order of 10^{20} - 10^{21} ,
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13 which matches the results of studies on stainless steels [64, 71, 81, 82]. In general, the
14 values of N_{A1} and N_{D1} decrease with increasing potentials, since anodic polarisation has
15 an annealing effect which eliminates some defects in the passive film [23]. Thus,
16 passive films formed at low passive potentials have more disordered structures and
17 higher defect densities than those formed at higher passive potentials. It must be
18 remarked that the density of cation vacancies present in the inner layer of the passive
19 film, N_{A1} , is always higher than the density of oxygen vacancies or cation interstitials
20 present in the outer layer of the film, N_{D1} . This result is consistent with the result
21 obtained from the PDM diagnostic criterion concerning the relationship between $\ln i_{SS}$
22 and E_f , as explained above in eq. (3). This criterion has been used to identify the
23 predominant crystallographic defect type within the passive film, which has been found
24 to be cation vacancy. However, although cation vacancies are the main defects within
25 the passive film and determine the *p*-type semiconductivity of the inner layer of the
26 passive film, Mott-Schottky analysis has revealed that the outer layer of the passive film
27 behaves as an *n*-type semiconductor, doped with oxygen vacancies and/or cation
28 interstitials. Therefore, the diagnostic criteria provided by the PDM should be used
29 along with the Mott-Schottky analysis to avoid possible ambiguities.
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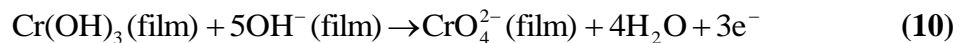
At formation potentials above 0.1 V, an increase in the number of defects in the outer layer, NV_{outers} , is observed. This increase is a consequence of the appearance of Cr^{6+} ions as deep donor species (N_{D2}) and cation vacancies, $V_{Cr}^{3'}$, as acceptor species (N_{A2}) according to eq. (2). Therefore, while the number of defects in the outer layer of the passive film decreases with film formation potential within the passive region, it increases dramatically at formation potentials within the transpassive region. The more defective structure of the film formed at potentials within the transpassive region can explain the lower resistance values obtained in the EIS experiments at high formation potentials (**Table 1**).

According to the results obtained in the Mott-Schottky analysis and to the proposed model for the electronic structure of the passive film formed on Alloy 31 (**Figure 10**), two space charge regions appear at the metal/inner layer and outer layer/electrolyte interfaces. The capacitance of these space charge regions, C_{SC} , can be obtained from the measured capacitance values using eq. (7). As it has been explained above, the capacitances of the Helmholtz layer, C_H , should not be neglected. It can be assumed that at the flat-band potential, C_H is equal to the total measured capacitance, since no depletion layer exists at this potential and the contribution of the space charge or the passive film to the total capacitance values is negligible [55, 83]. Thus, C_H values were estimated to be about 20-22 $\mu F cm^{-2}$.

The thickness of the space charge layers formed in both inner and outer regions of the passive film can be calculated from the C_{SC} values determined at the formation potential (thickness of the outer layer) and at the most negative potential (thickness of the inner layer) with the formula for a parallel plane condenser [54, 84]:

$$C_{sc} = \frac{\varepsilon \cdot \varepsilon_0}{W} \quad (9)$$

where W is the space charge layer thickness. **Table 3** gives the thickness values of the space charge layers formed on the two regions of the passive film (inner p -type layer and outer n -type layer, W_i and W_o , respectively). In the passive region, the thickness of both layers increases with increasing formation potentials. In the transpassive region, however, the thickness of the outer layer diminishes, whereas the thickness of the inner layer remains nearly constant. These results, along with the Mott-Schottky analysis, suggest that transpassive dissolution of Cr species takes place mainly in the outer layer of the passive film in contact with the electrolyte. Ben-Haim and co-workers [85] observed lower values of hydroxide content for transpassive films in comparison to primary passive films on stainless steels, which indicates that the solid state oxidation of Cr(III) to Cr(VI) in the passive films formed on stainless steels takes place through the oxidation of chromium hydroxide, according to [86, 87]:



Consequently, and according to the results obtained in the present work, it can be concluded that transpassive dissolution of Alloy 31 in the 400 g/l LiBr solution is restricted to the outer layer of the passive film, where Cr(III) species are in the form of Cr(OH)_3 .

The magnitude of the thickness of the space charge layers shown in **Table 3** are in good agreement with the thickness of passive films formed on stainless steels, which is in the range of 1-3 nm [70]. The steady-state thickness of the passive film, L_{SS} , can be

1 estimated from the sum of W_i and W_o . **Figure 11** shows the relationship between the
 2 estimated steady-state thickness of the passive film, L_{SS} , and the formation potential.
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 4 Two regions can be clearly distinguished, corresponding to the passive and transpassive
 5 regions. There is a linear dependence between L_{SS} and E in both zones, although the
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 7 slope of the straight line in Region I (passive region) is positive, whereas the slope of
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 9 the straight line in Region II (transpassive region) is negative. In the case of Region II,
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 11 the transpassive state is induced by the oxidative emission of cations from the passive
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 13 film into the interface film/electrolyte, eq. (2), and by the oxidative dissolution of the
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 15 outer layer of the passive film, eq. (10), resulting in a decrease of the film layer
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 17 thickness (mainly the outer layer of the film) as the potential increases within the
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 19 transpassive region, as other authors have observed [25, 26].
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29 The linear dependence between L_{SS} and E in the passive region (Region I) is a well
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 31 established experimental result in the anodic oxidation of metals [16, 18, 70]. The value
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 33 of the positive slope, 1.59 nm V^{-1} , is in good agreement with the $1\text{-}2.5 \text{ nm V}^{-1}$ normally
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 35 found for the passive film formation on metal and alloys [23, 26, 48, 88]. The simplified
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 37 relation between formation potential, E_f , and steady-state thickness, L_{SS} , in the PDM is
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 39 given in the following equation, for those cases where no change in the oxidation state
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 41 occurs upon ejection of a cation from the passive film and at constant pH:
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$$49 \quad L_{SS} = \frac{1-\alpha}{\varepsilon} E_f + B \quad (12)$$

