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Additional Information

1	Properties of starch-hydroxypropyl methylcellulose based films obtained by
2	compression molding.
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13 ABSTRACT

Corn starch-glycerol (1:0.3) films, containing or not citric acid (1g/100 g starch) and 14 HPMC (10 and 20 g/100g starch), are obtained by compression moulding. The 15 microstructure of the films, the thermal behaviour, the X-Ray diffraction spectra and the 16 physical properties (mechanical, barrier and optical) were analysed after 1 and 5 storage 17 weeks at 25°C and 53% relative humidity. The bonded citric acid and film solubility 18 were also determined. Starch-HPMC blend films showed a dispersed phase of HPMC in 19 a continuous, starch-rich phase with lower glass transition than HPMC-free films. The 20 addition of citric acid also provoked a decrease in glass transition in line with the partial 21 22 hydrolysis of starch chains. Both components implied a decrease in the water vapour permeability while the oxygen permeability slightly increased. Although citric acid only 23 provoked a small hardening effect in the films, it greatly decreased their extensibility 24 25 (weak cross-linking effect), which seems to increase during film storage. Starch crystallization during storage was inhibited by both citric acid and HPMC. 26

27

28 Key words: Starch, compression molding, citric acid, HPMC, crystallization

30 1. INTRODUCTION

31 Society's awareness of the importance of both environmental conservation and green technologies, and the growing environmental contamination caused by synthetic 32 polymers based on petroleum, have led to an increased interest in developing 33 environmentally friendly materials, such as biodegradable polymers based on 34 polysaccharides. In the development of biodegradable materials, starch is the most 35 promising of the polysaccharide polymers, due to its low cost, great processability, and 36 abundance (Yoon, Chough & Park, 2006; Ghanbarzadeh, Almasi & Entezami, 2011). 37 Starch films exhibit some good properties, such as high barrier to oxygen, carbon 38 dioxide and lipids. However, poor water vapor permeability and mechanical properties, 39 and the recrystallization during storage, are limitations of this material (Kester & 40 Fennema, 1986; Arık Kibar & Us, 2013). 41

42 The deficiencies in the properties of starch films can be improved by different methods. The phenomenon of the recrystallization of starch films could be solved by combining 43 44 starch with other polymers, as has been proven by other authors (Funami, Kataoka, Omoto, Goto, Asai & Nishinari, 2005; Jiménez, Fabra, Talens & Chiralt, 2012a). 45 Hydroxypropyl methylcellulose (HPMC) is a cellulose-derived polymer commonly 46 used for obtaining edible, biodegradable films (Albert & Mittal, 2002; Villalobos, 47 Hernández-Muñoz & Chiralt, 2006; Sánchez-González, Vargas, González-Martínez, 48 Chiralt & Cháfer, 2009) with good availability and processability (Fahs, Brogly, Bistac 49 & Schmitt, 2010; Jiménez et al., 2012a) which have excellent film-forming properties 50 (Villalobos et al., 2006). Compared to other polymers, HPMC films have great 51 mechanical strength, (Jiménez, Fabra, Talens & Chiralt, 2010; 2012a) but limited 52 barrier properties. In this sense, Jiménez et al. (2012a) observed that the oxygen 53 permeability of HPMC films obtained by casting was approximately 100 times higher 54

than cornstarch films, while the water barrier properties are similar for films made from
both polymers.

Nevertheless, the thermal stability of HPMC films means that they can be thermally 57 processed using industrial equipment, and previous studies (Jiménez et al., 2012a) 58 revealed inhibition of starch crystallization when blend films were obtained by casting 59 the aqueous dispersions, the films showing a more amorphous character. So, HPMC-60 starch blends could be used to obtain thermally processed films with interesting 61 properties, although phase separation in corn starch-HPMC films obtained by casting 62 has been observed by scanning electron microscopy (Jiménez et al., 2012a), with the 63 64 films exhibiting a starch-rich phase and a HPMC-rich phase in what is practically a bilayer film. 65

The poor compatibility of these polymers can be limited by the incorporation of 66 67 compatibilizer compounds, which promotes the esterification of the starch -OH groups. For this purpose, cross-linking agents, such as phosphorus oxychloride, sodium 68 69 trimetaphosphate, sodium tripolyphosphate, epichlorohydrin, and 1,2,3,4diepoxybutane, were used (Seker & Hanna, 2006; Reddy & Yang, 2010). These 70 substances are relatively toxic and expensive (Reddy & Yang, 2010), so their use in 71 food packaging is not recommendable. However, using polycarboxylic acids as cross-72 linking agents is a good alternative. This is especially so in the case of citric acid, a low 73 cost organic acid widely used in the food industry, that acts as a cross-linking agent due 74 to the presence of several carboxyl groups in its molecular structure (Ghanbarzadeh, 75 Almasi & Entezami, 2010). These groups can react with the hydroxyl groups of starch 76 molecules through the formation of esters. According to Reddy & Yang (2010), the 77 esterification reaction using polycarboxylic acids occur with the polymer hydroxyl 78 groups, at high temperatures (about 160 °C), through the formation of anhydride groups 79

