

Universidad Politécnica de Valencia

Escuela Técnica Superior de Ingeniería de Diseño

· Diseño y simulación de un convertidor
DC/DC para alimentación de un sistema de
iluminación mediante LED ·

ANEXOS

Trabajo Fin de Grado

David Ramón Marco

Dirigido por:

Fernando Ibáñez Escobar

Grado en Ingeniería Electrónica Industrial y Automática

Elección del programa de cálculo

Se elige Mathcad como programa de cálculo ya que permite modificar valores y fórmulas de forma instantánea agilizando así el proceso previo a la simulación del sistema. Además, permite graficar las diferentes funciones de transferencia y diagramas de Bode correspondientes.

Los cálculos realizados son los siguientes:

- Especificaciones del diseño:

$$V_i := 30V \quad V_o := 24V \quad P := 30W \quad f_s := 50kHz$$

$$R_s := 20\Omega \quad L_s := 600\mu H \quad C_s := 2200\mu F \quad R_c := 52m\Omega$$

$$V_{ref} := 2.5V$$

$$\text{Modulador:} \quad V_m := 3V \quad F_m := \frac{1}{V_m} \quad F_m = 0.333 \frac{1}{V}$$

- Cálculo Ciclo de Trabajo - Cálculo de la RCarga inicial

$$D := \frac{V_o}{V_i} = 0.8 \quad R_{carga} := \frac{V_o^2}{P} = 19.2 \Omega$$

- Cálculo del valor de la Bobina

$$L_{prox} := (1 - D) \frac{V_o}{2f_s \cdot 0.1A} = 4.8 \times 10^{-4} H \quad L_{proxp} := L_{prox} \cdot 0.25 = 1.2 \times 10^{-4} H$$

$$L_{final} := L_{prox} + L_{proxp} = 6 \times 10^{-4} H$$

- Cálculo del valor del Condensador

$$C_{prox} := V_o \cdot \frac{(1 - D)}{8 \cdot L \cdot f_s^2 \cdot 0.05V} = 8 \times 10^{-6} F \quad \Delta V_o := \frac{20}{100 \cdot 4} = 0.05$$

$$C_{final} := 2200\mu F$$

- Intensidades (I_o, I_i)

- Potencias (P_o, P_{in})

$$I_o := \frac{V_o}{R_{carga}} = 1.25 \text{ A} \quad I_i := D \cdot I_o = 1 \text{ A} \quad P_{in} := V_i \cdot I_i = 30 \text{ W} \quad P_o := \frac{V_o^2}{R_{carga}} = 30 \text{ W}$$

- Rendimiento

$$P_{out} := I_o \cdot V_o = 30 \text{ W}$$

$$\eta := \frac{P_o}{P_{in}} = 1$$

-Modelización de la Etapa de potencia: FDT

$$I_{L_riz} := \frac{V_i - V_o}{L} \cdot D \cdot T_s \quad I_{L_riz} = 0.16 \cdot \text{A} \quad \frac{I_{L_riz}}{I_o} = 12.8\%$$

$$I_{L_riz} := \frac{(V_i - V_o) \cdot D}{L \cdot f_s} = 0.16 \text{ A} \quad \frac{I_{L_riz}}{8 \cdot f_s \cdot C} = 0.182 \cdot \text{mV} \quad I_{L_riz} \cdot R_c = 8.32 \cdot \text{mV}$$

$$V_{o_riz_ESR} := R_c \cdot I_{L_riz} \quad V_{o_riz_ESR} = 8.32 \cdot \text{mV} \quad \frac{V_{o_riz_ESR}}{V_o} = 0.035\%$$

$$V_{o_riz_C} := \frac{1}{8 \cdot C} \cdot I_{L_riz} \cdot T_s \quad V_{o_riz_C} = 0.182 \cdot \text{mV}$$

$$\omega_z := \frac{1}{R_c \cdot C} \quad f_z := \frac{\omega_z}{2\pi} \quad f_z = 1.391 \cdot \text{kHz}$$