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 54 where α represents the polarizability of the film/electrolyte interface and B is a constant.
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 56 From the slope of the straight line in Region I and assuming a value of $\alpha = 0.7$ [24-26],
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1 the mean electric field strength has been calculated to be $1.89 \cdot 10^6 \text{ V cm}^{-1}$, which is in
2 agreement with other studies [15, 23, 25, 26].
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7 Finally, the previous results must be discussed in terms of local breakdown of the
8 passive film and the onset of pitting corrosion. According to the PDM [16], the
9 breakdown of passivity occurs as a result of an enhanced flux of cation vacancies from
10 the film/electrolyte interface (where they are formed) to the metal/film interface (where
11 they are annihilated). This enhanced flux is envisaged to arise from the adsorption of
12 aggressive anions (such as Br^-) into oxygen vacancies at the film/electrolyte interface. If
13 the flux of cation vacancies exceeds the rate at which they are annihilated at the
14 metal/film interface, the excess vacancies condense at the interface. When the
15 condensate exceeds a critical areal concentration ($\text{mol vacancies/cm}^2$), the film is
16 detached locally from the underlying metal, its thickness decreases and film breakdown
17 occurs. In the present study, an increase in the total number of cation vacancies ($N_{A1} +$
18 N_{A2}) has been observed at formation potentials within the transpassive region.
19 Moreover, in the transpassive region the Warburg resistance has been found to decrease
20 significantly, which indicates that transport of defects within the passive film is
21 enhanced in this region, as it has been explained above. Therefore, as formation
22 potential increases within the transpassive region, the density and transport rate of
23 cation vacancies in the film increase, generating the necessary conditions for the rupture
24 of the film. In fact, the transpassive region of Alloy 31 in the 400 g/l LiBr solution
25 (**Figure 2**) is located at potentials below the pitting potential ($E_p = 0.68 \text{ V}$ [20]),
26 indicating that transpassive dissolution of Cr-containing species present in the passive
27 film is closely related to the passive film breakdown and localised corrosion
28 phenomena.
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4. CONCLUSIONS

Cation vacancies have been found to be the dominant defect in the passive films formed anodically on Alloy 31 in a 400 g/l LiBr solution at 25 °C in both passive and transpassive regions. The steady-state passive current density, i_{SS} , increases significantly at potentials located on the transpassive region.

The charge transfer resistance, R_I , increases with applied formation potential within the passive region, which is indicative of the formation of a protective passive film. The Warburg resistance, R_W , remains approximately constant in the passive range, indicating that the electric field strength is independent of the applied potential, as postulated by the PDM. At formation potentials within the transpassive region, a decrease in R_I and R_W has been observed, which is an indication of the increasing concentration of defects in the passive film and increasing conductivity.

Mott-Schottky plots for Alloy 31 in the 400 g/l LiBr solution at 25 °C and at formation potentials within the passive range reveal the existence of two regions where a Mott-Schottky type behaviour can be observed (n -type semiconductor at potentials higher than E_{FB} and p -type semiconductor at potentials lower than E_{FB}). These results can be explained considering a bilayer model of the passive film, with a n -type outer region enriched in Fe^{3+} species, such as Fe_2O_3 , $FeO(OH)$ and $Fe(OH)_3$, as well as $Cr(OH)_3$ and $CrO(OH)$, and a p -type inner region made up of an anhydrous mixed Fe-Cr oxide, most probably with a spinel structure.

1 At film formation potentials within the transpassive region, a deep donor level has been
2 observed, corresponding to the formation of Cr^{6+} ions due to transpassivity of Cr
3 species. Above 0.2 V a progressive change in the linear region slope at high potentials
4 has been observed, evidencing a change in the electronic properties of the film, from *n*-
5 type to *p*-type semiconductivity. This change has been attributed to the increase in the
6 concentration of cation vacancies in the outer layer of the passive film due to the
7 oxidative emission of cations.
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19 It has been demonstrated from Mott-Schottky analysis that cation vacancies are the
20 preponderant defects within the passive film, confirming the results obtained by the
21 PDM diagnostic criterion concerning the relationship $\ln i_{SS}$ vs E_f . These two methods
22 should be used together to complement each other and to provide complete results.
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31 The density of defects in the outer layer of the film increases and the thickness of this
32 outer layer decreases noticeably in the transpassive region, while both parameters
33 remain constant for the inner layer of the film. These observations suggest that the solid
34 state oxidation of Cr(III) to Cr(VI) takes place through the oxidation of chromium
35 hydroxide present in the outer layer of the passive film.
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47 The thickness of the passive film is found to increase linearly with formation potentials
48 within the passive region, while it decreases in the transpassive region. The decrease of
49 film thickness in the transpassive region is a consequence of the oxidative emission of
50 cations from the passive film into the film/electrolyte interface and the oxidative
51 dissolution of the outer layer of the passive film.
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Tables captions

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4 Table 1. Equivalent circuit parameters obtained by fitting the experimental results of EIS, for Alloy 31 in
5 the 400 g/l LiBr solution at 25 °C, at different film formation potentials within the passive and
6 transpassive regions.
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12 Table 2. Acceptor and donor densities for Alloy 31 in the 400 g/l LiBr solution at 25 °C, at different film
13 formation potentials within the passive and transpassive regions.
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18 Table 3. Thicknesses of the inner (W_i) and outer (W_o) space charge layers for Alloy 31 in the 400 g/l LiBr
19 solution at 25 °C, at different film formation potentials within the passive and transpassive regions.
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Figures captions

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28 Fig. 1. Current density transients for Alloy 31 in the 400 g/l LiBr solution at 25 °C recorded after stepping
29 the potential from the cathodic cleaning value (-1 V) to several film formation potential (-0.3, -0.1 and 0.1
30 V within the passive region, and 0.4 V within the transpassive region).
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36 Fig. 2. Potentiodynamic polarisation curve of Alloy 31 in the 400 g/l LiBr solution at 25° C. The insert
37 shows the passive and transpassive regions with detail.
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43 formation potential for Alloy 31 in the 400 g/l LiBr solution at 25 °C.
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48 Fig. 4. Nyquist and Bode-phase plots for Alloy 31 in the 400 g/l LiBr solution at 25 °C, at several film
49 formation potentials (-0.3, -0.1 and 0.1 V within the passive region, and 0.4 V within the transpassive
50 region).
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56 Fig. 5. Kramers–Kronig transforms of EIS data for Alloy 31 in the 400 g/l LiBr solution at 25 °C and at
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2 Fig. 6. Representation of the equivalent circuit proposed for the interpretation of EIS spectra of Alloy 31
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4 in the 400 g/l LiBr solution at 25 °C.
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10 solution at 25 °C, scanning the potential from the film formation value of -0.1 V in the negative direction.
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14 Fig. 8. Capacitance-potential curve obtained at 5 kHz for Alloy 31 in the 400 g/l LiBr solution at 25 °C
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16 scanning the potential from the film formation values of -0.1 V (passive region) and 0.4 V (transpassive
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18 region), in the negative direction.
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22 Fig. 9. Mott-Schottky plots for Alloy 31 in the 400 g/l LiBr solution at 25 °C obtained at 5 kHz at
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24 different film formation potentials within the passive and transpassive regions.
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26 Fig. 10. Schematic representation of the electronic energy band for the passive film formed on Alloy 31 in
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28 the 400 g/l LiBr solution at 25 °C, at formation potentials within the passive region.
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32 Fig. 11. Estimated values of the steady-state thickness of the passive film formed on Alloy 31 surface
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34 (L_{SS}) as a function of the film formation potential, in the 400 g/l LiBr solution at 25 °C.
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Table 1

