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Gomis, O.; Ortiz, HM.; Sans Tresserras, JÁ.; Manjón Herrera, FJ.; Santamaría-Pérez, D.; Rodríguez-Hernández, P.; Muñoz, A. (2016). InBO3 and ScBO3 at high pressures: an ab initio study of elastic and thermodynamic properties. *Journal of Physics and Chemistry of Solids*. 98:198-208. doi:10.1016/j.jpcs.2016.07.002.



The final publication is available at

<http://dx.doi.org/10.1016/j.jpcs.2016.07.002>

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Additional Information

1 **InBO₃ and ScBO₃ at high pressures: an *ab initio* study**
2 **of elastic and thermodynamic properties**

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Abstract

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We have theoretically investigated the elastic properties of calcite-type orthoborates ABO_3 ($A = \text{Sc}$ and In) at high pressure by means of *ab initio* total-energy calculations. From the elastic stiffness coefficients, we have obtained the elastic moduli (B , G and E), Poisson's ratio (ν), B/G ratio, universal elastic anisotropy index (A_U), Vickers hardness, and sound wave velocities for both orthoborates. Our simulations show that both borates are more resistive to volume compression than to shear deformation ($B > G$). Both compounds are ductile and become more ductile, with an increasing elastic anisotropy, as pressure increases. We have also calculated some thermodynamic properties, like Debye temperature and minimum thermal conductivity. Finally, we have evaluated the theoretical mechanical stability of both borates at high hydrostatic pressures. It has been found that the calcite-type structure of InBO_3 and ScBO_3 becomes mechanically unstable at pressures beyond 56.2 and 57.7 GPa, respectively.

Keywords:

A. oxides

A. semiconductors

C. *ab initio* calculations

C. high pressure

D. mechanical properties

59 1. Introduction

60 Scandium [1] and indium [2] orthoborates crystallize in the calcite-type structure
61 (space group: $R\bar{3}c$, No. 167, $Z=6$) where Sc (or In) atoms and B atoms are coordinated
62 by 6 and 3 O atoms, respectively (see **Fig. 1**). Orthoborates have a wide potential at
63 room conditions for luminescent applications. Noteworthy, rare-earth-doped ABO_3
64 emitting phosphors are known for fifty years [3]. In particular, $ScBO_3$ and $InBO_3$ doped
65 with rare-earth ions and transition metals have been studied due to their properties as
66 phosphor or scintillating materials [4-9]. Furthermore, $ScBO_3$ operates as a room-
67 temperature near-infrared tunable laser when doped with Cr^{3+} [10], and recently it has
68 been found to operate as a Q-switched laser when doped with Yb^{3+} [11]. On the other
69 hand, $InBO_3$ was postulated as a candidate for neutrino detection [12] and has been
70 confirmed in the last years as a promising photocatalyst for future applications in
71 treatment of environment contaminants [13-15]. Besides, Eu-doped $InBO_3$ has been
72 recently found to be a good candidate for highly efficient solar cells [16].

73 Despite the important technological applications of $InBO_3$ and $ScBO_3$, many
74 properties of these borates are unknown. Apart from the well known structure of calcite-
75 type orthoborates, their exceptional luminescence properties, and their mechanical,
76 thermal, radiation-resistant and chemical stability, not many other properties are known.
77 Raman scattering characterization have been reported for $ScBO_3$ and $InBO_3$ [17, 18]
78 and the refractive index of $InBO_3$ has been just recently measured [19]. Besides, the
79 experimental thermal and spectral properties along with the Vickers hardness of
80 $Yb^{3+}:ScBO_3$ have been recently reported [20].

81 The elastic properties of orthoborates are poorly known and, to the best of our
82 knowledge, only the axial compressibilities and the bulk modulus at zero pressure (B_0)
83 are known for $ScBO_3$ and $InBO_3$ from a recent experimental and theoretical work [21]

84 along with the experimental Vickers hardness for $\text{Yb}^{3+}:\text{ScBO}_3$ as stated above [20].
85 Moreover, while the elastic stiffness coefficients for some calcite-type carbonates have
86 been studied at 1 atm and at high pressures [22-27], no information is available for any
87 calcite-type orthoborate.

88 In this work, we report a theoretical study of the elastic and thermodynamic
89 properties at 0 GPa and at high pressure (HP) of scandium and indium orthoborates with
90 rhombohedral calcite-type structure. The knowledge of the elastic behaviour of the two
91 borates under pressure allows us to discuss the mechanical stability of these calcite-type
92 compounds at high pressures. Elastic and thermodynamic data reported for the two
93 orthoborates can be highly interesting for the comparison with those of calcite-type
94 carbonates in order to understand better the elastic and thermodynamic properties of
95 compounds crystallizing in the important calcite-type structure both at zero and high
96 pressures.

97

98 **2. Theoretical calculation details**

99 We have performed *ab initio* total-energy calculations within the density
100 functional theory (DFT) [28] using the plane-wave pseudopotential method with the
101 Vienna *Ab initio* Simulation Package (VASP) [29]. The projector-augmented wave
102 scheme (PAW) [30] was used as implemented in this package to take into account the
103 full nodal character of the all-electron charge density in the core region. In order to
104 achieve highly converged results and an accurate description of the electronic
105 properties, plane waves up to an energy cutoff of 520 eV were used in the basis set. The
106 exchange-correlation energy was described with the generalized gradient approximation
107 (GGA) with the PBEsol prescription [31]. A dense Monkhorst–Pack grid (6 x 6 x 6) of
108 special k-points was used to perform integrations along the Brillouin zone (BZ) to

109 obtain very well-converged energies and forces. The cutoff energy and the k-point
110 sampling employed ensure a high convergence of 1 meV per formula unit in the total
111 energy as well as an accurate calculation of the forces on the atoms. At each selected
112 volume, the structures were fully relaxed to their optimized configuration through the
113 calculation of the forces on atoms and the stress tensor. With this procedure we obtain a
114 set of energies, volumes, pressures, and the related structural parameters. In the relaxed
115 optimized configurations, the forces on the atoms are less than 0.006 eV/Å, and
116 deviations of the stress tensor from a diagonal hydrostatic form are less than 1 kbar (0.1
117 GPa). The application of DFT-based total-energy calculations to the study of
118 semiconductor properties under HP has been reviewed in **Ref. [32]**, showing that the
119 phase stability, electronic, and dynamical properties of compounds under pressure are
120 well described by DFT.

121 In order to study the mechanical properties of calcite-type borates by means of
122 *ab initio* calculations we have calculated the elastic constants, which describe the
123 mechanical properties of a material in the region of small deformations; i.e., where the
124 stress-strain relations are still linear. The elastic constants can be obtained by computing
125 the macroscopic stress for a small strain with the use of the stress theorem [33].
126 Alternatively, they can be also calculated using density functional perturbation theory
127 (DFPT) [34]. In this work, we have evaluated the elastic constants of the calcite-type
128 borates with the use of method implemented in the VASP code: the ground state and
129 fully relaxed structures were strained in different directions taking into account their
130 symmetry [35]. Total-energy variations were evaluated according to a Taylor expansion
131 for the total energy with respect to the applied strain [36]. Due to this fact, it is
132 important to check that the strain used in the calculations guarantees the harmonic
133 behavior. This procedure allows the computation of the C_{ij} elastic constants.

134

135 **3. Results and discussion**

136 **3.1. Elastic properties**

137 The calcite-type structure belongs to the rhombohedral (trigonal) Laue group RI.
138 This Laue group contains all crystals with $3m$, 32 , and $-3m$ point groups. In this Laue
139 group, there are 6 independent second-order elastic constants [37] which, in the Voigt
140 notation, are C_{11} , C_{12} , C_{13} , C_{14} , C_{33} and C_{44} [38-41]. Note that $C_{66} = (C_{11}-C_{12})/2$ is not an
141 independent elastic constant [37]. When a non-zero uniform stress is applied to the
142 crystal, the elastic properties are described by the elastic stiffness, or stress-strain,
143 coefficients, which are defined as

144

$$145 \quad B_{ijkl} = C_{ijkl} + 1/2 [\delta_{ik} \sigma_{jl} + \delta_{jk} \sigma_{il} + \delta_{il} \sigma_{jk} + \delta_{jl} \sigma_{ik} - 2 \delta_{kl} \sigma_{ij}], \quad (1)$$

146

147 with C_{ijkl} being the elastic constants evaluated at the current stressed state, σ_{ij}
148 correspond to the external stresses, and δ_{kl} is the Kronecker delta [42-44]. In the special
149 case of hydrostatic pressure ($\sigma_{11} = \sigma_{22} = \sigma_{33} = -P$) applied to a rhombohedral crystal, the
150 elastic stiffness coefficients in the Voigt notation B_{ij} are: $B_{11} = C_{11} - P$, $B_{12} = C_{12} + P$,
151 $B_{13} = C_{13} + P$, $B_{14} = C_{14}$, $B_{33} = C_{33} - P$, $B_{44} = C_{44} - P$, and $B_{66} = C_{66} - P$, where P is the
152 hydrostatic pressure. Note that the B_{ij} and C_{ij} are equal at 0 GPa. When the elastic
153 stiffness coefficients B_{ij} are used, all relationships of the elasticity theory can be applied
154 for the crystal under any loading, including Born's stability conditions which are
155 identical in both loaded and unloaded states [43-47].