(Yang, Wang, & Kang, 1997). This interaction can decrease the retrogradation and 80 81 recrystallization of starch during storage time (Ghanbarzadeh et al., 2011). The compatibilizer effect of the citric acid in the starch-polymer blends, as well as an 82 improvement in the properties of starch films, have been reported in several studies (Yu, 83 Wang & Ma, 2005; Shi, Bi, Zhang, Zhu, Chen, Zhou, Zhang & Tian, 2008; Ma, Chang, 84 Yu & Stumborg, 2009; Reddy & Yang, 2010; Ghanbarzadeh et al., 2010; 2011). The 85 most promising results derived from the addition of citric acid to the polymeric matrix 86 are the increase in thermal stability and the improvement in the barrier properties (Yu et 87 al., 2005; Reddy & Yang, 2010). 88

The aim of this work was to study the effect of citric acid addition on the structural and physical properties of corn starch films obtained by compression molding, combined with different ratios of HPMC, using glycerol as plasticizer. The effect of storage time on the film properties was also analyzed.

93

94 2. MATERIALS AND METHODS

95 2.1. Materials

96 Corn starch was obtained from Roquette (Roquette Laisa España, Benifaió, Spain). Its
97 moisture content was 10 % w/w and amylose percentage was 14%. Glycerol was
98 purchased from Panreac Química, S.A. (Castellar del Vallès, Barcelona, Spain).
99 Hydroxypropyl methylcellulose (HPMC) and citric acid (CA) were provided by Fluka
100 (Sigma–Aldrich Chemie, Steinheim, Germany).

101

102 **2.2. Film preparation**

Native starch and glycerol, as plasticizer, were dispersed in water. HPMC was hydrated
in cold water (5% w/w) under continuous stirring. The HPMC dispersion and the

aqueous mixture of starch and glycerol were mixed in different ratios to obtain two blends with 1:0.1 and 1:0.2 starch:HPMC ratios. The polymer:glycerol ratio was 1:0.3. CA was mixed to obtain four blends with and without CA; a constant starch:CA ratio of 1:0.01 was used in every case. Blends of starch-glycerol and starch-glycerol-citric acid, in the previously described ratios, were studied as control formulations. The abbreviations used for the studied formulations were: SG: starch-glycerol; CA: citric acid; H10: 10g HPMC/100 g starch; H20: 20g HPMC/100 g starch.

The formulations were hot-mixed on a two-roll mill (Model LRM-M-100, Labtech Engineering, Thailand) at 160 °C and 8 rpm for 20 minutes. A visual good miscibility of HPMC, CA and starch was obtained. A trowel was used during mixing to smoothly spread the material on the rolls. The paste sheet formed was removed from the mill and conditioned at 25 °C and 53% Relative Humidity (RH), using a Mg(NO₃)₂ saturated solutions (Panreac Quimica, SA, Castellar del Valles, Barcelona, Spain), for 48 hours.

Afterwards, films were obtained by compression molding (Model LP20, Labtech Engineering, Thailand). Four grams of the pre-conditioned paste were put onto steel sheets and pre-heated on the heating unit for about 5 min. Compression molding was performed at 160°C for 2 minutes at a pressure of 30 bars, followed by 6 minutes at 130 bars; thereafter, the cooling cycle was applied for 3 minutes. The films were conditioned at 25°C and 53% RH for 1 week for the initial time characterization and for 5 weeks for the final time characterization.

125

126 **2.3. Film characterization**

127 <u>2.3.1. Film thickness</u>

A Palmer digital micrometer was used to measure film thickness to the nearest 0.0025
mm at six random positions around the film.

130

131 <u>2.3.2. Scanning electron microscopy (SEM)</u>

The microstructural analysis of the cross-sections and surface of the films was carried out by means of a scanning electron microscope (JEOL JSM-5410, Japan). The film samples were maintained in desiccators with P_2O_5 for two weeks to guarantee that water was not present in the sample and observations were taken in duplicate for each film sample and in two films per formulation.

Film pieces, 0.5 cm^2 in size, were cryofractured from films and fixed on copper stubs,

138 gold coated, and observed using an accelerating voltage of 10 kV.

139

140 <u>2.3.3. X-ray diffraction</u>

A diffractometer (XRD, Bruker AXS/D8 Advance) was used to record the X-ray diffraction patterns. All the samples (equilibrated for one and five weeks at 25 °C and at 53% RH) were analyzed at 25 °C and 53% RH, between $2\theta = 5^{\circ}$ and $2\theta = 30^{\circ}$ using K α Cu radiation (λ : 1.542 Å), 40 kV and 40 mA with a step size of 0.05°. For this analysis, samples were cut into 4 cm squares. Pure citric acid was also analyzed, so as to identify its characteristic peaks.