	E vs (Ag/AgCl)/V	$R_s/\Omega \text{ cm}^2$	$R_l/\text{k}\Omega \text{ cm}^2$	$C_l/\mu\text{F cm}^{-2}$	n_l	$R_w/\text{k}\Omega \text{ cm}^2$	$\chi^2 (\times 10^{-3})$
Passive region	-0.30	1.03 ± 0.05	$(1.2 \pm 0.4) \cdot 10^2$	9.1 ± 1.0	0.93 ± 0.01	$(1.3 \pm 0.2) \cdot 10^3$	6.97
	-0.25	1.06 ± 0.05	$(2.2 \pm 0.8) \cdot 10^2$	7.7 ± 0.9	0.93 ± 0.01	$(1.61 \pm 0.08) \cdot 10^3$	8.43
	-0.20	1.03 ± 0.06	$(4.5 \pm 1.0) \cdot 10^2$	8.0 ± 1.9	0.94 ± 0.01	$(1.5 \pm 0.2) \cdot 10^3$	7.96
	-0.15	1.12 ± 0.05	$(5.2 \pm 1.4) \cdot 10^2$	7.7 ± 2.0	0.93 ± 0.01	$(1.6 \pm 0.3) \cdot 10^3$	5.60
	-0.10	1.02 ± 0.01	$(8.2 \pm 1.3) \cdot 10^2$	7.0 ± 0.1	0.93 ± 0.01	$(1.14 \pm 0.07) \cdot 10^3$	6.44
	-0.05	1.09 ± 0.06	$(8.5 \pm 0.3) \cdot 10^2$	7.8 ± 0.3	0.94 ± 0.01	$(1.5 \pm 0.2) \cdot 10^3$	7.34
	0	1.04 ± 0.04	$(9.0 \pm 1.1) \cdot 10^2$	7.8 ± 0.2	0.94 ± 0.01	$(1.3 \pm 0.2) \cdot 10^3$	7.54
	0.05	1.09 ± 0.11	$(9.1 \pm 1.2) \cdot 10^2$	7.6 ± 0.1	0.93 ± 0.01	$(1.4 \pm 0.2) \cdot 10^3$	5.02
	0.10	1.06 ± 0.07	$(7.9 \pm 0.8) \cdot 10^2$	7.5 ± 0.4	0.93 ± 0.01	$(0.87 \pm 0.09) \cdot 10^3$	8.96
Transpassive region	0.15	1.05 ± 0.11	$(6.0 \pm 1.0) \cdot 10^2$	6.5 ± 2.3	0.90 ± 0.02	$(1.0 \pm 0.2) \cdot 10^3$	5.00
	0.20	1.13 ± 0.06	$(5.6 \pm 0.5) \cdot 10^2$	8.5 ± 1.1	0.91 ± 0.01	$(0.39 \pm 0.07) \cdot 10^3$	7.37
	0.25	1.18 ± 0.05	$(4.9 \pm 0.7) \cdot 10^2$	7.5 ± 0.6	0.88 ± 0.02	$(0.42 \pm 0.09) \cdot 10^3$	3.95
	0.30	1.02 ± 0.08	$(4.2 \pm 0.7) \cdot 10^2$	8.0 ± 2.1	0.88 ± 0.01	$(0.37 \pm 0.07) \cdot 10^3$	3.28
	0.35	0.96 ± 0.03	$(3.8 \pm 0.5) \cdot 10^2$	8.2 ± 0.9	0.87 ± 0.02	$(0.26 \pm 0.09) \cdot 10^3$	3.24
	0.40	1.07 ± 0.05	$(3.5 \pm 0.9) \cdot 10^2$	12.5 ± 0.8	0.90 ± 0.01	$(0.22 \pm 0.05) \cdot 10^3$	6.35

Table 2

E vs (Ag/AgCl)/mV	$N_{AI} / 10^{20} \text{ cm}^{-3}$	$N_{DI} / 10^{20} \text{ cm}^{-3}$	$N_{A2} / 10^{20} \text{ cm}^{-3}$	$N_{D2} / 10^{20} \text{ cm}^{-3}$	$NV_{outer} / 10^{20} \text{ cm}^{-3}$
-0.30	43 ± 8	4.0 ± 0.1	---	---	4.0 ± 0.1
-0.25	22 ± 5	3.9 ± 0.3	---	---	3.9 ± 0.3
-0.20	17 ± 3	3.9 ± 0.2	---	---	3.9 ± 0.2
-0.15	17 ± 6	3.8 ± 0.3	---	---	3.8 ± 0.3
-0.10	10 ± 1	3.8 ± 0.2	---	---	3.8 ± 0.2
-0.05	10 ± 1	3.8 ± 0.1	---	---	3.80 ± 0.1
0.00	7 ± 2	3.8 ± 0.5	---	---	3.80 ± 0.5
0.05	8 ± 1	4.0 ± 0.4	---	---	4.0 ± 0.4
0.10	8.2 ± 0.5	3.8 ± 0.4	---	10 ± 1	14 ± 1
0.15	5.8 ± 0.1	3.3 ± 0.2	---	11 ± 2	15 ± 2
0.20	8.2 ± 0.5	3.9 ± 0.3	---	26 ± 4	29 ± 4
0.25	5.3 ± 0.4	2.9 ± 0.3	---	39 ± 6	42 ± 6
0.30	5.7 ± 0.4	3.0 ± 0.3	39 ± 11	---	42 ± 11
0.35	5.4 ± 0.3	2.9 ± 0.2	26 ± 8	---	29 ± 8
0.40	7.2 ± 0.2	3.1 ± 0.1	13 ± 3	---	16 ± 3

Table 3

	E vs (Ag/AgCl)/mV	W_i / nm	W_o / nm
Passive region	-0.30	---	0.74 ± 0.03
	-0.25	0.12 ± 0.05	0.82 ± 0.03
	-0.20	0.13 ± 0.04	0.84 ± 0.04
	-0.15	0.20 ± 0.07	0.87 ± 0.01
	-0.10	0.23 ± 0.06	0.88 ± 0.02
	-0.05	0.28 ± 0.05	0.91 ± 0.03
	0.00	0.34 ± 0.05	0.92 ± 0.04
	0.05	0.52 ± 0.01	0.95 ± 0.01
	0.10	0.39 ± 0.03	0.97 ± 0.02
Transpassive region	0.15	0.46 ± 0.07	0.94 ± 0.12
	0.20	0.45 ± 0.04	0.82 ± 0.09
	0.25	0.36 ± 0.02	0.76 ± 0.10
	0.30	0.41 ± 0.07	0.64 ± 0.03
	0.35	0.45 ± 0.03	0.61 ± 0.03
	0.40	0.46 ± 0.04	0.37 ± 0.02

