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Additional Information

1 **Behaviour of metakaolin-based geopolymers incorporating sewage**
2 **sludge ash (SSA)**

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10
11 **ABSTRACT**

12 In recent years, geopolymers have become a widely researched binding material. There are technological
13 and environmental advantages to using this type of binder instead of Portland cement. In this study,
14 binary systems of geopolymers were produced by using mixtures of metakaolin (MK), a well-known
15 aluminosilicate raw material, and a residue from sewage sludge incineration: sewage sludge ash (SSA).
16 This ash was used to partially replace the metakaolin in proportions of 0–20%. The mixtures were
17 activated with alkaline solutions and they were cured by using two different conditions: at room
18 temperature (25 °C) and in a thermal bath (65 °C). The samples were assessed by X-ray diffraction,
19 scanning electron microscopy (pastes) and compressive strength (mortars). The results from these studies
20 showed zeolite formation (faujasite) in geopolymers cured in the thermal bath, which caused a decrease in
21 the compressive strength of the alkali-activated mortars. Replacement of MK with SSA caused a lower
22 reduction in the compressive strength of mortars cured at 65 °C. However, at room temperature, similar
23 mechanical strength was observed for the MK and MK-SSA systems. These results demonstrated that
24 SSA is a suitable mineral precursor for partial replacement of MK in geopolymer production.

25
26 **KEY WORDS:** alkali-activated binder, microstructure, residue, X-ray techniques
27
28

29 **1. INTRODUCTION**

30 Geopolymers are a new class of material obtained by a chemical reaction of an aluminosilicate material
31 and a highly concentrated alkaline solution [1]. This binding material can be used as a construction
32 material due to their high strength and durability, replacing Portland cement (OPC) in concrete [2].

33

34 Metakaolin (MK) is usually used as the aluminosilicate source in geopolymers [3-5]. Previously studies
35 on metakaolin-based geopolymers have shown high compressive strength after a few hours of curing at
36 temperatures ranging from 40 to 95 °C [3]. However, research has shown that some geopolymers,
37 especially metakaolin-based ones cured at high temperatures, tend to form crystalline structures: zeolites
38 [6-9]. These crystalline phases significantly reduce the compressive strength of geopolymers, a critical
39 behaviour for building materials [2,9].

40

41 In this sense, the combination of different raw materials containing silicon and/or aluminium oxides on
42 their composition are being carried out (binary systems) in order to reduce the zeolite formation [10,11].

43 Sewage sludge ash (SSA), a waste generated in large amounts (1.7million tons per year) has been studied
44 extensively in blended Portland cements [12-14]. The first study related to the use of SSA in geopolymers
45 were reported by Yamaguchi et al. where authors used fly ash/SSA yielding the maximum flexural
46 strength (about 5.5 MPa) for mixture containing 75%SSA [15].

47

48 In this paper is presented the influence of SSA on the mechanical strength and on the crystallization
49 process (zeolite formation) of metakaolin-based geopolymers. Specimens were cured at both high-
50 temperature and 25 °C and they were assessed through compressive strength, X-ray diffraction and
51 scanning electron microscopy.

52

53 **2. MATERIALS AND METHODS**

54 **2.1 Materials and Equipment**

55

56 Metakaolin was supplied by Metacaulim do Brasil®. Sewage sludge ash was obtained from an auto-
57 combustion process of sewage sludge from São José do Rio Preto city (São Paulo-Brazil). The chemical
58 composition of MK and SSA are shown in Table 1. The mean particle diameter, d_{50} and d_{90} of MK were

59 23.90, 18.16 and 53.96 μm , respectively; and for SSA they were 20.28, 11.77 and 52.45 μm , respectively.
60 For mortar preparation, siliceous sand (Castilho city, São Paulo-Brazil) with a fineness modulus of 2.05
61 and specific gravity of 2.67 ton/m^3 was used. Sodium hydroxide (98% purity) and sodium silicate (18%
62 Na_2O , 63% SiO_2) were used for the preparation of alkaline solutions (both supplied by Dinâmica
63 Química).
64 X-ray diffraction (XRD) patterns for raw materials and geopolymeric pastes were obtained using a
65 Shimadzu XRD-6000 system. The 2θ range was 5–60° using Cu-K α radiation and a Ni filter, at a voltage
66 of 30 kV, a current intensity of 40 mA, an angle step of 0.02°, and a step time of 1.20 s/step. Scanning
67 electron microscopy (SEM) images of fractured surface pastes were obtained using a ZEISS model EVO
68 LS15. The compressive strength of mortars was measured in an EMIC Universal machine with a 200-ton
69 load limit.