$$f_z := \frac{1}{2\pi R_c \cdot C} = 7.958 \text{ kHz} \quad \omega_z := \frac{1}{R_c \cdot C} = 8.741 \times 10^3 \cdot \frac{\text{rad}}{\text{s}}$$

$$\omega_n := \frac{1}{\sqrt{L \cdot C}} \quad f_n := \frac{\omega_n}{2\pi} \quad f_n = 0.139 \cdot \text{kHz}$$

$$f_n := \frac{1}{2\pi \sqrt{L \cdot C}} = 1.592 \text{ kHz} \quad \omega_n = 870.388 \cdot \frac{\text{rad}}{\text{s}}$$

$$Q := \frac{\omega_n}{\frac{1}{R \cdot C} + \frac{R_c}{L}} \quad Q = 7.956$$

Diseño del lazo de corriente

Para hallar el valor de A_i , primero hay que saber el valor de G_{id} que se halla de la siguiente forma: Consultar si es correcto.

Valor de G_{id}

$$G_{id}(\omega) := V_i \cdot \frac{1 + (R + R_c) \cdot C \cdot j \cdot \omega}{R + (R \cdot R_c \cdot C + L) \cdot j \cdot \omega - (R + R_c) \cdot L \cdot C \cdot \omega^2} \quad R \gg R_c$$

$$G_{id}(\omega) := V_i \cdot \frac{1 + R \cdot C \cdot j \cdot \omega}{R + (R \cdot R_c \cdot C + L) \cdot j \cdot \omega - R \cdot L \cdot C \cdot \omega^2}$$

$$G_{id}(\omega) := \frac{V_i}{R} \cdot \frac{1 + R \cdot C \cdot j \cdot \omega}{1 + \frac{R \cdot R_c \cdot C + L}{R} \cdot j \cdot \omega - L \cdot C \cdot \omega^2}$$

$$\omega_n := \frac{1}{\sqrt{L \cdot C}} \quad \omega_n = 870.388 \cdot \frac{\text{rad}}{\text{s}} \quad +$$

$$\omega_z := \frac{1}{R \cdot C} \quad \omega_z = 22.727 \cdot \frac{\text{rad}}{\text{s}}$$

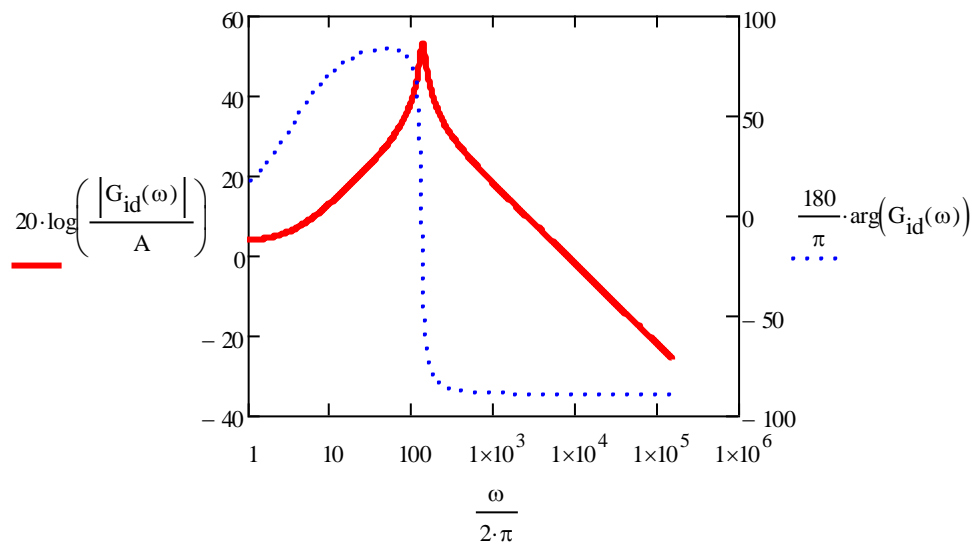
$$\zeta := \frac{1}{2 \cdot \omega_n} \cdot \left(\frac{1}{R \cdot C} + \frac{R_c}{L} \right) \quad \zeta = \frac{\sqrt{L \cdot C}}{2} \cdot \left(\frac{1}{R \cdot C} + \frac{R_c}{L} \right) \quad \zeta = 0.063$$