156

157 **Table 1** shows the set of C_{ij} elastic constants at zero pressure obtained from our
158 calculations for both ScBO_3 and InBO_3 . To our knowledge, there are no reported
experimental C_{ij} data in these borates to compare with. In particular, C_{11} and C_{33} exhibit

159 the largest values, followed by C_{12} and C_{13} which are similar and smaller than the
160 former, and finally C_{14} is the smallest one. It can be commented that, in general, values
161 for C_{ij} at zero pressure are similar in the two compounds. However, there is a decrease
162 of the value of C_{33} and C_{14} on going from ScBO_3 to InBO_3 , and the contrary occurs with
163 C_{12} . The same comments apply for the case of the B_{ij} elastic stiffness coefficients in
164 both compounds as $C_{ij} = B_{ij}$ at 0 GPa. It can be commented that the C_{33}/C_{11} ratio results
165 0.61 (0.58) for ScBO_3 (InBO_3) at 0 GPa. This ratio describes the longitudinal elastic
166 anisotropy for the single crystal [48] and tell us that the stiffness of ScBO_3 (InBO_3)
167 along the c -axis is 39% (42%) smaller than perpendicular to it. This result is in
168 agreement with chemical arguments since short B-O bonds located at the ab plane
169 perpendicular to the c -axis are less compressible than the long Sc-O and In-O bonds
170 (see **Fig. 1**) [21]. We have also obtained the axial compressibilities κ_a and κ_c from the
171 elastic constants. The used formulas are [49]:

172

$$173 \quad \kappa_a = \frac{C_{33} - C_{13}}{C_{33}(C_{11} + C_{12}) - 2C_{13}^2} \quad (2)$$

174

$$175 \quad \kappa_c = \frac{C_{11} + C_{12} - 2C_{13}}{C_{33}(C_{11} + C_{12}) - 2C_{13}^2} \quad (3)$$

176

177 **Table 2** includes the values for κ_a and κ_c , obtained at 0 GPa using **Eqs. 2** and **3**, which
178 are in good agreement with those reported in **Ref [21]** obtained from equation of state
179 fits which are also included in **Table 2** for comparison. This result gives us confidence
180 about the correctness of our elastic constants calculations. Another quantity to measure
181 the degree of elastic anisotropy of a rhombohedral single crystal is the ratio between the
182 axial compressibilities, κ_c/κ_a [50]. The κ_c/κ_a ratio is 2.67 (3.15) for ScBO_3 (InBO_3) at 0
183 GPa. This result shows that κ_c is greater than κ_a because the c -axis is more compressible

184 than the a -axis. This is in agreement with the C_{33}/C_{11} ratio smaller than 1 and the fact
 185 that the B-O bonds located at the ab plane are less compressible than the Sc-O and In-O
 186 bonds as stated above.

187 **Figures 2 and 3** show the pressure dependence of the elastic constants, C_{ij} , and
 188 elastic stiffness coefficients, B_{ij} , in ScBO₃ and InBO₃ up to 70 and 69 GPa, respectively.
 189 Despite only B_{ij} are meaningful at any pressure, we report also the pressure dependence
 190 of C_{ij} because they are the original magnitudes computed from which B_{ij} are obtained.
 191 **Table 1** summarizes the linear and quadratic pressure coefficients of C_{ij} for both
 192 compounds. In both borates, all C_{ij} show a positive linear pressure coefficient, whereas
 193 all B_{ij} except B_{66} exhibit a positive linear pressure coefficient. On the other hand, B_{44}
 194 increases up to 7.5 (11.5) GPa in ScBO₃ (InBO₃) and decreases at larger pressures. It is
 195 noteworthy that the linear pressure coefficient of all elastic constants and elastic
 196 stiffness coefficients is greater in InBO₃ than in ScBO₃ except for C_{33} and B_{33} . On the
 197 other hand, the quadratic pressure coefficient is negative in all C_{ij} and B_{ij} for both
 198 borates.

199 With the set of B_{ij} for calcite-type borates, standard analytical formulas for the
 200 bulk (B) and shear (G) moduli in the Voigt [38], Reuss [51], and Hill [52]
 201 approximations, labeled with subscripts V , R , and H , respectively, can be then applied
 202 under any loading [53]:

$$203 \quad B_V = \frac{2B_{11} + 2B_{12} + B_{33} + 4B_{13}}{9} \quad (4)$$

$$204 \quad G_V = \frac{M + 12B_{44} + 12B_{66}}{30} \quad (5)$$

$$205 \quad B_R = \frac{c^2}{M} \quad (6)$$

206

207 with

208
$$M = B_{11} + B_{12} + 2B_{33} - 4B_{13} \quad (7)$$

209 and

210
$$c^2 = (B_{11} + B_{12})B_{33} - 2B_{13}^2 \quad (8)$$

211

212
$$G_R = \frac{5}{2} \frac{c^2(B_{44}B_{66} - B_{14}^2)}{3B_V(B_{44}B_{66} - B_{14}^2) + c^2(B_{44} + B_{66})} \quad (9)$$

213
$$B_H = \frac{B_V + B_R}{2} \quad (10)$$

214
$$G_H = \frac{G_V + G_R}{2} \quad (11)$$

215 In the Voigt (Reuss) approximation, uniform strain (stress) is assumed
 216 throughout the polycrystal [38,51]. Hill has shown that the Voigt and Reuss averages
 217 are limits and suggested that the actual effective B and G elastic moduli can be
 218 approximated by the arithmetic mean of the two bounds [52]. The Young (E) modulus
 219 and the Poisson's ratio (ν) are calculated with the expressions [54,55]:

220
$$E_X = \frac{9B_X G_X}{G_X + 3B_X} \quad (12)$$

221
$$\nu_X = \frac{1}{2} \left(\frac{3B_X - 2G_X}{3B_X + G_X} \right) \quad (13)$$

222

223 where the subscript X refers to the symbols V , R , and H .

224 Elastic moduli at 0 GPa for the two calcite-type orthoborates are summarized in
 225 **Table 3**. It is found that the bulk, shear and Young moduli at 0 GPa are larger in ScBO₃
 226 than in InBO₃; therefore, the stiffness of ScBO₃ is greater than that of InBO₃. In fact, the
 227 value of the Hill bulk modulus, $B_H = 171.9$ GPa (166.5 GPa) in ScBO₃ (InBO₃), is in
 228 good agreement with experimental values of $B_0 = 166(4)$ GPa (158(3) GPa) in ScBO₃
 229 (InBO₃), and theoretical values of $B_0 = 167.7(6)$ GPa (160.3(5) GPa) in ScBO₃ (InBO₃),
 230 previously reported, which were obtained from fits of experimental and theoretical data

231 to a Birch-Murnaghan equation of state [21]. This agreement is again a check of the
232 goodness of our calculations of the elastic constants. Furthermore, it can be observed
233 that the two calcite-type borates are more resistive to volume compression than to shear
234 deformation ($B > G$) at any pressure.

235 **Table 3** also includes the values of the Poisson's ratio (ν), the ratio between the
236 bulk and shear modulus, B/G , and the universal elastic anisotropy index A_U at 0 GPa.
237 The Poisson's ratio provides information about the characteristics of the bonding forces
238 and chemical bonding. The value of the Poisson's ratio in the Hill approximation is
239 similar in both borates: $\nu = 0.30$ (0.31) in ScBO_3 (InBO_3). This value indicates that the
240 interatomic bonding forces are predominantly central ($\nu > 0.25$) and that ionic bonding
241 is predominant against covalent bonding at 0 GPa [56, 57].

242 The B/G ratio is a simple relationship given by Pugh [58], empirically linking
243 the plastic properties of a material with its elastic moduli. According to the Pugh
244 criterion, a high B/G ratio is associated with ductility, whereas a low ratio corresponds
245 to brittleness. The critical value for the B/G ratio is around 1.75, which separates ductile
246 and brittle materials. In our study, we have found values of B/G at 0 GPa above 1.75 for
247 InBO_3 and ScBO_3 . Therefore, both compounds are ductile at zero pressure, being InBO_3
248 more ductile than ScBO_3 .