Figure 1

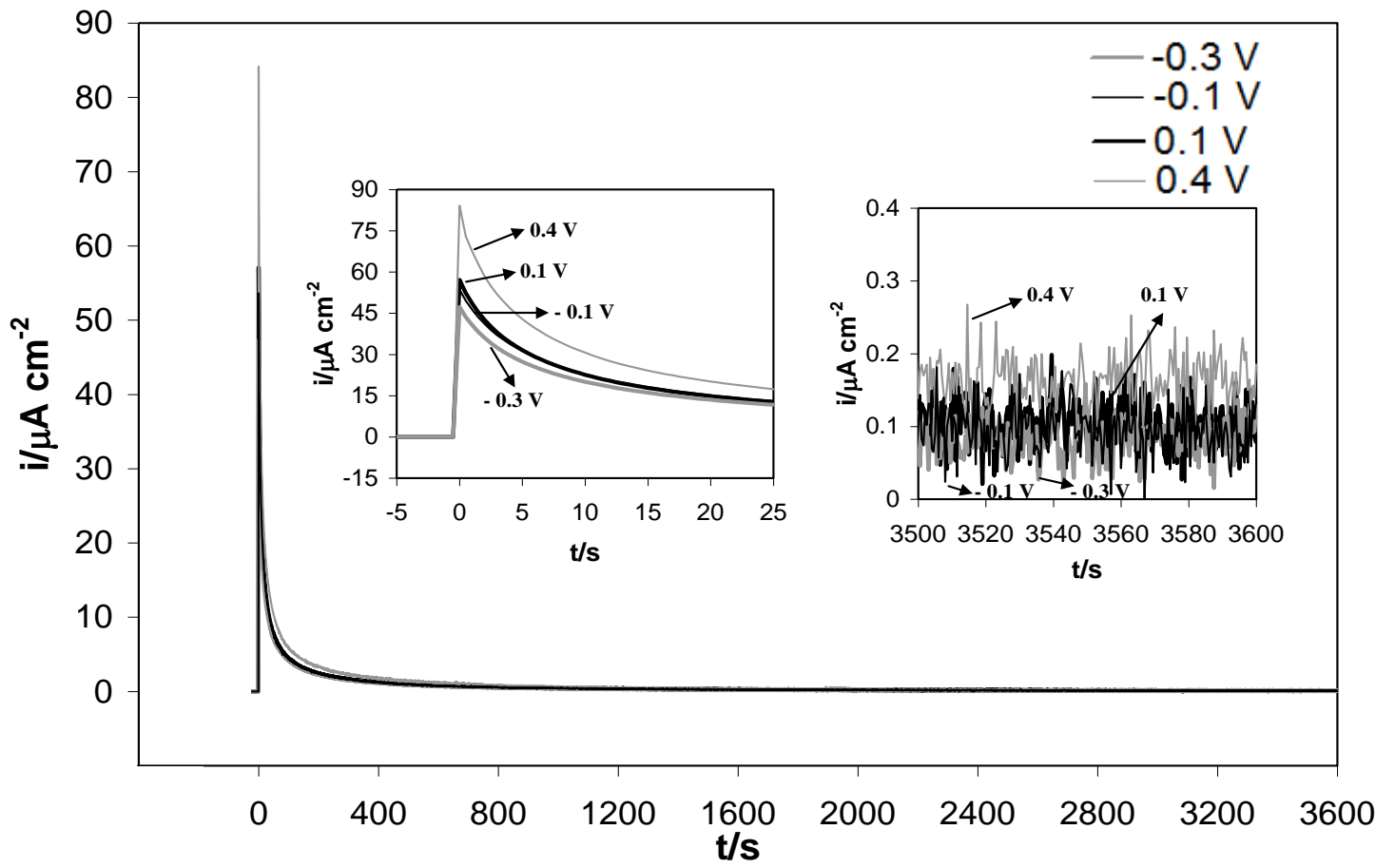


Figure 2

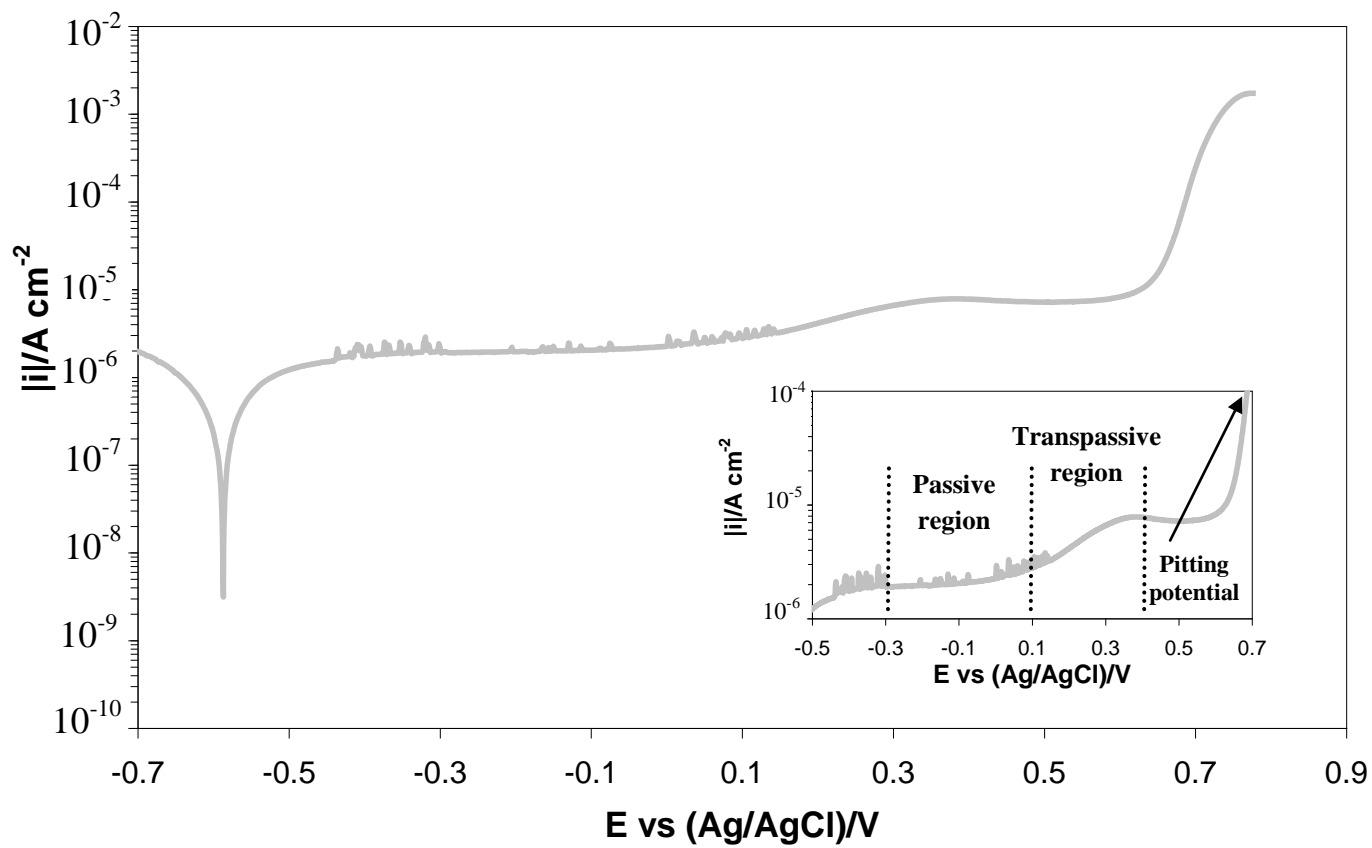


Figure 3