$$Q := \frac{\sqrt{L \cdot C}}{\frac{L}{R} + R_c \cdot C} \quad Q = 7.956$$

$$\frac{R \cdot r \cdot C + L}{R} := 2 \zeta \cdot \omega_n \cdot L \cdot C$$

$$G_{id}(\omega) := \frac{V_i}{R} \cdot \frac{1 + j \cdot \frac{\omega}{\omega_z}}{1 + j \cdot \frac{1}{Q} \cdot \frac{\omega}{\omega_n} - \left(\frac{\omega}{\omega_n} \right)^2}$$

$$G_{id}(j\omega) = \frac{V_i}{R_L} \cdot \frac{1 + j \cdot \frac{\omega}{\omega_z}}{1 + j \cdot \frac{1}{Q} \cdot \frac{\omega}{\omega_n} - \left(\frac{\omega}{\omega_n} \right)^2}$$



Hallamos también los valores de R_i y de F_m para completar la ecuación de T_i

Valor de R_i

$$R_i := 1\Omega$$

Valor de F_m

$$F_m := \frac{1}{V_m} \quad F_m = 0.333 \frac{1}{V}$$

+

Por último, se saca el valor de A_i con el método del factor K

1. Diseño del controlador por el método del Factor K :

$$10\% f_s < f_{ci} < 20\% f_s \quad f_{ci} > 10 f_n$$

$$40^\circ < MF_i < 70^\circ$$

$$MG > 10^\circ$$

$$f_s = 50\text{-kHz} \quad \omega_s := 2\pi f_s \quad \omega_s = 3.142 \times 10^5 \frac{\text{rad}}{\text{s}}$$

$$10\% \cdot f_s = 5\text{-kHz} < f_{ci} < 20\% \cdot f_s = 10\text{-kHz}$$

$$f_n := \frac{\omega_n}{2\pi} \quad f_n = 138.527\text{-Hz} \quad 10 \cdot f_n = 1.385\text{-kHz} < f_c$$

Valores de diseño

$$f_{ci} := 7\text{kHz}$$

$$MF_i := 70^\circ$$

$$\omega_{ci} := 2\pi f_{ci}$$

$$-\arg(G_{id}(\omega_{ci})) = 89.887^\circ$$

$$|G_{id}(\omega_{ci})| = 1.137 A$$

$$\text{Compensador tipo 2: } A_i(j\omega) = \frac{\omega_{p0c}}{j \cdot \omega} \cdot \frac{1 + j \cdot \frac{\omega}{\omega_{zc}}}{1 + j \cdot \frac{\omega}{\omega_{pc}}}$$

$$\text{Paso 1) } \arg(G_{id}(\omega_{ci})) - 90^\circ + \text{AUFA}_i = -180^\circ + \text{MFi}$$

$$\text{AUFA} = \text{MFi} - \arg(G_{id}(\omega_{ci})) - 90^\circ$$

$$\text{AUFA}_i := (\text{MFi} - \arg(G_{id}(\omega_{ci})) - 90^\circ) \quad \text{AUFA}_i = 69.887^\circ$$

$$\text{Paso 2) } K_i := \tan\left(45^\circ + \frac{\text{AUFA}_i}{2}\right) \quad K_i = 5.639 \quad K_i = \tan\left(45^\circ + \frac{\text{AUFA}_i}{2}\right)$$