249 One of the elastic properties of crystals with more importance for both
250 engineering science and crystal physics is the elastic anisotropy, because it is highly
251 correlated to the possibility of inducing microcracks in the materials [59]. This
252 anisotropy can be quantified with the universal elastic anisotropy index A_U [60], which
253 is defined as $A_U = 5(G_V/G_R) + (B_V/B_R) - 6$, where B_V , G_V , B_R and G_R are the bulk and shear
254 moduli in the Voigt and Reuss approximations, respectively. It is noteworthy that A_U
255 takes into account all the stiffness coefficients B_{ij} by recognizing the tensorial nature of

256 this physical magnitude [60]. If A_U is equal to 0, no anisotropy exists. On the other
257 hand, the more this parameter differs from 0 the more elastically anisotropic is the
258 crystalline structure. The two calcite-type orthoborates have A_U values above 0 at 0
259 GPa; therefore, they are anisotropic, being the anisotropy of InBO_3 slightly smaller than
260 that of ScBO_3 . The elastic anisotropy of both borates reflected by A_U is in agreement
261 with the longitudinal elastic anisotropy given by the C_{33}/C_{11} ratio and the anisotropy in
262 the axial compressibilities given by the κ_c/κ_a ratio both previously commented.

263 **Figures 4 and 5** show the pressure dependence of B , G , and E elastic moduli, ν
264 Poisson's ratio, B/G ratio and A_U for ScBO_3 and InBO_3 , respectively. It can be noted
265 that the Hill bulk modulus, B_H , increases with pressure reaching a maximum value of
266 294 GPa (258 GPa) at 51 GPa (38 GPa) for ScBO_3 (InBO_3) and above that pressure it
267 decreases as pressure increases. Contrarily, the G_H and E_H moduli decrease with
268 pressure for both borates. The Poisson's ratio increases with pressure, reaching a value
269 of 0.45 (0.43) at 54 GPa for ScBO_3 (InBO_3), and indicates an increment of the ductility
270 and of the metallic behavior with increasing pressure. However, we must note that our
271 *ab initio* calculations show that the bandgap of both borates increases with increasing
272 pressure so the increase of the Poisson's ratio is not related with the metallization of the
273 compound at high pressure because of a bandgap closure. Instead, the metallization
274 must be interpreted as a progressive loss of the ionic character of the material related to
275 the increase of atomic coordination and progressive loss of interatomic bond
276 directionality as pressure increases because bond directionality decreases in the series
277 covalent-ionic-metallic. Similarly, the B/G ratio is related to the Poisson's ratio [57] and
278 also increases with pressure in the two borates, thus indicating an increment of the
279 ductility with pressure, reaching a value of 9.3 (7.2) at 54 GPa in ScBO_3 (InBO_3).
280 Finally, the A_U universal anisotropy factor increases with increasing pressure in ScBO_3

281 and InBO₃, thus indicating that the elastic anisotropy increases in both compounds with
282 pressure.

283 One of the most common elastic properties and less easy to handle is hardness,
284 which is a property generally related to both the elastic and plastic properties of a
285 material. Hardness is an unusual physical property because it is not an intrinsic
286 materials property, but the result of a defined measurement procedure susceptible to
287 precise definitions in terms of fundamental units of mass, length, and time. In practice,
288 hardness is measured by the size of the indentation made on a specimen by a load of a
289 specified shape when a force is applied during a certain time. In this way, there are three
290 principal standard methods for expressing the relationship between hardness and the
291 size of the indentation, these being Brinell, Rockwell, and Vickers. The Vickers
292 hardness, H_v , can be calculated by the formula proposed by Tian et al. [61]:

293

$$294 \quad H_v = 0.92(G/B)^{1.137} G^{0.708} \quad (14)$$

295

296 We used this formula as it eliminates the possibility of unrealistic negative
297 hardness. The values of H_v for ScBO₃ and InBO₃ at 0 GPa are included in **Table 4**.
298 ScBO₃ is harder than InBO₃ and both have values of H_v of approximately 8-9 GPa when
299 using elastic moduli in the Hill approximation. Since H_v is smaller than 10 GPa, both
300 compounds can be classified as relatively soft materials. The soft behavior of both
301 orthoborates is correlated with their predicted ductility at zero pressure as previously
302 shown. It must be stressed that the calculated value of $H_v = 8.80$ GPa in the Hill
303 approximation for ScBO₃ is in good agreement with the measured average Vickers
304 hardness for Yb³⁺:ScBO₃ of $H_v = 8.19$ GPa [20]. On the other hand, the two

305 orthoborates have theoretical H_v values comparable to that of other ionic oxides such as
 306 ZrO_2 with theoretical $H_v \sim 9$ GPa and experimental $H_v = 13$ GPa [62].

307 **Figure 6** shows the pressure evolution of the Vickers hardness with pressure. It
 308 is observed that H_v decreases as pressure increases for both borates. This is related to
 309 the fact that the G/B ratio and the G elastic modulus decreases with pressure. In this
 310 way, as pressure increases, both borates become softer in good agreement with the
 311 increase of their ductility (B/G ratio) as stated above.

312 Finally, one elastic property which is fundamental for Earth Sciences in order to
 313 interpret seismic waves is the average sound velocity, v_m [63]. In polycrystalline
 314 materials v_m is given by [64]:

$$315 \quad v_m = \left[\frac{1}{3} \left(\frac{2}{v_{trans}^3} + \frac{1}{v_{lon}^3} \right) \right]^{-1/3} \quad (15)$$

316 where v_{trans} and v_{lon} are the transverse and longitudinal elastic wave velocities of the
 317 polycrystalline material which are given by:

$$318 \quad v_{lon} = \left(\frac{B + \frac{4}{3}G}{\rho} \right)^{1/2} \quad (16)$$

$$319 \quad v_{trans} = \left(\frac{G}{\rho} \right)^{1/2} \quad (17)$$

320 where B and G are the elastic moduli and ρ the density. Values of the density and wave
 321 velocities v_m , v_{lon} and v_{trans} at 0 GPa are given for the two orthoborates in **Table 4**. Wave
 322 velocities are greater for $ScBO_3$ than for $InBO_3$ because of the higher stiffness and
 323 smaller density of $ScBO_3$ than those of $InBO_3$. On the other hand, the average wave
 324 velocity for $ScBO_3$ (5408.8 m/s) is greater than that calculated for isoelectronic calcite-
 325 type $CaCO_3$ (4570 m/s) [65].

326 **Figure 7** reports the evolution of the elastic wave velocities for both borates.
 327 Using elastic moduli in the Hill approximation, the calculated v_{lon} increases with
 328 pressure reaching a maximum value of 9290.4 m/s (7171.1 m/s) at 27 GPa (21 GPa)
 329 for ScBO₃ (InBO₃) and decreases above that pressure. On the other hand, the
 330 corresponding velocities v_{trans} and v_m decrease as pressure increases.

331

332 **3.2. Thermodynamic properties**

333 The Debye temperature is a fundamental parameter that correlates with many
 334 physical properties of solids, such as specific heat, elastic constants, and melting
 335 temperature. One of the standard methods to calculate the Debye temperature, θ_D , is
 336 from elastic constant data using the semi-empirical formula [64]:

$$337 \quad \theta_D = \frac{h}{k_B} \left[\frac{3n}{4\pi} \left(\frac{N_A \rho}{M} \right) \right]^{1/3} v_m \quad (18)$$

338 where h is the Planck's constant, k_B is the Boltzmann's constant, n is the number of
 339 atoms in the molecule, N_A is the Avogadro's number, ρ is the density, M is the
 340 molecular weight, and v_m is the averaged sound velocity. As reported in **Table 4**, the
 341 values of θ_D at 0 GPa using the Hill approximation are 748.1 (553.3) K in ScBO₃
 342 (InBO₃). We note that the Debye temperature in InBO₃ is slightly greater than that
 343 obtained theoretically in calcite-type CaCO₃ (503 K) [65]. **Figure 8** reports the
 344 evolution with pressure of the Debye temperature, θ_D , for both borates. It is observed
 345 that θ_D decreases with pressure because v_m decreases with pressure.

346 The thermal conductivity is the property of a material that indicates its ability to
 347 conduct heat. In order to estimate the theoretical minimum of the thermal conductivity,
 348 we have used the following expression [66]:

$$\kappa_{\min} = k_B v_m \left(\frac{M}{n \rho N_A} \right)^{-2/3} \quad (19)$$

The values of κ_{\min} at 0 GPa in ScBO₃ (InBO₃) using the Hill approximation are 1.61 (1.17) W m⁻¹ K⁻¹. Therefore, both borates are low κ materials [67]. It must be stressed that the value of the minimum thermal conductivity in ScBO₃ at 0 GPa is in good agreement (i.e., smaller) with the average thermal conductivity for Yb³⁺:ScBO₃ measured at 300 K (3.3 W m⁻¹ K⁻¹) [20]. **Figure 9** reports the evolution with pressure of the minimum thermal conductivity, κ_{\min} , for both borates. As in the case of θ_D , κ_{\min} decreases with pressure because of the decreasing of v_m with pressure. On the other hand, if we use the simplified formula for κ_{\min} that considers $v_m = 0.87\sqrt{E/\rho}$ [66], the decreasing of κ_{\min} with pressure is explained by the decreasing of the tensile stiffness of both borates as pressure increases.