70

71 Table 1 – Chemical composition of MK and SSA in percentage by mass

Oxide (%)	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Na ₂ O	K ₂ O	SO ₃	TiO ₂	Others	LOI
MK	58.39	35.47	2.71	0.01	0.30	-	1.44	-	1.51	0.07	0.10
SSA	38.28	20.72	11.27	5.51	1.91	0.70	0.73	4.18	3.73	9.25	3.72

72

73 2.2 Geopolymer preparation

74 Three different proportions of MK replacement by SSA were assessed in this study: 0% (control), 10%
75 and 20% (by mass). The $\text{H}_2\text{O}/\text{Na}_2\text{O}$ and $\text{SiO}_2/\text{Na}_2\text{O}$ molar ratios were maintained constant at 9.26 and
76 2.00, respectively. For mortars, the sand/binder ratio was 2.5 (the binder amount being the sum of the
77 masses of MK and SSA). Two different curing temperatures were applied at a relative humidity greater
78 than 95%: 25 °C (room temperature) and 65°C (using a thermal bath). The compressive strength of the
79 mortars was determined after one, three and seven days of curing. XRD studies were performed on pastes
80 after the same curing times. SEM studies were performed only after three days of curing.

81 The samples used in this paper are named as MK c - xx , where c is the curing temperature (c , R: room
82 temperature, B: thermal bath) and xx is the percentage of SSA incorporated ($xx = 0, 10$ or 20).

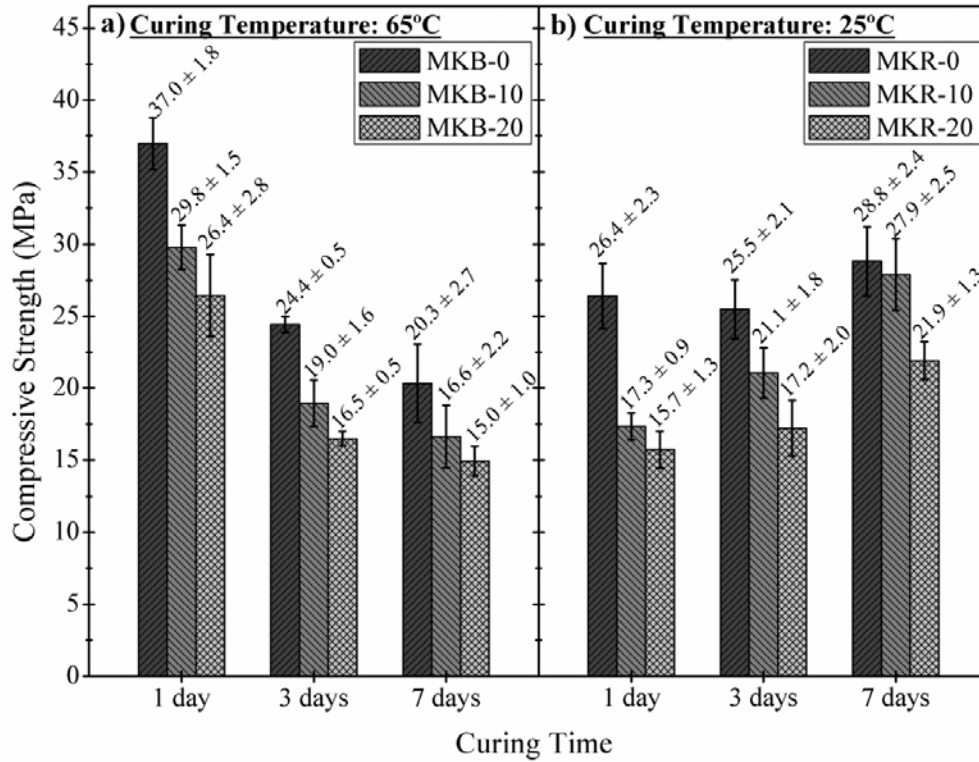
83

84 3. RESULTS AND DISCUSSION

85 The compressive strengths of the different mortars are shown in Figure 1. For mortars cured at 65 °C (Fig.
86 1a), the compressive strength of all mixtures decreased with increasing curing time. Similarly, the
87 strength of the mortars after one day of curing at 65 °C decreased with increasing replacement of MK by
88 SSA. After three days of curing at 65°C the compressive strength of the mortars decreased by 34% for
89 MKB-0, 36% for MKB-10 and 37% for MKB-20. The compressive strength of mixtures incorporating 10
90 or 20% of SSA decreased by a similar percentage as the control (MKB-0, 36%). After seven days of
91 curing, the compressive strength values and their respective percentage loss of compressive strength
92 compared to the values after three days of curing were 20.3 MPa (16.8%), 16.6 MPa (12.6%) and 15.0
93 MPa (9.1%) for MKB-0, MKB-10 and MKB-20, respectively. These results show that the relative
94 decrease in compressive strength with curing time is lower in mortars containing up to 20% SSA than in
95 the control sample. These results suggest that the use of SSA in the production of metakaolin-based
96 geopolymers stabilizes the compressive strength in mortars prepared with long curing times.