$$\omega_{zci} := \frac{\omega_{ci}}{K_i}$$

$$\omega_{zci} = 7.8 \cdot \frac{\text{krad}}{\text{s}}$$

$$\omega_{zci} = \frac{\omega_{ci}}{K_i}$$

$$\omega_{pci} := K_i \cdot \omega_{ci}$$

$$\omega_{pci} = 248.006 \cdot \frac{\text{krad}}{\text{s}}$$

$$\omega_{pci} = K_i \cdot \omega_{ci}$$

$$\text{Paso 3) } \text{Ganancia del regulador } \omega_{p0ci}$$

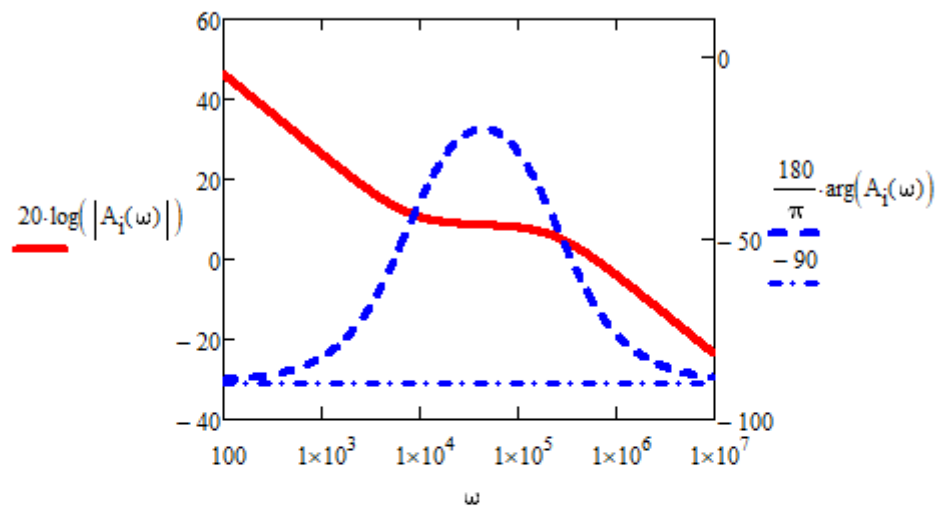
$$T_i(\omega) = G_{id}(\omega) \cdot A_i(\omega) \cdot F_m \cdot R_i \quad |T_i(\omega_{ci})| = 1$$

$$|G_{id}(\omega_{ci})| \cdot \left| \frac{\omega_{p0ci}}{j \cdot \omega_{ci}} \cdot \frac{\left(1 + j \cdot \frac{\omega_{ci}}{\omega_{zc}}\right)}{\left(1 + j \cdot \frac{\omega_{ci}}{\omega_{pc}}\right)} \right| \cdot F_m \cdot R_i = 1$$

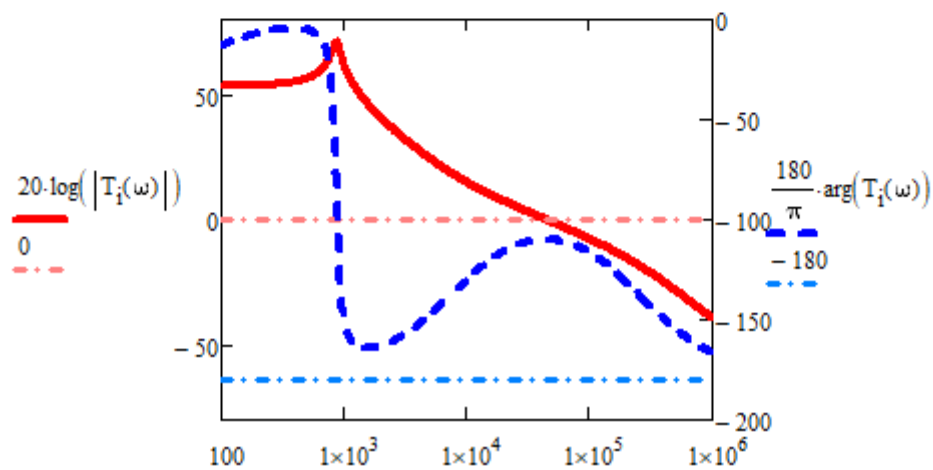
$$\omega_{p0ci} := \frac{\omega_{ci}}{F_m \cdot R_i \cdot |G_{id}(\omega_{ci})|} \cdot \frac{\left| \left(1 + j \cdot \frac{\omega_{ci}}{\omega_{pci}}\right) \right|}{\left| \left(1 + j \cdot \frac{\omega_{ci}}{\omega_{zci}}\right) \right|}$$