360

3.3. Mechanical stability of the calcite structure

In this section we are going to study the mechanical stability of the calcite-type structure in ScBO₃ and InBO₃ at HP. For that purpose, we will make use of the elastic stiffness coefficients reported in the previous section. The mechanical stability of a crystal at zero pressure can be studied with the Born stability criteria [68]. However, the study of the mechanical stability of a crystal at HP requires the generalization of the Born stability criteria to the case when an external load is applied [69-71]. These generalized stability criteria for trigonal crystals with six independent elastic constants are given by the following conditions:

$$M_1 = B_{11} > 0, \quad (20)$$

$$M_2 = B_{11} - B_{12} > 0 \quad (21)$$

$$M_3 = (B_{11} + B_{12})B_{33} - 2B_{13}^2 > 0 \quad (22)$$

$$M_4 = B_{44}(B_{11} - B_{12}) - 2B_{14}^2 = 2(B_{44}B_{66} - B_{14}^2) > 0 \quad (23)$$

$$M_5 = B_{44} > 0, \quad (24)$$

376 **Figure 10** shows the pressure dependence of the generalized stability criteria for
 377 ScBO₃ and InBO₃. As it can be observed, our calculations show that all the above
 378 criteria are satisfied for the two orthoborates at 0 GPa, thus the calcite-type structure is
 379 mechanically stable at 0 GPa. In ScBO₃, all stability criteria are satisfied at HP except
 380 M_4 and M_3 (note that these two criteria are divided by 100 in the figure) which are
 381 violated at 57.7 and 69.7 GPa, respectively. Similarly, all stability criteria are satisfied
 382 at HP in InBO₃ except M_3 and M_4 which are violated at 56.2 and 59.6 GPa, respectively.
 383 In summary, our calculations show that calcite-type ScBO₃ and InBO₃ become
 384 mechanically unstable between 56 and 58 GPa.

385 As regards the mechanical stability of solids, it is interesting to note that the A_U
 386 universal anisotropy factor increases quickly at HP when the compound approaches the
 387 mechanical instability (see **Figs. 4 and 5**). On the other hand, M_3 enters the numerator
 388 of B_R and G_R (**Eqs. 6 and 9**) while $M_4/2$ is in the numerator of G_R (**Eq. 9**). Therefore, B_R
 389 and G_R moduli for InBO₃ (see **Fig. 5**) and G_R modulus for ScBO₃ (see **Fig. 4**) go to zero
 390 as pressure approaches to the instability region. HP experimental studies reported to
 391 date have not checked the stability of these borates up to those pressures [21].

392 Finally, we must mention that the structural stability of the calcite-type structure
 393 in ScBO₃ on doping has been previously studied. In this way, it has been demonstrated
 394 the higher structural stability of the calcite-type structure than the vaterite-type structure
 395 at room pressure in ScBO₃ when Sc atoms are substituted by Y atoms [72]. However,
 396 substitution of Sc atoms in ScBO₃ by much larger Gd and La ions has been found to

397 result in the formation of the huntite-type structure [73]. We hope the present work will
398 foster studies of structural stability of these borates with different dopants and at higher
399 pressures to those already reported.

400

401 **4. Conclusions**

402 We have theoretically studied the elastic and thermodynamic behavior of two
403 calcite-type orthoborates (ScBO_3 and InBO_3) at high pressure. It has been found that the
404 elastic stiffness coefficients in both borates are similar at 0 GPa. The elastic constants
405 and the elastic stiffness coefficients increase with increasing pressure in all the pressure
406 range except for B_{44} and B_{66} . The evolution with pressure of the B , G , and E elastic
407 moduli, ν Poisson's ratio, B/G ratio and A_U universal elastic anisotropy index is similar
408 in both borates. In this context, both compounds are ductile and more resistive to
409 volume compression than to shear deformation ($B > G$) at all pressures. Furthermore,
410 the elastic anisotropy increases with increasing pressure in both borates. The two
411 borates are relatively soft at 0 GPa and their hardness decreases with increasing
412 pressure. The average elastic wave velocity, Debye temperature and minimum thermal
413 conductivity of both borates decreases with increasing pressure and are lower in InBO_3
414 than in ScBO_3 . From the behavior of the elastic stiffness coefficients at high pressure
415 we have studied the mechanical stability of the calcite-type structure at high pressure in
416 both compounds and have found that this structure becomes mechanically unstable at
417 56.2 (57.7) GPa in InBO_3 (ScBO_3).

418

419

420

421 **Acknowledgements**

422 This study is supported by the Spanish MICINN projects MAT2013-46649-C4-
423 2-P/3-P, CSD2007-00045 and MAT2015-71070-REDC. H.M.O., A.M., and P.R-H.
424 acknowledge computing time provided by Red Española de Supercomputación (RES)
425 and MALTA-Cluster. J.A.S. acknowledges Juan de la Cierva fellowship program for
426 financial support.

427

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539 **Table 1.** C_{ij} elastic constants (in GPa) for the two calcite-type orthoborates at 0 GPa are
540 given in column C^0 . The linear and quadratic pressure coefficients a and b for the C_{ij}
541 obtained by fitting data to the equation $C_{ij} = C_{ij}^0 + a \cdot P + b \cdot P^2$ are also given. Note that
542 taking into account the definition of the elastic stiffness coefficients B_{ij} from C_{ij} , the
543 linear and quadratic pressure coefficients a_B and b_B for B_{ij} ($B_{ij} = B_{ij}^0 + a_B \cdot P + b_B \cdot P^2$) are
544 given by: $a_B = a - 1$ and $b_B = b$ for B_{11} , B_{33} , B_{44} , and B_{66} ; $a_B = a + 1$ and $b_B = b$ for B_{12}
545 and B_{13} ; and $a_B = a$ and $b_B = b$ for B_{14} .

546

	ScBO ₃			InBO ₃		
	C^0 (GPa)	a	b ($\times 10^{-2}$ GPa ⁻¹)	C^0 (GPa)	a	b ($\times 10^{-2}$ GPa ⁻¹)
C_{11}	337.4	4.54(3)	-1.06(5)	321.5	5.34(4)	-0.96(8)
C_{12}	134.7	3.67(1)	-0.28(1)	139.0	3.82(1)	-0.07(2)
C_{13}	113.0	3.13(1)	-0.82(2)	113.9	3.52(2)	-1.27(2)
C_{14}	30.3	0.71(1)	-0.39(1)	21.0	0.87(1)	-0.43(2)
C_{33}	205.5	2.50(2)	-0.93(3)	187.8	2.26(3)	-1.03(5)
C_{44}	78.7	1.03(1)	-0.62(2)	68.4	1.14(2)	-0.70(3)
C_{66}	101.3	0.55(1)	-0.71(4)	91.2	0.92(2)	-0.96(6)

547

548 **Table 2.** κ_a and κ_c axial compressibilities in ScBO₃ and InBO₃ obtained from the elastic
 549 constants along with the κ_c/κ_a ratio at 0 GPa. Values for κ_a and κ_c reported in **Ref [21]**
 550 are also included for comparison.

551
 552

Compound	κ_a (10^{-3} GPa ⁻¹)	κ_c (10^{-3} GPa ⁻¹)	κ_c/κ_a	
ScBO ₃	1.29	3.44	2.67	This work
ScBO ₃	1.30(2)	3.40(3)	2.62(2)	Ref [21] ^a
ScBO ₃	1.13(3)	3.6(3)	3.2(1)	Ref [21] ^b
InBO ₃	1.22	3.84	3.15	This work
InBO ₃	1.38(3)	3.75(3)	2.72(3)	Ref [21] ^a
InBO ₃	1.6(2)	3.49(5)	2.2(1)	Ref [21] ^b

553

554 ^a Obtained from a Murnaghan equation of state fit to theoretical data.

555 ^b Obtained from a Murnaghan equation of state fit to experimental data.

556 **Table 3.** Elastic moduli B , G , and E (in GPa) and Possion's ratio (ν) given in the Voigt,
 557 Reuss and Hill approximations, labeled respectively with subscripts V , R , and H , in
 558 ScBO_3 and InBO_3 at 0 GPa. The B/G ratio and the universal anisotropy index (A_U) are
 559 also included.