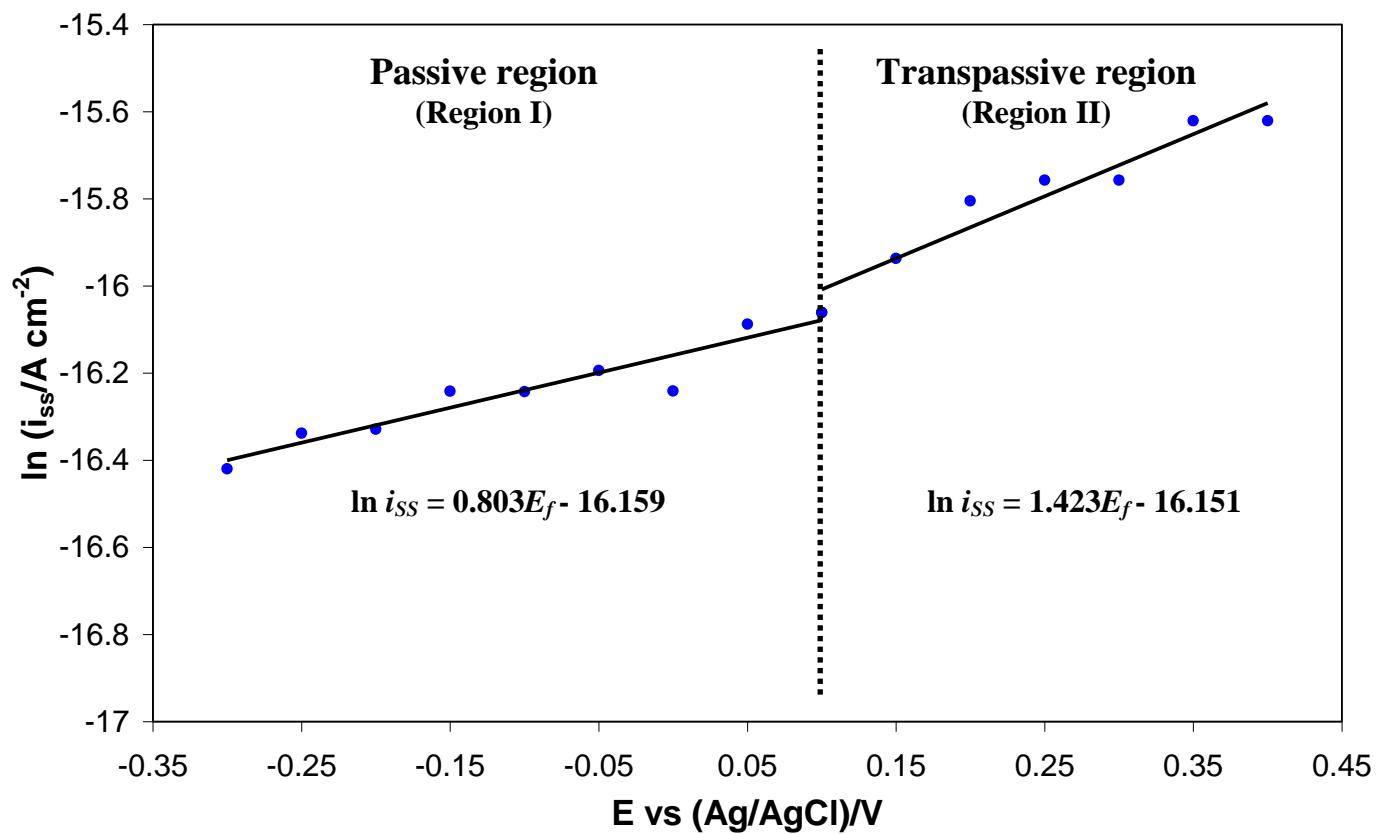
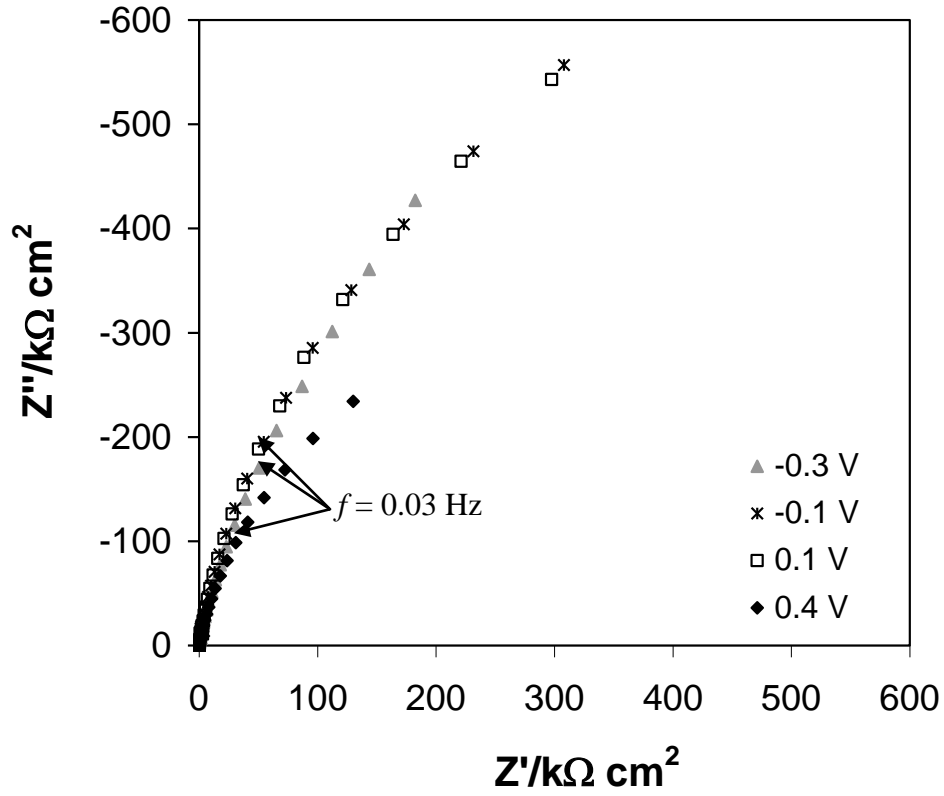
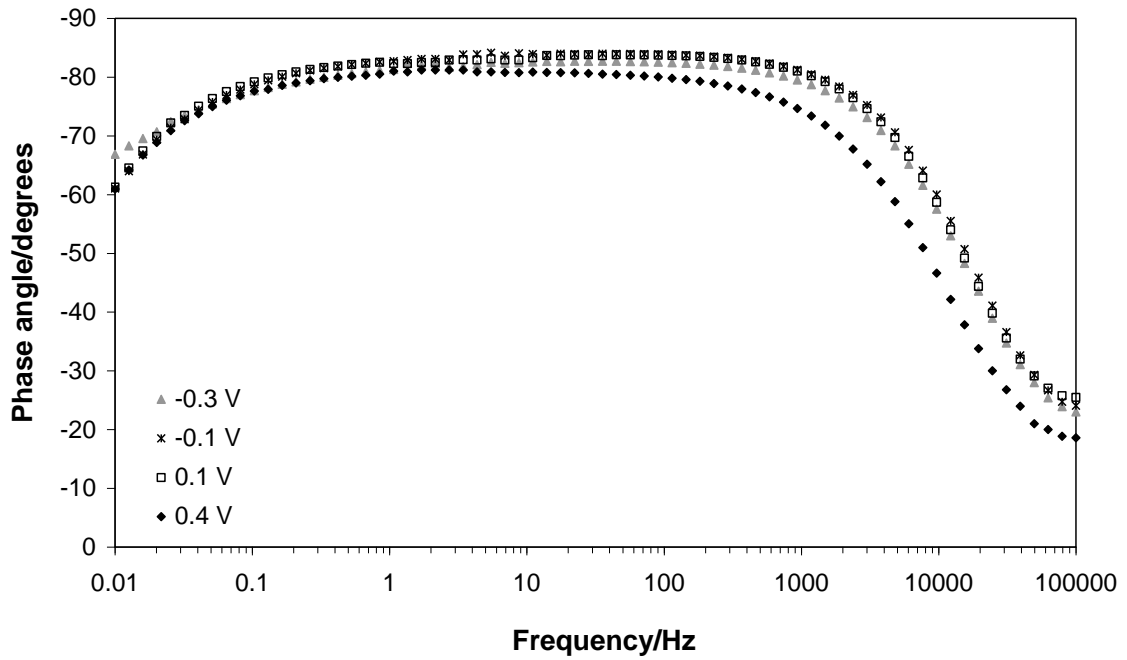