$$\omega_{p0ci} = 20.576 \cdot \frac{\text{krad}}{\text{s}}$$

$$A_i(\omega) := \frac{\omega_{p0ci}}{j \cdot \omega} \cdot \frac{\left(1 + j \cdot \frac{\omega}{\omega_{zci}}\right)}{\left(1 + j \cdot \frac{\omega}{\omega_{pci}}\right)}$$



$$T_i(\omega) := G_{id}(\omega) \cdot A_i(\omega) \cdot F_m \cdot R_i$$



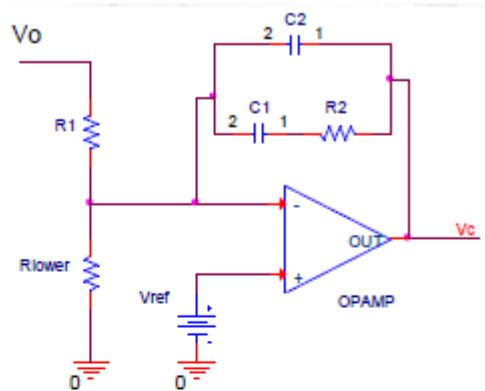
Dado $\omega_{max} := 1 \frac{\text{krad}}{\text{s}}$ $|T_i(\omega_c)| = 1$

$$\omega_{ci} := \text{Find}(\omega_c)$$

$$f_{ci} := \frac{\omega_{ci}}{2\pi} = 7 \text{ kHz}$$

$$MF_i := \arg(T_i(\omega_{ci})) + 180^\circ = 70^\circ$$

Regulador tipo 2 con 1 AO:



$$\omega_{zc} = 20.253 \cdot \frac{\text{krad}}{\text{s}}$$

$$\omega_{pc} = 95.513 \cdot \frac{\text{krad}}{\text{s}}$$

$$\omega_{p0c} = 464.042 \cdot \frac{\text{krad}}{\text{s}}$$

$$(C_2 < C_1) \quad R_1 := 10\text{k}\Omega$$

$$V_{\text{ref}} = 2.5\text{V}$$

$$\omega_{p0c} := \frac{1}{R_1 \cdot (C_1 + C_2)}$$

$$C_1 := \frac{1}{R_1 \cdot \omega_{p0c}} = 4.86 \cdot \text{nF}$$

$$\omega_{zci} := \frac{1}{C_1 \cdot R_2}$$

$$R_2 := \frac{1}{C_1 \cdot (\omega_{zci})} = 26.379 \cdot \text{k}\Omega$$

$$\omega_{p0c} := \frac{(C_1 + C_2)}{R_2 \cdot C_1 \cdot C_2}$$

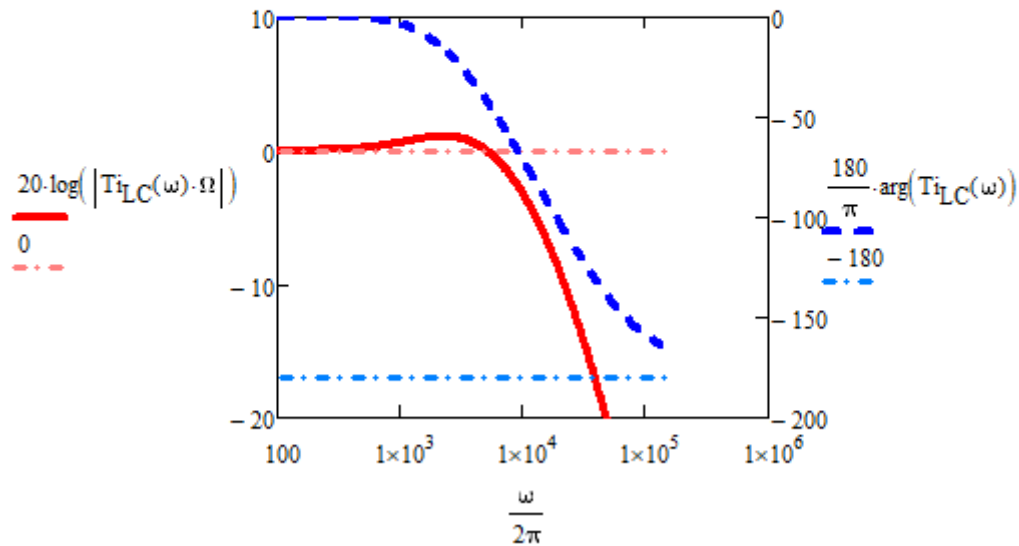
$$C_2 := \frac{\omega_{zci}}{\omega_{p0c} \cdot \omega_{p0c} \cdot R_1} = 152.854 \cdot \text{pF}$$