560

	ScBO_3	InBO_3
B_V, B_R, B_H	178.0, 165.8, 171.9	173.8, 159.1, 166.5
G_V, G_R, G_H	86.4, 75.8, 81.1	76.5, 69.2, 72.8
E_V, E_R, E_H	223.1, 197.4, 210.2	200.2, 181.2, 190.7
ν_V, ν_R, ν_H	0.29, 0.30, 0.30	0.31, 0.31, 0.31
$B_V/G_V, B_R/G_R, B_H/G_H$	2.06, 2.19, 2.12	2.27, 2.30, 2.29
A_U	0.77	0.63

561

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564

565 **Table 4.** Vickers hardness (H_v in GPa), longitudinal (v_{lon} in m/s), transverse (v_{trans} in
566 m/s) and averaged (v_m in m/s) elastic wave velocity, Debye temperature (θ_D in K), and
567 minimum thermal conductivity (κ_{min} in $\text{W m}^{-1} \text{K}^{-1}$) in ScBO_3 and InBO_3 at 0 GPa. Data
568 are given in the Voigt, Reuss and Hill approximations indicated with V , R , and H ,
569 respectively. The density, ρ , of both borates is also included.

570

	ScBO_3	InBO_3
$H_v (V, R, H)$	9.50, 8.10, 8.80	7.81, 7.16, 7.49
$v_{\text{lon}} (V, R, H)$	9210.8, 8788.4, 9002.1	7070.3, 6748.4, 6911.2
$v_{\text{trans}} (V, R, H)$	5000.1, 4684.3, 4844.7	3723.9, 3540.1, 3633.2
$v_m (V, R, H)$	5578.7, 5233.3, 5408.8	4163.8, 3959.4, 4062.9
$\theta_D (V, R, H)$	771.6, 723.8, 748.1	567.0, 539.2, 553.3
$\kappa_{\text{min}} (V, R, H)$	1.66, 1.56, 1.61	1.20, 1.14, 1.17
$\rho (\text{g/cm}^3)$	3.455	5.519

571

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573

574 **Figure captions**

575

576 **Figure 1. (Color online)** Calcite-type structure for ScBO₃. The large (blue) spheres
577 correspond to Sc atoms, the medium (green) spheres to B atoms, and the small (red)
578 spheres to O atoms.

579 **Figure 2. (Color online)** Pressure dependence of the theoretical elastic constants (a)
580 and elastic stiffness coefficients (b) in ScBO₃. Solid lines connecting the calculated data
581 points are guides to the eyes.

582 **Figure 3. (Color online)** Pressure dependence of the theoretical elastic constants (a)
583 and elastic stiffness coefficients (b) in InBO₃. Solid lines connecting the calculated data
584 points are guides to the eyes.

585 **Figure 4. (Color online)** Pressure dependence of (a) B , (b) G , (c) E , (d) ν , (e) B/G , and
586 (f) A_U in ScBO₃. Squares, circles, and triangles refer to the Voigt, Reuss, and Hill
587 approximations; respectively. Solid lines connecting the calculated data points are
588 guides to the eyes in panels (a) to (f).

589 **Figure 5. (Color online)** Pressure dependence of (a) B , (b) G , (c) E , (d) ν , (e) B/G , and
590 (f) A_U in InBO₃. Squares, circles, and triangles refer to the Voigt, Reuss, and Hill
591 approximations; respectively. Solid lines connecting the calculated data points are
592 guides to the eyes in panels (a) to (f).

593 **Figure 6. (Color online)** Evolution with pressure of the Vickers hardness in ScBO₃ (a)
594 and InBO₃ (b). Squares, circles, and triangles refer to the Voigt, Reuss, and Hill
595 approximations, respectively.

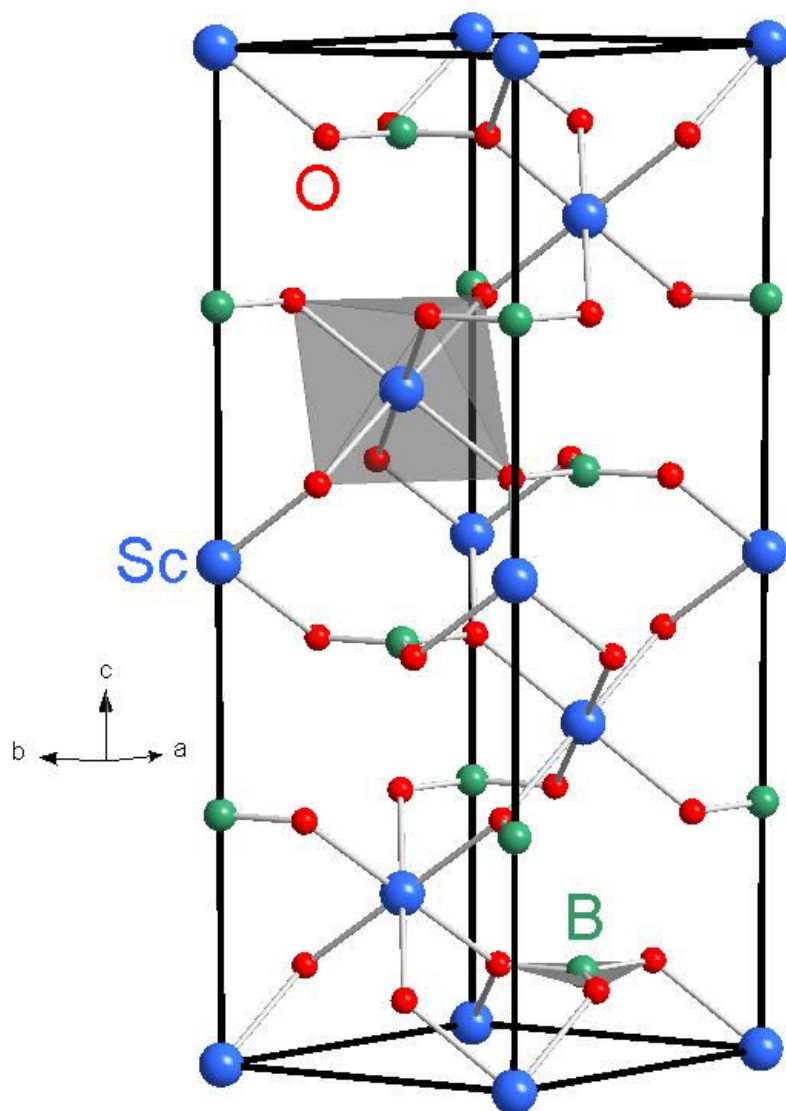
596 **Figure 7. (Color online)** Pressure dependence of the longitudinal (v_{lon}), transverse
597 (v_{trans}), and average (v_m) elastic wave velocity in ScBO₃ and InBO₃. Squares, circles, and
598 triangles refer to the Voigt, Reuss, and Hill approximations, respectively.

599 **Figure 8. (Color online)** Evolution with pressure of the Debye temperature in ScBO₃
600 (a) and InBO₃ (b). Squares, circles, and triangles refer to the Voigt, Reuss, and Hill
601 approximations, respectively.

602 **Figure 9. (Color online)** Evolution with pressure of the minimum thermal conductivity
603 (κ_{min}) in ScBO₃ (a) and InBO₃ (b). Squares, circles, and triangles refer to the Voigt,
604 Reuss, and Hill approximations, respectively.

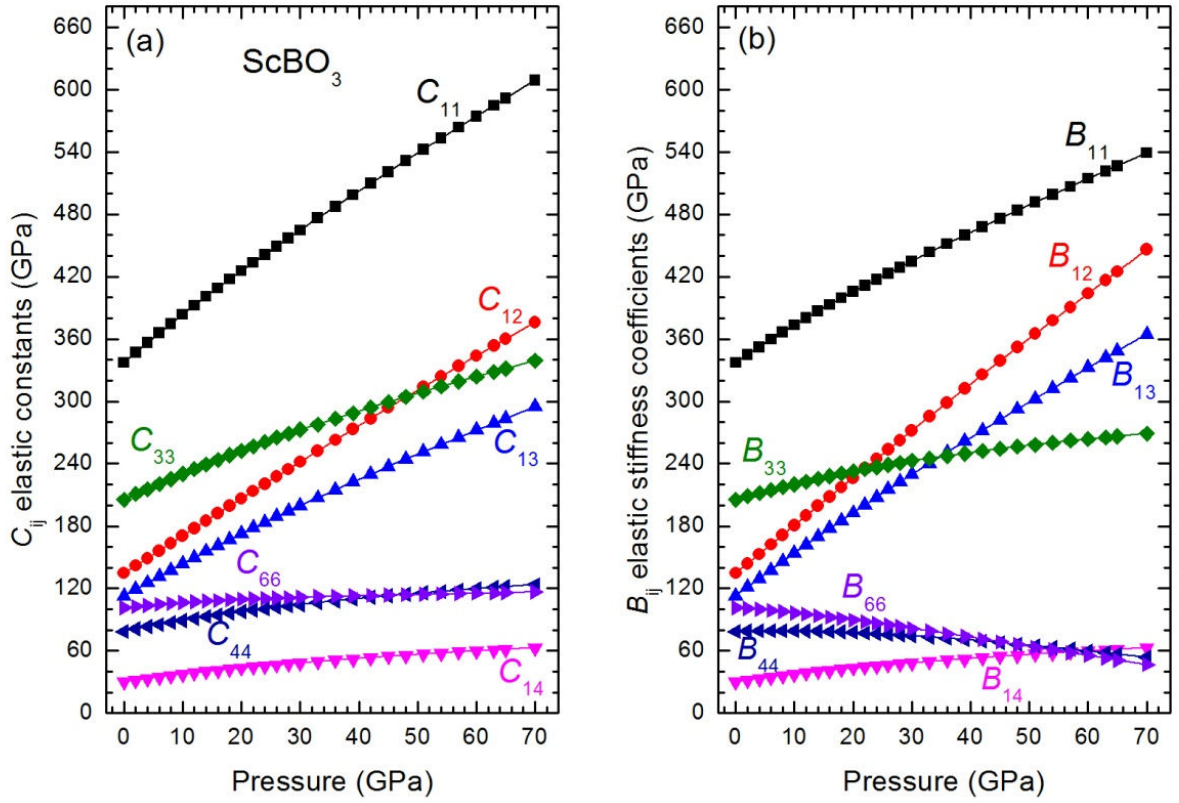
605 **Figure 10. (Color online)** General stability criteria in ScBO₃ (a) and InBO₃ (b). The
606 pressure P_{mu} at which each borate becomes mechanically unstable is indicated.