Figure 4



(a)



(b)

Figure 5

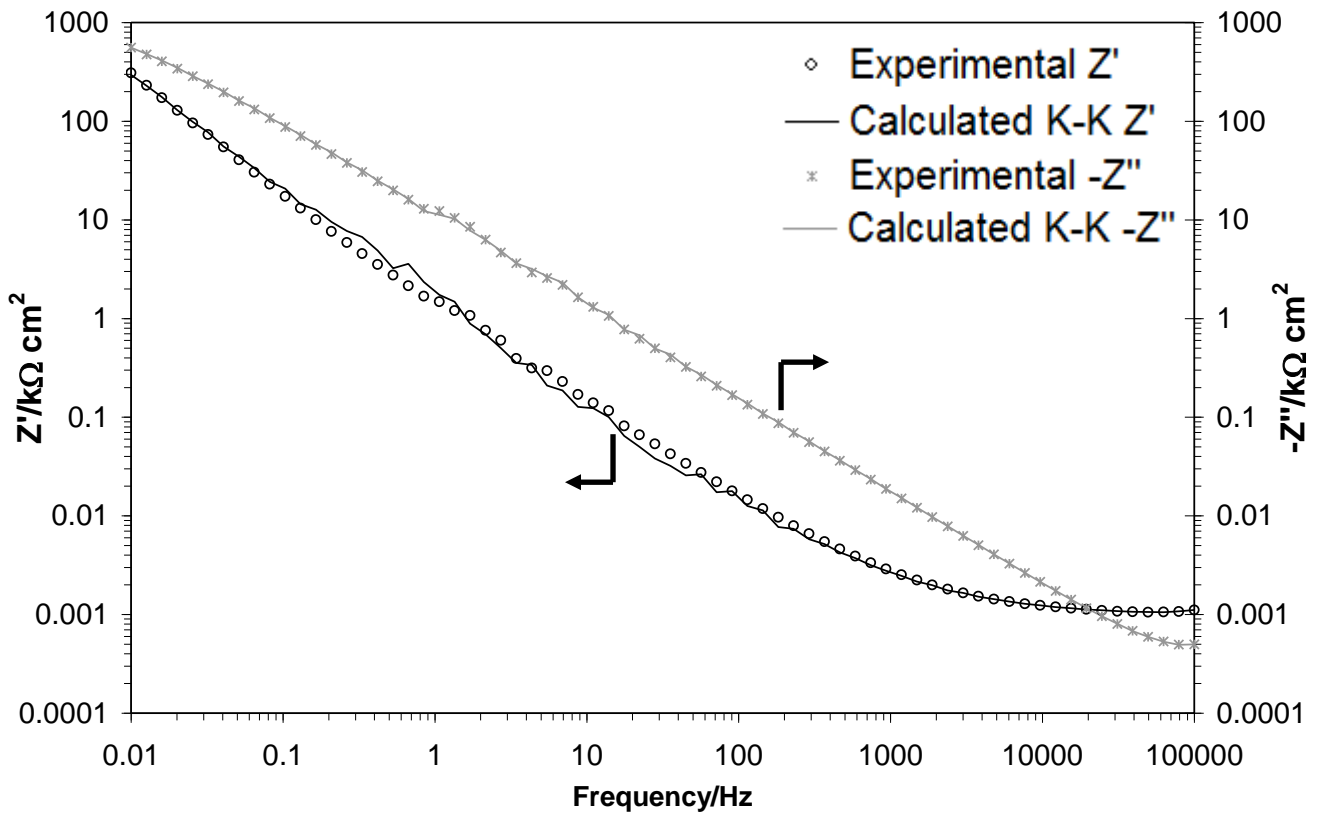


Figure 6

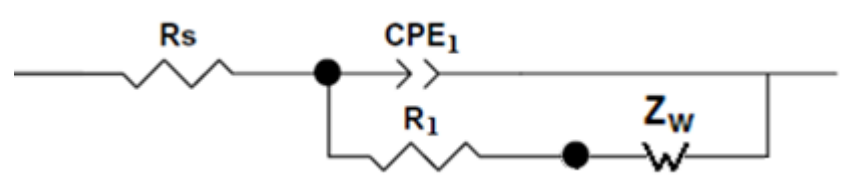