147

148 2.3.4. Atomic force microscopy (AFM)

Samples equilibrated for five weeks at 25 °C and 0 % RH, using P₂O₅ saturated solutions (Panreac Quimica, SA, Castellar del Valles, Barcelona, Spain), were used. The surface morphology of the films was analyzed using an atomic force microscope (Multimode 8, Bruker AXS, Santa Barbara, USA) with NanoScope[®] V controller electronics. Measurements were taken from several areas of the film surface ($20 \mu m^2$) using the PeakForce QNM mode. Method ASME B46.1 (ASME, 1995) was used to

calculate the following statistical parameters related with sample roughness: average 155 roughness (Ra: average of the absolute value of the height deviations from a mean 156 surface), root-mean-square roughness (Rq: root-mean-square average of height 157 deviations taken from the mean data plane), and factor of roughness (r: ratio between 158 the three-dimensional surface and two-dimensional area projected onto the threshold 159 plane). The DMT modulus, derived from the Peak Force QNM Mode, was also applied 160 to obtain the surface maps showing the heterogeneities present in the surface properties. 161 Three replicates were considered for each sample. 162

163

164 <u>2.3.5. Optical properties</u>

The Kubelka-Munk theory for multiple scattering was applied to the reflection spectra 165 to determine the film's transparency (Hutchings, 1999). The surface reflectance spectra 166 167 were determined from 400 to 700 nm using a spectro-colorimeter CM- 3600d (Minolta Co., Tokyo, Japan) on both a white and a black background. As the light passes through 168 169 the film, it is partially absorbed and scattered, which is quantified by the absorption (K) 170 and the scattering (S) coefficients. The internal transmittance (Ti) of the films was determined using eq. (1). In this equation, R_0 is the reflectance of the film on an ideal 171 black background. Parameters a and b were calculated by means of eqs. (2) and (3), 172 where R is the reflectance of the sample layer backed by a known reflectance, Rg. Three 173 replicates were used for each sample on the free film surface. For the purposes of the 174 analysis, a wavelength of 450 nm was considered. 175

176

$$T_i = \sqrt{(a - R_0)^2 - b^2}$$
(1)

178

179
$$a = \frac{1}{2} \left(R + \frac{R_0 - R + R_g}{R_0 R_g} \right)$$
(2)

180

$$b = \sqrt{a^2 - 1} \tag{3}$$

182

181

The gloss was determined on the free film surface, at a 60° incidence angle by means of a flat surface gloss meter (Multi Gloss 268, Minolta, Germany), following the ASTM standard D523 method (ASTM, 1999). The measurements of each sample were taken in triplicate and three films were measured from each formulation. The results were expressed as gloss units (GU), relative to a highly polished surface of black glass standard with a value near to 100 GU.

189

190 <u>2.3.6. Moisture content</u>

The films that had been previously conditioned at 53% RH were dried for 24h at 60 °C (J.P. Selecta, S.A. Barcelona, España) and placed in a desiccator with P_2O_5 (Panreac Quimica, S.A. Castellar Vallés, Barcelona) adjusting them to 0% RH and 25 °C for 2 weeks. The reported results represent the average of three samples.

195

196 <u>2.3.7. Water vapour permeability (WVP)</u>

The WVP of films was determined by means of the ASTM E96-95 (ASTM, 1995) 197 gravimetric method, taking the modification proposed by McHugh, Avena-Bustillos & 198 Krochta (1993) into account. Distilled water was placed in Payne permeability cups (3.5 199 cm diameter, Elcometer SPRL, Hermelle/s Argenteau, Belgium) to expose the film to 200 100% RH on one side. Once the films were secured, each cup was placed in a relative 201 humidity equilibrated cabinet at 25 °C, with a fan placed on the top of the cup in order 202 to reduce resistance to water vapour transport, thus avoiding the stagnant layer effect in 203 this exposed side of the film. The RH of the cabinets (53%) was held constant using 204

205 oversaturated solutions of magnesium nitrate-6-hydrate. The cups were weighed 206 periodically (0.0001 g) and water vapour transmission (WVTR) was determined from 207 the slope obtained from the regression analysis of weight loss data versus time, once the 208 steady state had been reached, divided by the film area. From WVTR data, the vapour 209 pressure on the film's inner surface (p2) was obtained using eq. (4), proposed by 210 McHugh *et al.* (1993), to correct the effect of concentration gradients.

- 211
- 212

$$WVTR = \frac{P \cdot D \cdot L_n \left[P - p_2 \setminus P - p_1\right]}{R \cdot T \cdot \Delta z} \tag{4}$$

213

where P, total pressure (atm); D, diffusivity of water through air at 25 °C (m2 /s); R, gas law constant (82.057 x 10^{-3} m³ atm kmol⁻¹ K⁻¹); T, absolute temperature (K); Δz , mean stagnant air gap height (m), considering the initial and final z value; p₁, water vapour pressure on the solution surface (atm); and p₂, corrected water vapour pressure on the film's inner surface (atm). Water vapour permeance was calculated using eq. (5) as a function of p₂ and p₃ (pressure on the film's outer surface in the cabinet).