607 **Figure 1**



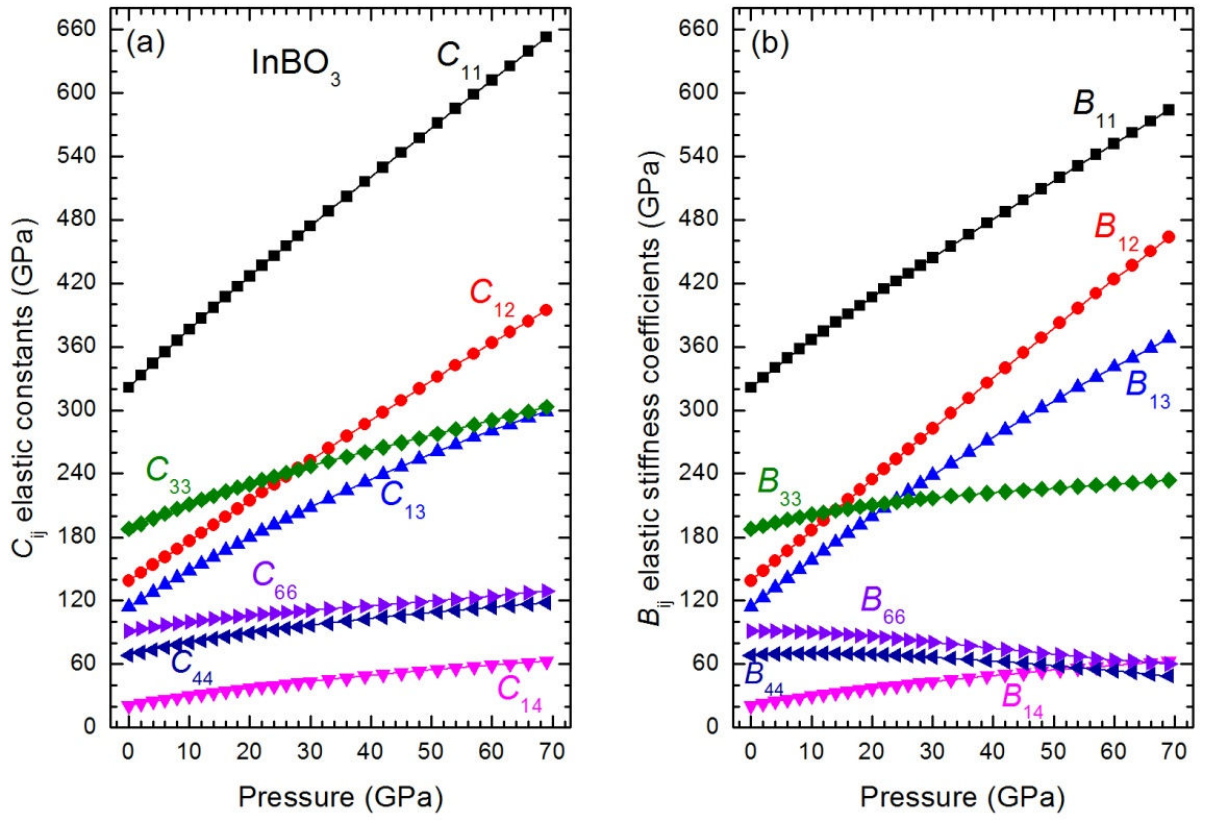
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610 **Figure 2**



611
612

613 **Figure 3**



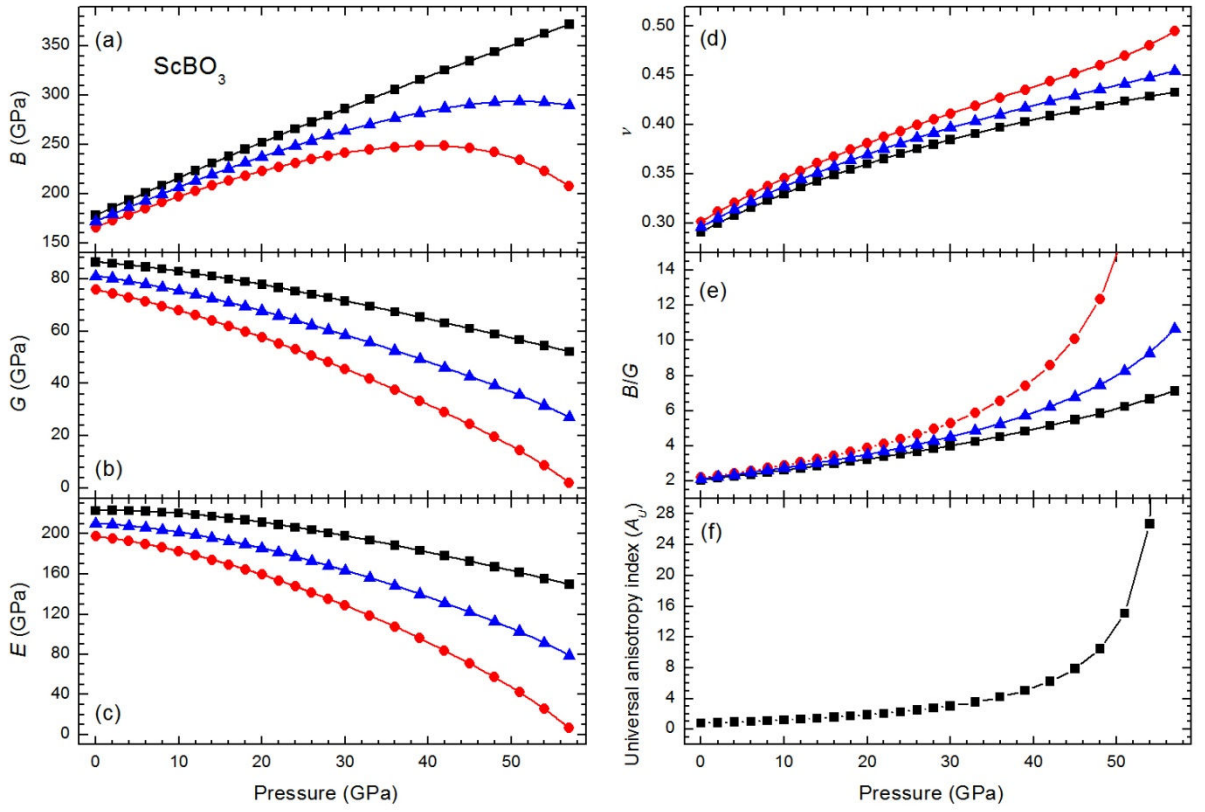
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617 **Figure 4**