Figure 7

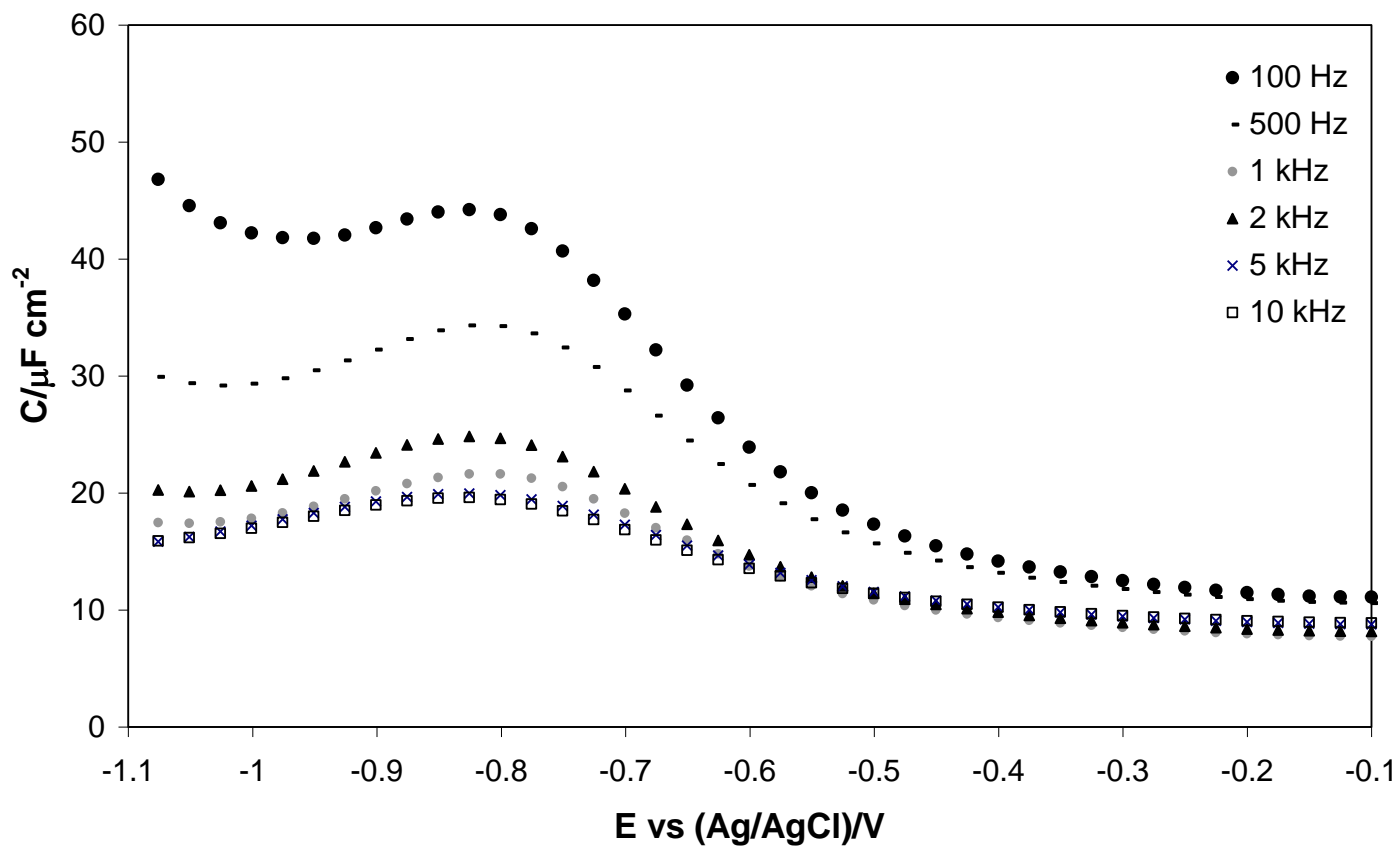


Figure 8

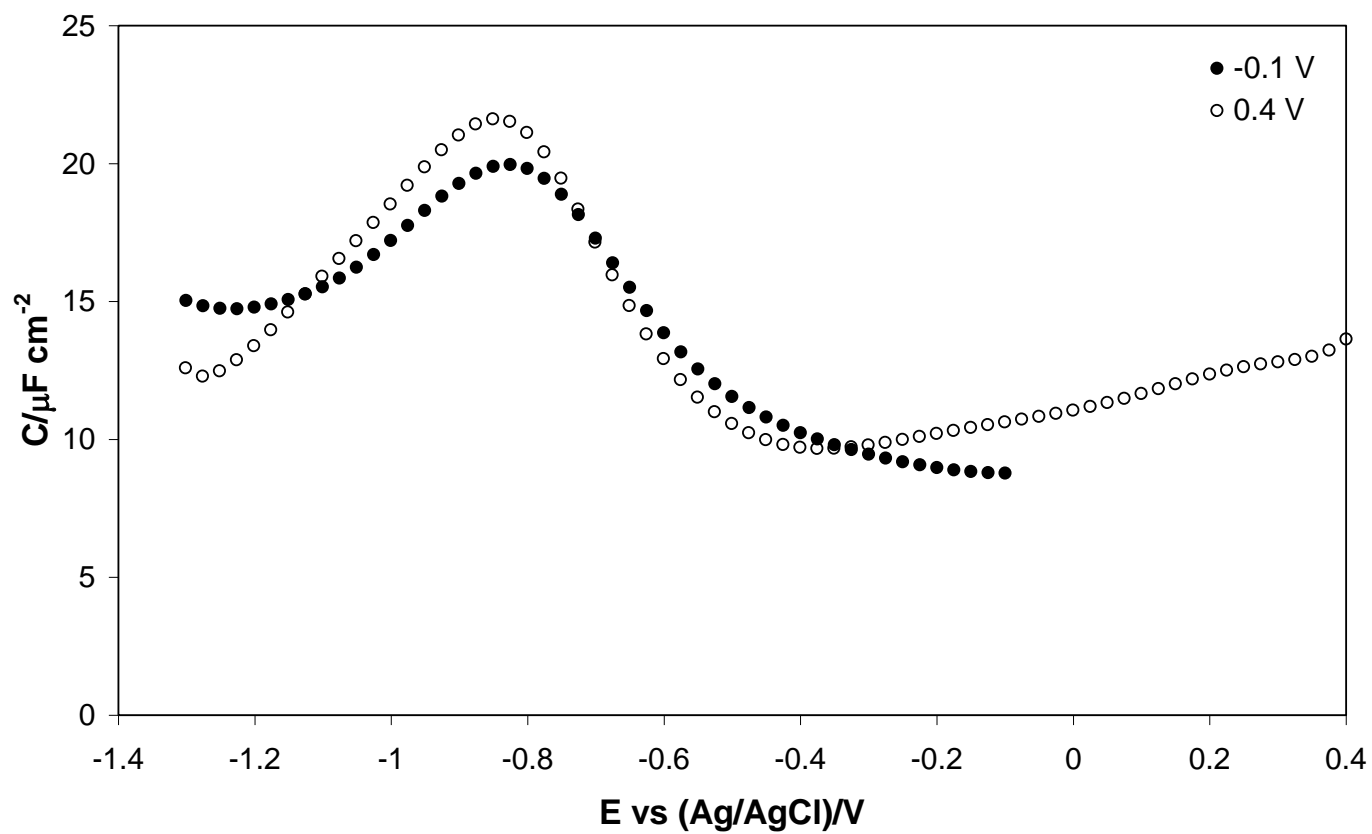