97 Mortars cured at room temperature (Fig. 1b) behaved differently to samples cured at 65 °C. At room
98 temperature, mortars did not show a decrease in compressive strength with curing time. After one day of
99 curing at room temperature, the strength decreased when SSA content was increased, similar to the
100 situation for mortars cured at 65°C. After three and seven days of curing, the compressive strength of
101 MKR-0 increased slightly, whereas samples incorporating SSA presented an important strength gain.
102 After seven days of curing at room temperature, the MKR-10 sample achieved a similar strength to MKR-
103 0 (27.9 and 28.8 MPa, respectively). This result suggests that the use of SSA in metakaolin-based
104 geopolymers may be an interesting possibility.

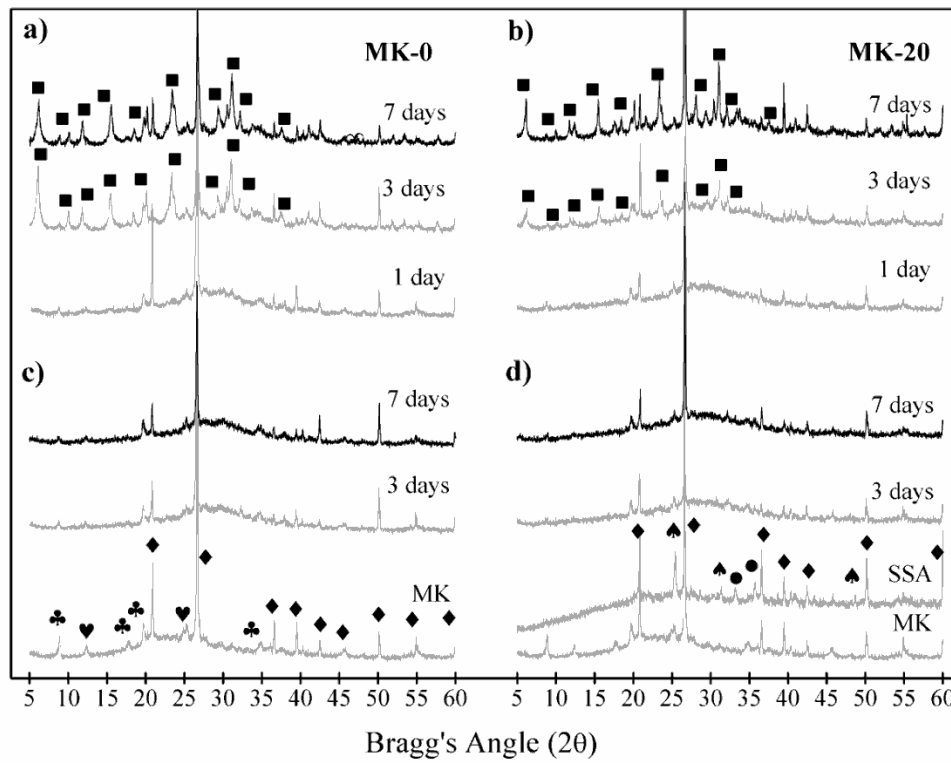
105 XRD studies were carried out on MKB-0, MKB-20, MKR-0 and MKR-20 pastes in order to examine the
106 formation of crystalline phases, both at 25°C and 65°C (Figure 2). The raw materials MK and SSA show a
107 baseline deviation in the range 16–32° and 18–32°, respectively, which is characteristic of the presence of
108 an amorphous phase. Quartz (SiO_2 , PDFcard#331161), kaolinite ($\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4$, PDFcard#140164) and
109 muscovite ($\text{KA}_3\text{Si}_3\text{O}_{10}(\text{OH})_2$, PDFcard#210993) were found in MK, and quartz, anhydrite (CaSO_4 ,
110 PDFcard#371496), anorthite ($\text{CaAl}_2\text{Si}_2\text{O}_8$, PDFcard#411486) and hematite (Fe_2O_3 , PDFcard#130534)
111 were found in SSA.