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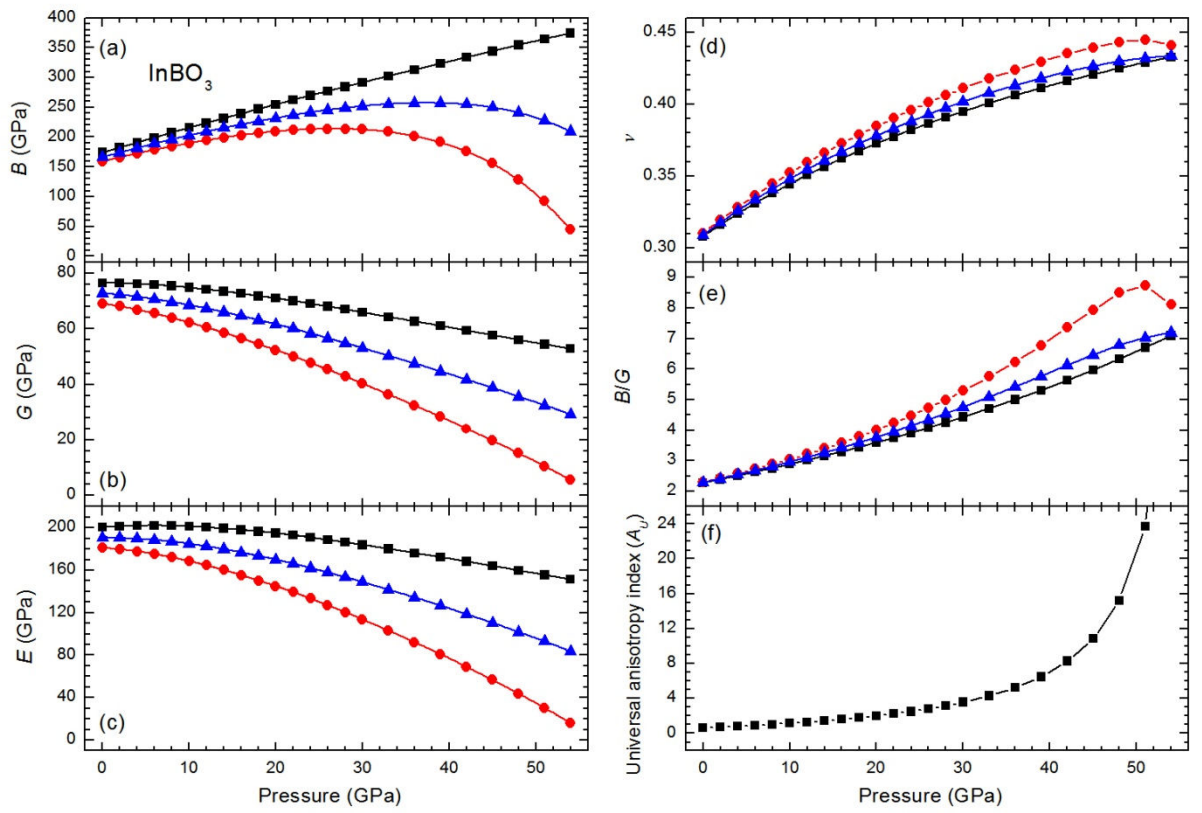
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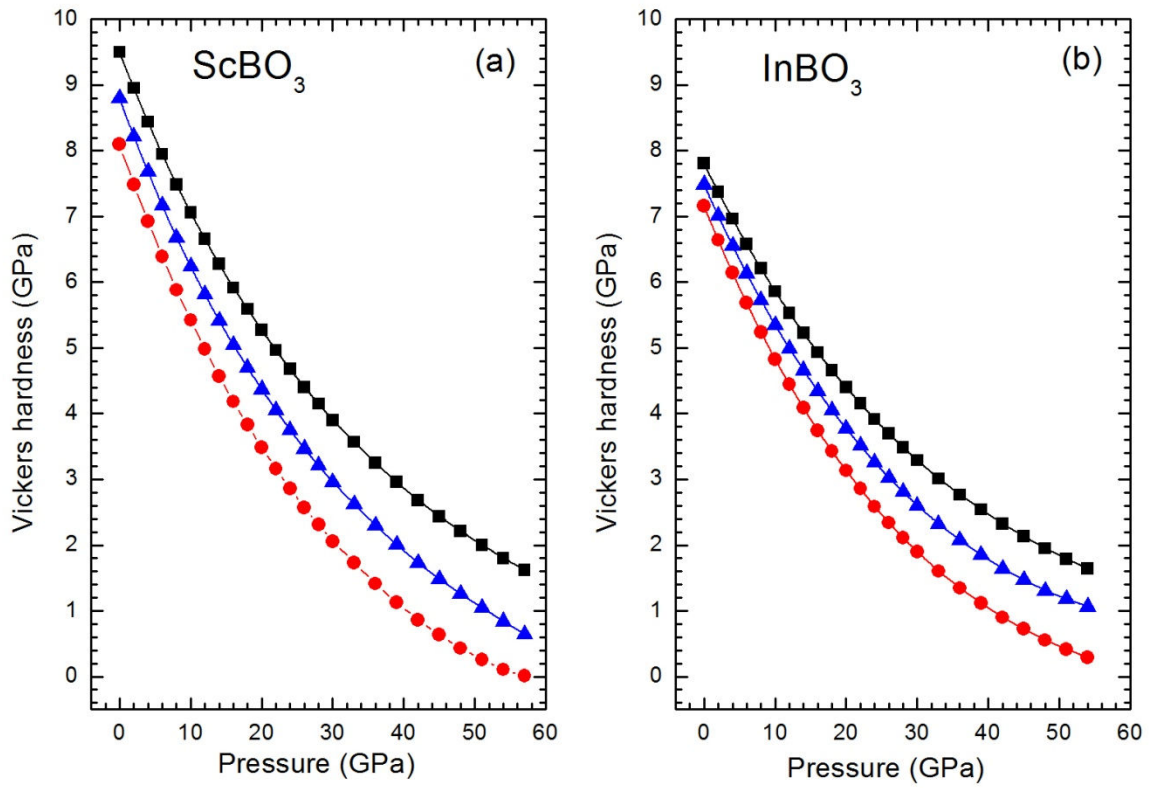
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624 **Figure 5**
625



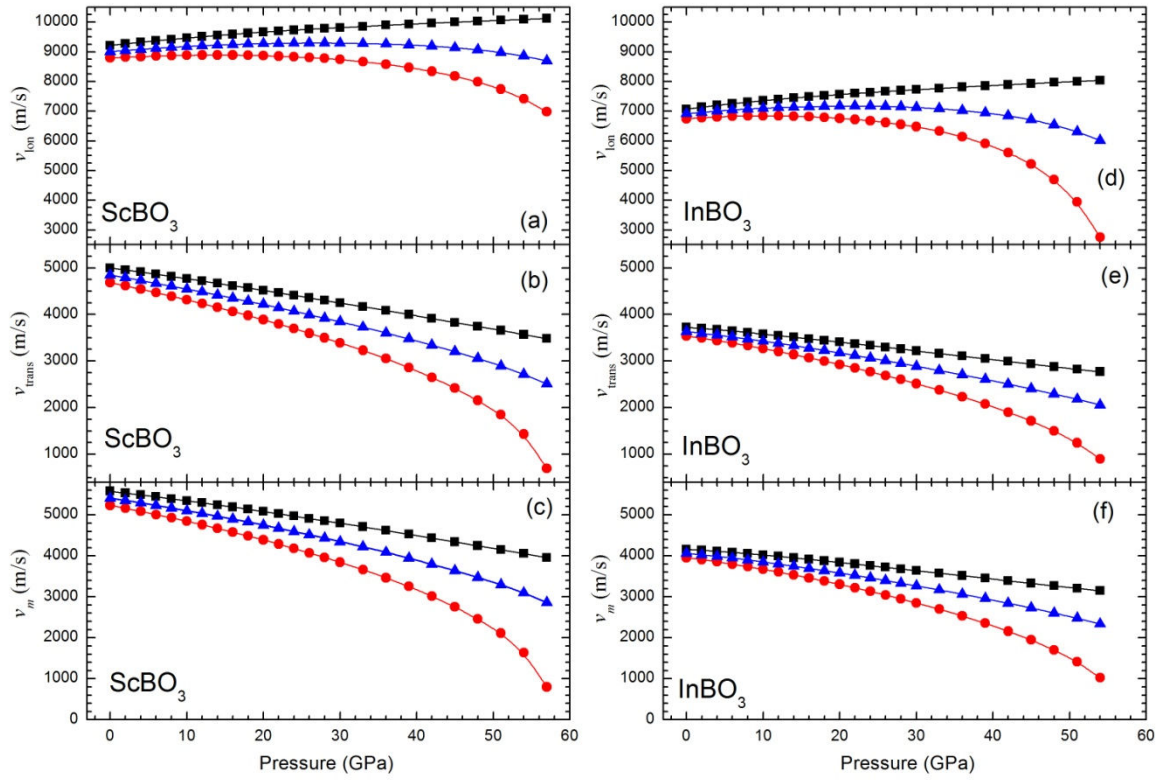
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628 **Figure 6**