220

221

$$permeance = \frac{WVTR}{p_2 - p_3} \tag{5}$$

222

223 Permeability was calculated by multiplying the permeance by film thickness.

224

225 <u>2.3.8. Oxygen permeability (OP)</u>

The oxygen permeation rate of the films was determined at 53% RH and 25 °C using an OX-TRAN (Model 2/21 ML Mocon Lippke, Neuwied, Germany). The samples were conditioned at the relative humidity level of the test in a desiccator using magnesium nitrate-6-hydrate saturated solutions. Three samples were placed in the equipment for analysis, and the transmission values were determined every 20 min until equilibrium was reached. The exposure area during the tests was 50 cm^2 for each sample. To obtain the oxygen permeability, the film thickness was considered in every case.

233

234 <u>2.3.9. Tensile properties</u>

A universal test Machine (TA.XTplus model, Stable Micro Systems, Haslemere, 235 England) was used to determine the tensile strength (TS), elastic modulus (EM), and 236 elongation (E) of the films, following ASTM standard method D882 (ASTM, 2001). 237 EM, TS, and E were determined from the stress-strain curves, estimated from force-238 distance data obtained for the different films (2.5 cm wide and 5 cm long). Equilibrated 239 samples were mounted in the film-extension grips of the testing machine and stretched 240 at 50 mm min⁻¹ until breaking. The relative humidity of the environment was held 241 242 constant, at approximately 53% during the tests, which were performed at 25 °C. At least ten replicates were obtained from each sample. 243

244

245 <u>2.3.10. Film solubility and bonded citric acid</u>

Film solubility was determined by keeping the sample in bidistilled water at a film: 246 water ratio of 1:10, for 48 h. Three replicates were made for each formulation. After 247 48h, the film samples were transferred to a convection oven (J.P. Selecta, S.A., 248 Barcelona, Spain) for 24 h at 60 °C to remove the free water and afterwards transferred 249 to a desiccator with P₂O₅ at 25 °C for 2 weeks to complete film drying. Film water 250 solubility was estimated from its initial and final weights. The water solution was used 251 to determine the bonded citric acid in the film. Free citric acid was assumed to dissolve 252 in the aqueous phase and was determined by titration of an aliquot of the solution with 253

NaOH (0.1 N), using phenolphthalein as indicator. Three replicates were considered foreach formulation.

256

257 <u>2.3.11. Thermal properties</u>

A Differential Scanning Calorimeter (DSC 1 Star^e System, Mettler-Toledo Inc., 258 Switzerland) was used to analyze the thermal properties. Weighted amounts of samples 259 were placed into aluminum pans and sealed and drilled to promote the bonded moisture 260 loss during heating. The curves were obtained using a double scan. First, a scan from 0 261 °C to 160 °C at 50 °C / min was used where the bonded water in the film was 262 eliminated. Then the temperature was lowered to 0 °C at the same speed, and finally 263 heated to 160 °C at 20 °C / min (in this scan, starch glass transition was analyzed). The 264 initial and final weights of the pans were registered to assess water loss during the first 265 266 heating.

267

268 <u>2.3.12. Statistical analysis</u>

Statgraphics Plus for Windows 5.1 (Manugistics Corp., Rockville, MD) was used to carry out statistical analyses of data through an analysis of variance (ANOVA). Fisher's least significant difference (LSD) was used at the 95% confidence level.

272

273 **3. RESULTS**

3.1. Film thickness, water solubility and bonded citric acid.

275 Constant compression molding conditions were maintained during processing in order 276 to submit all the formulations to a similar thermomechanical treatment. In agreement 277 with the different composition, the differing response of the samples to the same 278 treatment can be estimated by the film thickness. The values of this parameter obtained

for every formulation are shown in Table 1. As can be observed, the film thickness 279 decreases when HPMC was incorporated into the film (from 268 µm to 204 µm). This 280 phenomenon is related with the increase in the blend flowability when HPMC is present 281 in the blend, which is probably related with the decrease in the glass transition of the 282 blend commented on below. The addition of citric acid also contributed to the decrease 283 in the film thickness, thus indicating the promotion of the blend's flowability. Due to its 284 cross-linking effect, citric acid has not only been reported to be a compatibilizer of 285 biopolymers (Reddy & Yang, 2010; Olivatto, Grossmann, Yamashita, Eiras & Pessan, 286 2012; Menzel, Olsson, Plivelic, Andersson, Johansson, Kuktaite, Järnström & Koch, 287 288 2013) but also a plasticizer in its free form (Ghanbarzadeh et al., 2011). Thus, this organic acid can have a relevant impact on the rheological behaviour of blends during 289 compression, which affects the final film thickness. 290

291 Table 1 also shows the solubility of the studied films in water at initial time. Values at final time (5 weeks) were not included due to the fact that no significant differences 292 293 were found with respect to the initial values. The results show that the addition of citric acid is a key factor in terms of the integrity of films submitted to water action. Films 294 containing citric acid showed higher solubility (0.31-0.35g/g) than citric acid-free films 295 (0.15-0.19g/g). These results seem contradictory since the cross-linking activity of citric 296 acid is related with an increase in the hydrophobicity as a result of the formation of ester 297 groups. Nevertheless, the addition of citric acid is also related with a decrease in the pH 298 values, which may give rise to a partial hydrolysis of glucosidic chains (Olsson, 299 Menzel, Johansson, Andersson, Koch & Järnström, 2013). In this way, the values of 300 bonded citric acid in films at 5 weeks of storage time (Table 1) are relevant since an 301 important amount of citric acid remains free to contribute to the pH decrease. The 302 contents of bonded citric acid ranged from 80 % (SG-H20-CA) to 89 % (SG-H10-CA) 303

with respect to the total amount present in the film, there being no significant differences (p>0.05) between samples. This indicates that this component partially reacts with the –OH groups of the polymer chains, although about 15 % of the added amount is free in the matrix and could act as plasticizer.