112

113

Figure 1 – Compressive strength of mortars: a) cured at 65°C; and b) cured at 25°C



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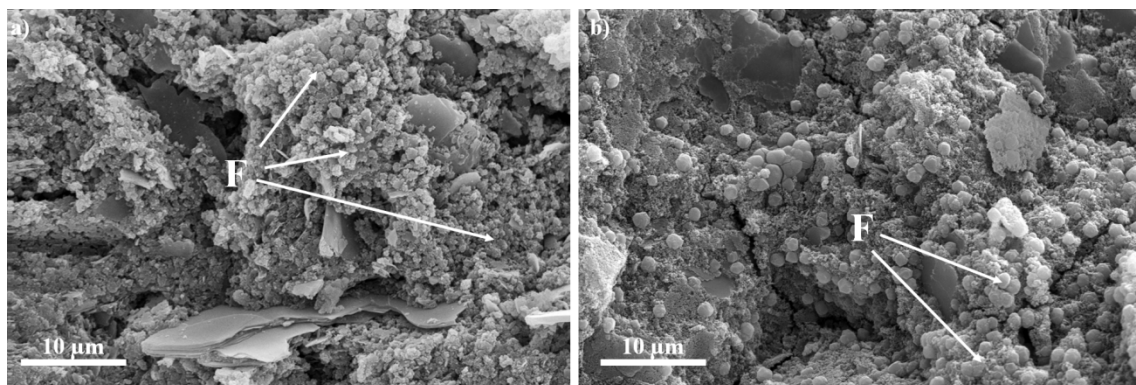
Figure 2 – XRD patterns for MK/SSA pastes: a) MKB-0; b) MKB-20; c) MKR-0; d) MKR-20 (Key: ♦:

116

Quartz; ♥: Kaolinite; ♣: Muscovite; ♠: Anhydrite; ●: Hematite; ■: Faujasite)

117 For the geopolymeric pastes, all samples presented a baseline deviation line between 16 and 40°, which
118 can be attributed to the amorphous phase of the geopolymeric gels. This shift of the baseline to higher 2θ
119 values compared to the MK and SSA amorphous phases due the geopolymerisation reaction has also been
120 observed in others studies [16]. For pastes cured at 65°C, faujasite ($\text{Na}_2\text{Al}_2\text{Si}_4\text{O}_{12}\cdot 8\text{H}_2\text{O}$,
121 PDFcard#391380) formation was observed after three days of curing (Fig. 2a and 2b). However, the
122 presence of SSA influences the zeolite formation, since a lower zeolite peak intensity is observed after
123 three days of curing at 65°C compared to MKB-0. No signals attributed to zeolites were distinguished by
124 XRD analyses on pastes cured at room temperature, either in MKR-0 (Fig. 2c) or MKR-20 (Fig. 2d),
125 whatever the curing time (three and seven days).
126 Both geopolymeric gel and zeolite formation are directly related to the reactivity of the raw materials and
127 to the curing temperature [2,17]. For high alkaline environment, high curing-temperatures favours the
128 crystallization of aluminosilicate gels forming zeolite-type structures and, according to Bosnar et al., the
129 crystallization process is sharply reduced with the increase on the $\text{SiO}_2/\text{H}_2\text{O}$ [17]. In this paper, MK
130 presented higher reactivity than SSA, so it was expected that geopolymers with higher amounts of MK
131 would present more intense zeolite formation and, consequently, greater reduction in compressive
132 strength. It is due to the microporous-crystalline structure based on 3D-cage system of zeolites that
133 reduces the compressive strength of mortars when compared to the amorphous structure based on 3D-
134 network of aluminate and silicate tetrahedral of geopolymers [2,18].

135



136

137 Figure 3 – SEM micrographs of geopolymer fractured surfaces: a) MKB-0; b) MKB-20 (Key: F-
138 faujasite)

139

140 Faujasite was also observed in SEM on fractured samples of MKB-0 and MKB-20 after three days of
141 curing (Fig.3). Rounded crystalline particles of 2–4 μm size were formed. Since the raw material mainly
142 contains metakaolin, faujasite was formed in both pastes.

143 **4. CONCLUSION**

144

145 Metakaolin-based geopolymers with partial replacement of MK with SSA were studied. XRD analysis
146 showed that geopolymers cured at 65 °C produced faujasite after three days of curing. This zeolite
147 formation caused a decrease in compressive strength with the curing age at 65 °C. The addition of SSA
148 (up to 20%) to the mixture resulted in a smaller loss of compressive strength in mortars cured at 65°C
149 when compared to the control without SSA. In addition, in samples cured at 25°C, those containing 10%
150 SSA presented similar compressive strength as the control mortar after seven days of curing. Thus partial
151 replacement of metakaolin with SSA showed advantages in both curing conditions.

152

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