Figure 9

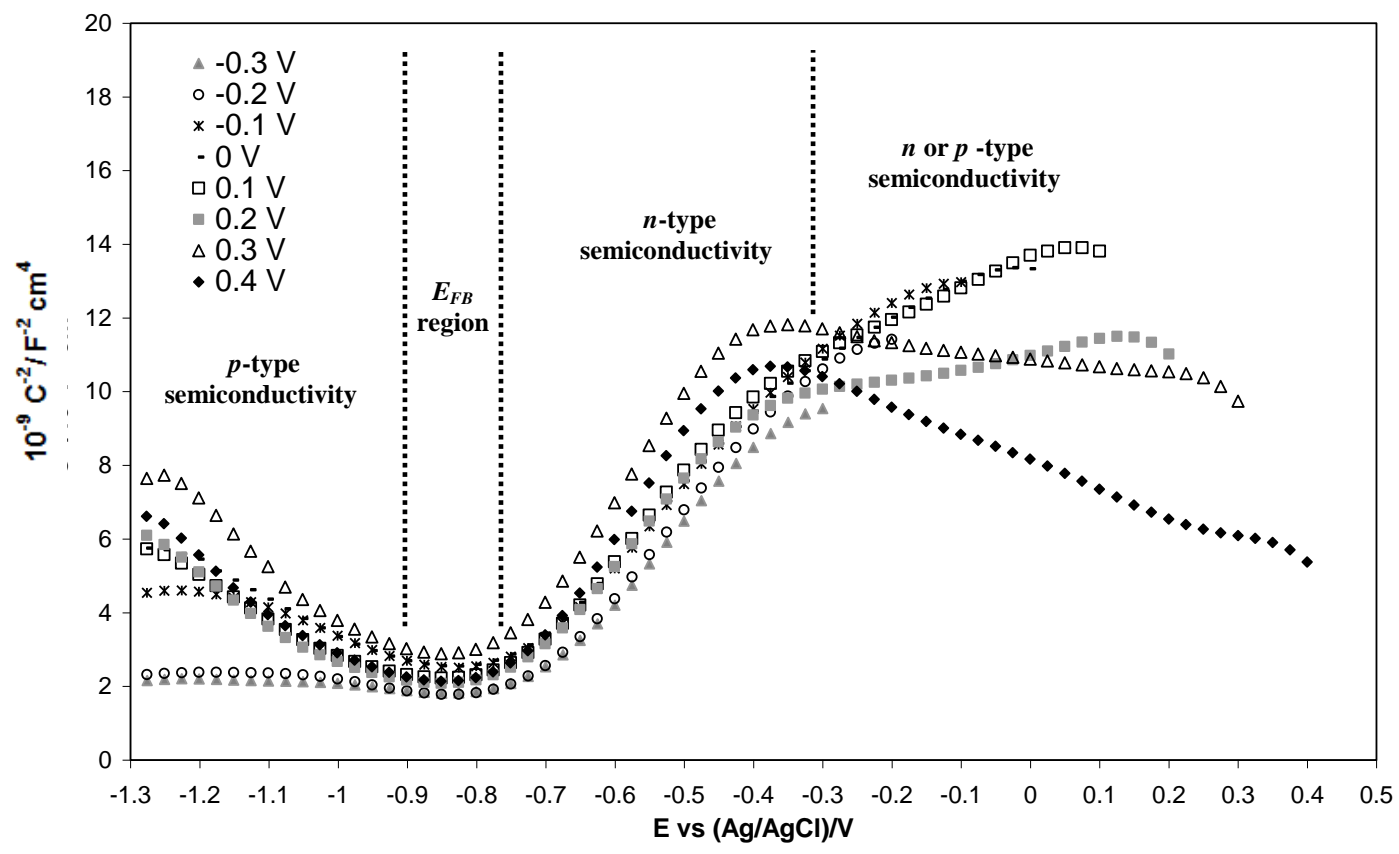


Figure 10

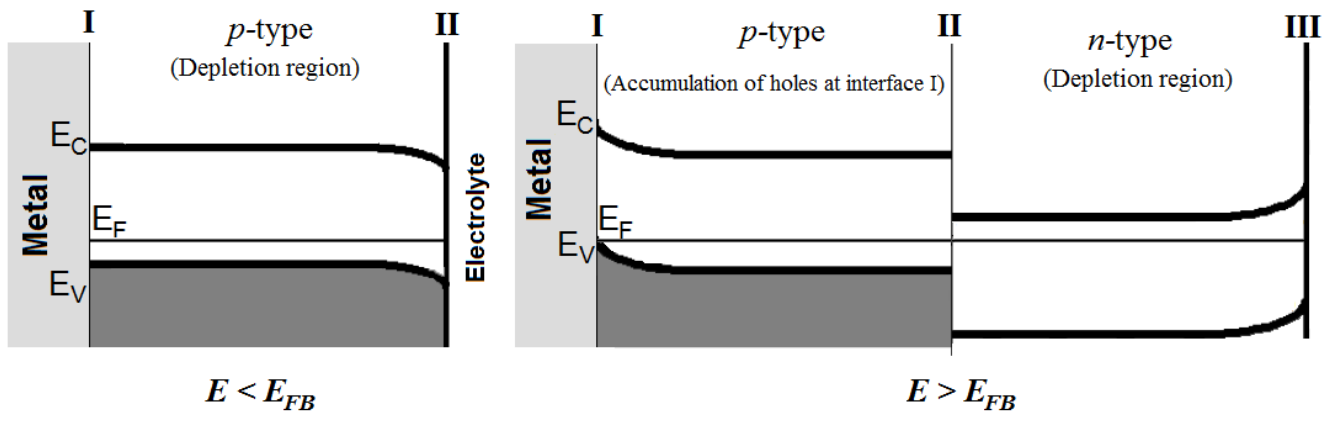


Figure 11