308

309 **3.2. Film microstructure**

Figures 1a and b show SEM micrographs of the cross sections of films, containing 310 (Figure 1b) or not (Figure 1a) citric acid, conditioned at 25 °C and 53 % RH for 1 311 (initial time) or 5 weeks (final time). At the initial time, the control formulations (SGi 312 313 and SG-CAi) exhibited a homogeneous structure with some cracks which are related with the more brittle nature of this formulation under the observation conditions. The 314 low water content and the electron beam in the microscopy chamber provoked the 315 316 formation of these microcracks, as observed previously for other starch films (Jiménez, Fabra, Talens & Chiralt, 2012b). The addition of HPMC gave rise to a two-phase 317 318 structure in which this polysaccharide constitutes the dispersed phase embedded in a 319 starch continuous phase, which can be observed both at initial and final storage times. The incompatibility of HPMC and starch has previously been observed in films 320 obtained by casting (Jiménez et al., 2012a). Phase separation has also been reported in 321 other polysaccharide blends such as potato maltodextrin in admixture with locust bean 322 gum, gum arabic and carboxymethyl cellulose, and starch-chitosan blend films 323 (Annable, Fitton, Harris, Philips, & Williams, 1994; Mathew & Abraham, 2008). The 324 different behaviour of continuous and dispersed phases in response to cryofracture is 325 remarkable. Whereas a very hard, rigid matrix can be deduced for the starch continuous 326 phase, HPMC particles can be inferred to be more rubbery and soft in nature, and, in 327 some cases, they appeared greatly deformable (sample SG-H20-CAf). 328

Citric acid addition did not contribute to avoid the formation of microcracks as can be observed in Figure 1b (SG-CAi), despite its plasticizing effect on the matrix (Yu, Wang & Ma, 2005) as deduced from the film thickness values. In HPMC-containing films, citric acid addition did not significantly affect their microstructural appearance in comparison with acid-free films and the HPMC dispersed phase was also observed in films. Nevertheless, a small increase in the polymer miscibility could be promoted, without notably affecting the visible film microstructure.

The effect of storage time on the film microstructure is also shown in Figure 1. Starch-336 glycerol films, containing or not citric acid (SGf, SG-Caf), show the extensive 337 formation of crystalline zones, as revealed by the irregular, layered fracture surface, 338 which point to the growth of the crystalline regions. This was especially notable for CA-339 free starch films whereas wider amorphous regions are still observable for starch films 340 341 containing CA. In this case, the advance of the crystalline front from the film surface to the inner part of the film can be observed, probably due to the easier water uptake from 342 343 the environment and the subsequent increase in the molecular mobility. The greater advance of these crystalline structures in citric acid-free films suggests that, despite its 344 apparent plasticizing effect, this organic acid contributes to partially inhibit starch 345 recrystallization as mentioned by other authors (Shi, Zhang, Liu, Han, Zhang, Chen & 346 Tian, 2007). The possible starch depolymerization provoked by acid hydrolysis could 347 also affect the crystallization advance. 348

In HPMC-containing films, crystalline regions are not observed to the same extent as in starch films and, although HPMC appears in a dispersed phase, its partial miscibility in starch matrix may also contribute to inhibit starch crystallization as observed by Jiménez *et al.* (2012a) for HPMC-corn starch films obtained by casting.

The peak force quantitative nanomechanical mapping AFM-based method is a good tool 353 354 with which to analyse the nanostructure of biopolymer based films. This tool allows us to measure the Young modulus of the film at each point on its surface. Figure 2 shows 355 the results obtained for studied films stored for 1 week and 5 weeks under controlled 356 conditions. Raw data were converted into 2D images and their scale is expressed as 357 DMT modulus. At initial time, films show a more homogeneous Young's modulus (up 358 to 3.5 GPa), since no drastic changes are observed in the surface maps. Citric acid 359 addition implied an increase in the surface modulus in agreement with the cross-linking 360 effect, which is less marked in films containing HPMC. Likewise, the modulus values 361 significantly increased with storage time (up to 15 GPa in HPMC-free films with citric 362 acid), in part due to the progress of recrystallization phenomena. In HPMC-free 363 samples, a greater increase was observed in line with a greater ratio of crystallinity, as 364 observed by SEM. This increase was especially marked when these samples contained 365 citric acid (SG-CAf), probably due to the combined effect of the cross-linking, which 366 367 could progress throughout time. In samples with HPMC, more heterogeneous values of surface modulus were obtained, probably due to the fact that crystal growth was 368 inhibited in areas near to HPMC zones. 369