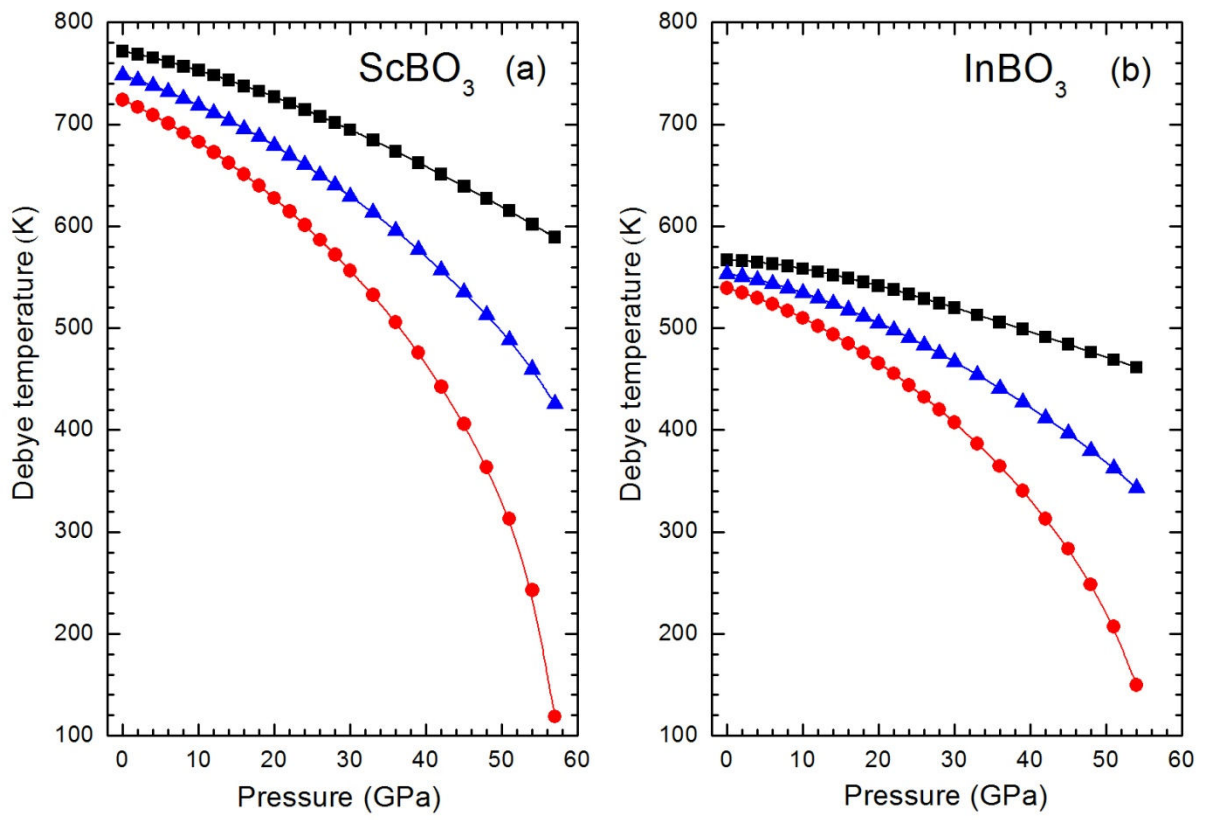
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631 **Figure 7**



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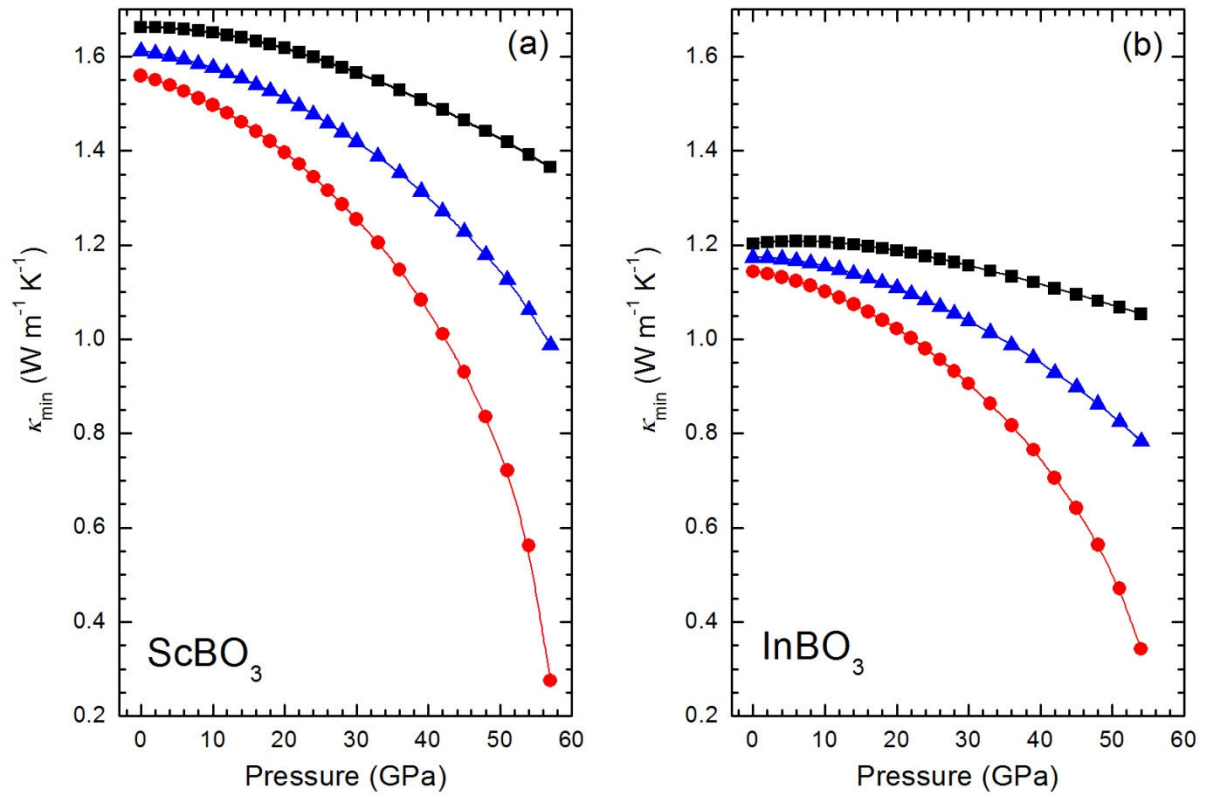
634 **Figure 8**



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637 **Figure 9**

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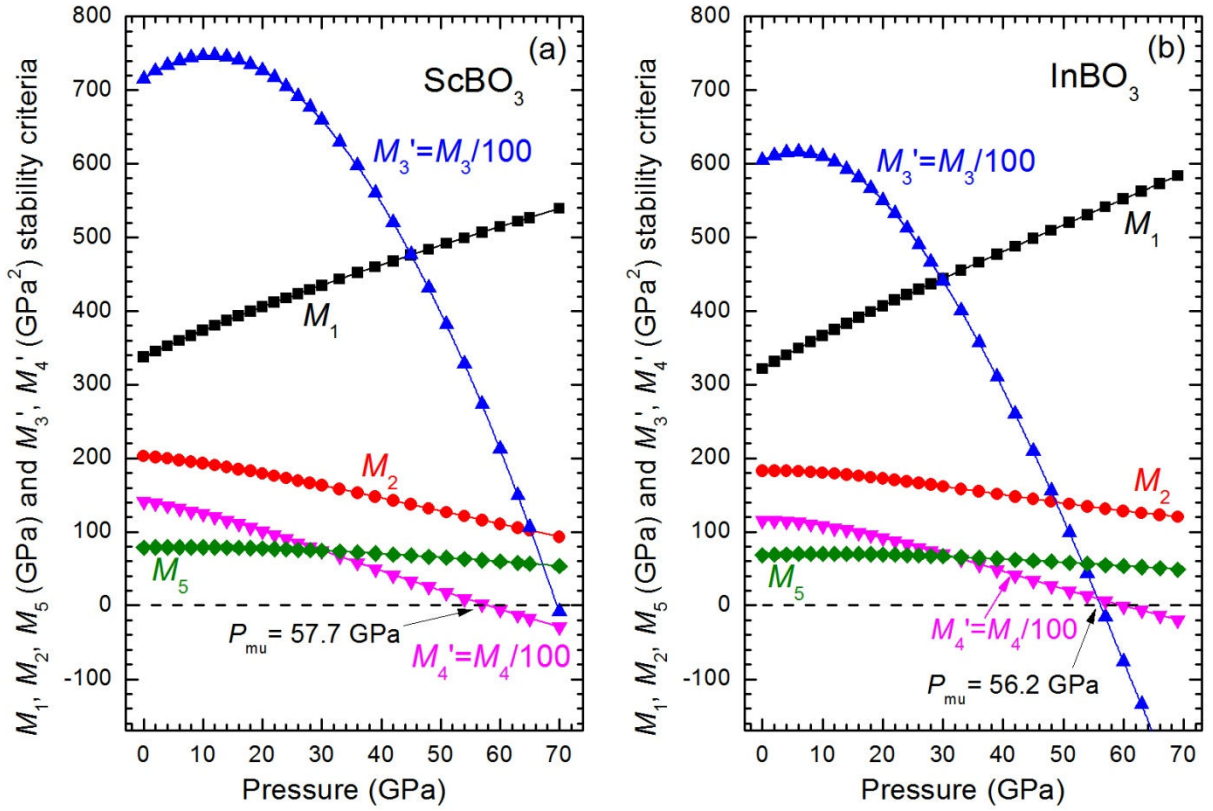
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642 **Figure 10**

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