370

371 **3.3. X-ray diffraction**

X-ray diffraction patterns obtained for both films stored for 1 week and those aged for 5 weeks are presented in Figure 3. Obtained patterns correspond with the formation of Vtype structures, resulting from the formation of complexes of helical amylose forms with substances such as aliphatic fatty acids, surfactants, emulsifiers, alcohols, glycerol or dimethyl sulfoxide (Famá, Rojas, Goyanes & Gerschenson, 2005). This type of conformation may be formed when endogenous lipids form complexes within the amylose helices (Gelders, Vanderstukken, Goesaert, & Delcour, 2004). These patterns have previously been observed by other authors for starch or amylose with peaks at 20 ~7, 14 and 20° (Famá *et al.*, 2005; Chen, Kuo & Lai, 2009; Lesmes, Cohen, Shener & Shimoni, 2009). Nevertheless, the addition of citric acid or HPMC to the starch films promoted the formation of polymorphs since the intensity of peaks at 20 7° and 21° is enhanced, whereas the intensity at 20 20° decreased in most of the samples stored for 1 week.

In general, the intensity of the peaks increased for stored samples thus indicating the growth in the crystal size, which was especially marked for control film (SG), as observed by SEM (Figure 1). Nevertheless, most of the crystalline regions for the rest of the films seem to be formed during the film drying step, when the molecular mobility is still high (Rindlav-Westling, Stading, Hermansson, & Gatenholm, 1998; Standing, Rindlav-Westling, & Gatenholm, 2001).

When citric acid was added, the surface modulus obtained by peak force quantitative 391 nanomechanical mapping significantly increased, as mentioned above. Nevertheless, 392 393 this change is not only attributable to a greater increase in crystallinity, as deduced from 394 X-R diffraction patterns at initial and final storage times. So, the cross-linking progress or rearrangement of crystals and components throughout storage can be inferred for this 395 sample. In this sense, Reddy & Yang (2010) suggested that some of the amorphous 396 397 regions of citric-acid cross-linked starch films may be better oriented after cross-linking, thus affecting the film mechanical behaviour. In this sense, SG-CA film presented a 398 sharp peak at $2\theta 21^\circ$ at initial time whose intensity decreased with storage, whereas the 399 intensity of the $2\theta 20^{\circ}$ peaks increased. This confirms the reorganization of components 400 401 and the final formation of other polymorph crystals.

Regarding the effect of HPMC addition, it seems that this component is able to limit 402 403 the starch recrystallization, since no significant changes in intensity are observed in XR diffraction spectra after 5 storage weeks. Nevertheless, as observed for SG-CA film, the 404 relative intensity of some peaks increased or decreased due to the molecular 405 rearrangement and the formation of other polymorphic structures closer to that of starch 406 films. Although HPMC is a totally amorphous polymer (Cai, Xu, Wang, Liu, Yang, & 407 Zhang, 2011; Jiménez et al., 2012a), starch films containing HPMC were 408 semicrystalline, as observed in Figure 3. Jiménez et al. (2012a) obtained starch-HPMC 409 films and analysed, by wide angle X-ray diffraction, their crystallinity. This was lower 410 as the HPMC content increased, the films being almost totally amorphous when the 411 HPMC content was 50 %. 412

Figure 4 shows the X-ray diffraction pattern of pure citric acid in which the main peaks are at $20 \, 14^\circ$, 17° , 19° , 24° , 26° and 29° . These are not found in the obtained films, which indicate that no crystalline citric acid is formed during film drying, even when it is nonbonded to the polymers. Similar results are obtained by (Shi *et al.*, 2007), which point to its dispersion in the polymeric matrix at molecular level.

418

419 **3.4. Glass transition of films**

DSC analysis of the films allows us to know the possible changes in the glass transition of components due to their interactions in the matrix. In principle, two glass transitions are expected according to the two phases (continuous-starch and dispersed-HPMC phases) observed by SEM. Different authors have also reported the presence of two different glass transitions due to the phase separation of plasticizer at high water activity, where water-polymer interactions predominate over plasticizer-polymer ones (Debeaufort & Voilley, 1997; Jiménez, Fabra, Talens & Chiralt, 2013). Glass transition

values of dry films are shown in Table 1, together with the value of HPMC with the 427 428 same ratio of glycerol as that present in the films. Figure 5 shows the obtained thermograms for the different samples in the range of glass transitions. The value for 429 HPMC-glycerol blends was slightly lower than that obtained for starch-glycerol films 430 (113 compared to 125 °C at the midpoint). In the blend films, only one glass transition 431 was clearly observed, which was attributed to the starch phase which represents the 432 greatest proportion of the film. The relatively low ratio of HPMC in the film makes the 433 observation of its glass transition difficult. Nevertheless, the Tg value of the starch 434 phase changed when citric acid or HPMC were added to the film. Citric acid 435 incorporation supposed a decrease of about 5 °C in Tg, which can be attributed to the 436 plasticizing effect of the free citric acid in the matrix and/or to the degree of starch 437 depolymerization provoked by citric acid, as deduced from the film solubility values, 438 439 which reduces the overall molecular weight of the polymers. Different authors (Menzel, Olsson, Plivelic, Andersson, Johansson, Kuktaite, Järnström & Koch, 2013) report this 440 441 effect of citric acid in starch systems when it was added as a cross-linking agent. 442 Although an anti-plasticizing effect could be expected from cross-linking due to the associated decrease in the molecular mobility (Yu, Wang & Ma, 2005), the overlapped 443 hydrolysis effect masks it. 444

When HPMC was incorporated in the film without citric acid, a decrease in the Tg of about 10 °C was also observed, which indicates that a partial miscibility of both polymers occurs in the blend with a Tg value nearer to that of HPMC. When both, citric acid and HPMC, are present in the film, Tg value ranged between 100-105 °C, reflecting both the plasticizing effect of citric acid and the mixing effect of HPMC. So, phase separation between starch and HPMC was not total as deduced from these results and the continuous phase is a starch-rich phase containing glycerol, free citric acid and

HPMC molecules. Both free citric acid and glycerol could also be present in the HPMC
dispersed phase since their chemical structures are compatible.

The decrease in the Tg provoked by both components explains the higher flowability of the blends shown during compression-molding, commented on above.

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457 **3.5. Mechanical properties**

Figure 6 shows the stress-Hencky strain curves obtained for the films studied, 458 conditioned at 25 °C and 53 % RH for 1 week. The SG film was the most resistant and 459 flexible, while the addition of HPMC brought about a slight reduction to the film 460 461 resistance to break and to the elongation at break: the higher the HPMC content, the less resistant the film. This can be attributed to the presence of a dispersed phase in the 462 starch matrix (as observed in Figure 1) which leads to a loss in the cohesion forces in 463 464 the film. In this sense, a greater dispersed phase ratio lowers the cohesion forces and then the film resistance to break. 465

466 The addition of citric acid had a great impact on the film stretchability, since elongation at break was reduced by up to 60 % (from 28 % to 11 %). The shortening of the films 467 caused by the citric acid is coherent with the cross-linking effect, since the slippage of 468 polymer chains during the tensile test is limited by their strong inter-chain bonds. 469 Nevertheless, the elastic modulus only slightly increases after the addition of citric acid, 470 this increase only being significant in the sample with 20 % HPMC. Similar behaviour 471 was observed for the tensile strength at break. These results seem to indicate that inter-472 chain bonding did not progress enough, as observed by other authors for higher contents 473 of citric acid (Reddy & Yang (2010), and that HPMC chains seem to participate in the 474 cross-linking reactions, probably through the hydroxy-propyl group which can be more 475 readily available for reaction. 476

Figure 7 also shows the values of the mechanical parameters of the films after 5 storage 477 478 weeks. For every formulation, the elongation at break significantly decreases while the elastic modulus and the tensile strength increase. There are different mechanisms 479 responsible for this behaviour. On the one hand, starch tends to recrystallize over time, 480 as commented on above, which explains the observed behaviour of the formulation 481 without HPMC or citric acid (Mali, Grossmann, García, Martino & Zaritzky, 2006). 482 Apart from crystallization, the progressive aggregation of polymer chains throughout 483 time has been observed for starch films and starch dispersions (Rindlav-Westling et al., 484 1998; Funami et al., 2005; Jiménez et al., 2012a) which provokes an increase in the 485 486 matrix compactness and the subsequent changes in the tensile response. The cross linking effect of citric acid could also be extended throughout time, thus contributing to 487 the changes in the mechanical properties. In this sense, the sample with the highest 488 489 elastic modulus and lowest stretchability after 5 storage weeks is the one that contains the highest ratio of HPMC and citric acid, which also points to the fact that HPMC 490 491 chains participate in the citric acid cross-linking action. This phenomenon would be associated with the non-bonded citric acid (11-20%, according to Table 1) that remains 492 free after film formation and which is able to react with the hydroxyl groups of 493 polymers during storage 494

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496 **3.6. Barrier properties**

One of the main features to take into account when biodegradable polymers are used for packaging application is their ability to avoid mass transfer mechanisms. In this way, a good barrier against aroma, water vapour and gases is generally desired. Table 2 shows the values of water vapour, oxygen permeability and water content for films conditioned for 1 week and those aged for 5 weeks. At initial time, the water vapour permeability

values were significantly reduced by HPMC and the addition of citric acid, exhibiting 502 503 the lowest value when both citric acid and the highest HPMC ratio were present in the film. Ghanbarzadeh et al. (2011) also found that the addition of citric acid reduced 504 WVP when the concentrations ranged between 5 and 20 %. They explained this effect 505 in terms of the substitution of hydroxyl groups (-OH) by hydrophobic esters and by the 506 fact that citric acid introduced a tortuous path for water molecules to pass through the 507 films due to the cross linking effect. These authors also found that another cellulose 508 derivative (carboxymethylcellulose) was effective at reducing the WVP and related this 509 phenomenon with the fact that carboxymethylcellulose is less hydrophilic than starch 510 (Ma, Chang & Yu, 2008). Nevertheless, HPMC has been reported to produce worse 511 water vapour barriers (Jiménez et al., 2010; 2012a). Thus, the positive effect of HPMC 512 513 on the water vapour barrier of the studied films may be due to its cooperative effect on 514 the cross-linking effect, as previously commented on.

Storing the films for 5 weeks had no effect on the WVP values, regardless of the film 515 516 composition, despite the fact that a significant increase (p < 0.05) in the film moisture 517 content occurred during storage. A similar result was reported by Jiménez et al. (2012c) for starch-glycerol films. They found a significant increase in the film's moisture 518 content after 5 storage weeks, at the same time as they became more brittle, as observed 519 in the present work. In this sense, it is remarkable that the formation of crystalline 520 regions implies a gain in water content, since a great amount of water molecules are 521 bonded to the crystalline conformations (Rindlav, Hulleman, & Gatenholm, 1997). So, 522 the water gain of the films could be associated with the water bonded to the crystalline 523 regions which did not contribute to the plasticization of the amorphous matrix and 524 therefore, did not affect the barrier properties. 525

As regards oxygen permeability, SG was the least permeable film, mainly at initial time 526 527 when the equipment was not able to take measurements due to the very low quantity of oxygen molecules that passed through the film. Different studies have pointed out the 528 very good oxygen barrier properties of starch compared with other polymers (Miller & 529 Krochta, 1997; Jiménez et al., 2012ab). The addition of HPMC significantly increased 530 (p<0.05) the oxygen permeability as previously observed by Jiménez *et al.*, 2012a, 531 which coincides with the higher oxygen permeability of this polymer. Storage time did 532 not affect the oxygen barrier properties, unlike what occurred with the water vapour 533 barrier. 534

535 **3.7. Optical properties**

Optical properties are relevant when a polymeric matrix is tested as a packaging 536 material. Ghanbarzadeh et al. (2010) commented that film colour can be an important 537 538 factor in terms of the consumer acceptance of both edible and inedible films. In the same sense, Hutchings (1999) explained that the most outstanding optical properties 539 540 with which to evaluate the impact on the appearance and colour of coated products are 541 opacity and gloss. Table 3 shows the gloss values (measured at 60°) and internal transmittance values (at 450 nm) for films stored for 1 or 5 weeks at 25 °C and 53 % 542 RH. The gloss values were very low for every formulation (between 10.2 GU to 12 543 GU), regardless of the film composition and the storage time. Higher gloss values have 544 been found for both pure HPMC (Jiménez et al., 2010) and starch-glycerol films 545 (Jiménez et al., 2012c) obtained by casting. Nevertheless, for starch films blended with 546 other polymers, such as chitosan (Bonilla, Talón, Atarés, Vargas & Chiralt, 2013) or 547 HPMC (Jiménez et al., 2012a), similar gloss values are reported. Film gloss is directly 548 related with the surface topography, which can be determined by atomic force 549 microscopy. The corresponding surface roughness parameters for the obtained films are 550

shown in Table 3, where neither a different composition nor a varying storage time ledto there being any significant differences in the parameters.

Table 3 also includes the values of internal transmittance (Ti) for films after 1 and 5 553 storage weeks. High values of internal transmittance are associated with highly 554 transparent films. On the contrary, more opaque films correspond with low values of 555 internal transmittance. The Ti values ranged from 74 to 81 and were dependent on the 556 formulation, but were not significantly affected by the storage time. Considering these 557 results, all of the films can be considered quite transparent. It is remarkable that, 558 whereas the incorporation of citric acid promotes a slight increase in transparency, 559 HPMC slightly increases film opacity, in agreement with the appearance of a dispersed 560 phase which enhances light scattering. The effect of citric acid is opposite to that 561 observed by Olivatto, Grossmann, Yamashita, Eiras & Pessan (2012) for starch-PBAT 562 563 films obtained by reactive extrusion with citric acid, where a significant increase in opacity is observed. These authors related the cross-linking activity of the acid with a 564 565 higher polymeric chain compaction, which modifies the refractive index and hinders the passage of the light through the matrix. The relatively low ratio of citric acid (1 % with 566 respect to starch) in the films and the commented depolymerisation effect, which gives 567 rise to a less compact matrix, can explain the different behaviour 568

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571 **4. CONCLUSIONS**

572 Corn starch films containing HPMC (10 and 20 %, with respect to starch) obtained by 573 compression molding showed a dispersed phase of HPMC in a continuous starch-rich 574 phase with a lower glass transition than HPMC-free films. The addition of citric acid as 575 a compatibilizer also provoked a decrease in glass transition in line with a

depolymerisation effect brought about by acid hydrolysis. Both components implied a 576 577 decrease in the water vapour permeability but a slight increase in oxygen permeability. Although citric acid provoked a mild hardening effect in the films, it greatly decreased 578 extensibility pointing to a weak cross-linking effect, which seems to increase during 579 film storage to a greater extent in films with the highest ratio of HPMC. Starch 580 crystallization was slightly modified by both components which induce the formation of 581 other polymorphs mainly at initial time (1 storage week). Starch crystallization during 582 storage was inhibited by both citric acid and HPMC. A greater ratio of citric acid could 583 be interesting as a means of promoting both a more significant cross-linking effect and 584 greater HPMC compatibility with starch. 585

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