$$R_{\text{LOWER1}} := V_{\text{ref}} \cdot \frac{R_1}{V_o - V_{\text{ref}}} = 1.163 \times 10^3 \Omega$$

Se saca el valor del lazo cerrado para así seguir diseñando el lazo de tensión

Ganancia de corriente en lazo cerrado T_{iLC} :

$$T_{iLC}(\omega) := \frac{1}{R_i} \frac{T_i(\omega)}{1 + T_i(\omega)}$$



Diseño del lazo de tensión

Sabiendo que $G_{vi}(j\omega) = Z(j\omega)$ hallamos el valor de G_{vi} y G_{vc}

Valor de G_{vi}

$$G_{vi}(\omega) := R \cdot \frac{1 + j \cdot R_c \cdot C \cdot \omega}{1 + j \cdot (R_c + R) \cdot C \cdot \omega}$$

Valor de G_{vc}

$$G_{vc}(\omega) := T_{iLC}(\omega) G_{vi}(\omega)$$

Valor de Beta

$$\text{Beta} := 1$$

Por último, se saca el valor de A_v con el método del factor K

1. Diseño del controlador por el método del Factor K:

$$10\% f_s < f_c < 20\% f_s \quad f_c > 10 f_n$$

$$40^\circ < MF_v < 70^\circ$$

$$MG > 10^\circ$$

$$f_s = 50 \text{ kHz} \quad \omega_s := 2\pi f_s \quad \omega_s = 3.142 \times 10^5 \frac{\text{rad}}{\text{s}}$$

$$10\% \cdot f_s = 5 \text{ kHz} < f_{cv} < 20\% \cdot f_s = 10 \text{ kHz}$$

$$f_n := \frac{\omega_n}{2\pi} \quad f_n = 138.527 \text{ Hz} \quad 10 \cdot f_n = 1.385 \text{ kHz} < f_{cv}$$

Valores de diseño $f_{cv} := \frac{f_{ci}}{5} = 1.4 \text{ kHz}$ $MF_v := 70^\circ$

$$\omega_{cv} := 2\pi f_{cv} = 8.796 \frac{\text{krad}}{\text{s}}$$

$$-\arg(G_{vc}(\omega_{cv})) = 51.552^\circ \quad |G_{vc}(\omega_{cv})| = 0.081$$

Compensador tipo 2: $A_v(j\omega) = \frac{\omega_{p0c}}{j \cdot \omega} \cdot \frac{\left(1 + j \cdot \frac{\omega}{\omega_{zc}}\right)}{\left(1 + j \cdot \frac{\omega}{\omega_{pc}}\right)}$

Paso 1) $\arg(G_{vc}(\omega_{cv})) - 90^\circ + AUFA = -180^\circ + MF_v$

$$AUFA = MF_v - \arg(G_{vc}(\omega_{cv})) - 90^\circ$$

$$AUFA_v := (MF_v - \arg(G_{vc}(\omega_{cv})) - 90^\circ) \quad AUFA_v = 31.552^\circ$$

Paso 2) $K_v := \tan\left(45^\circ + \frac{AUFA_v}{2}\right) \quad K_v = 1.788$

$$\omega_{zcv} := \frac{\omega_{cv}}{K_v} \quad \omega_{zcv} = 4.921 \frac{\text{krad}}{\text{s}}$$

$$\omega_{pcv} := K_v \cdot \omega_{cv} \quad \omega_{pcv} = 15.724 \frac{\text{krad}}{\text{s}}$$

$$\sqrt{\frac{\omega_{pcv}}{\omega_{zcv}}} = 1.788$$

Paso 3) Ganancia del regulador ω_{p0c}

+

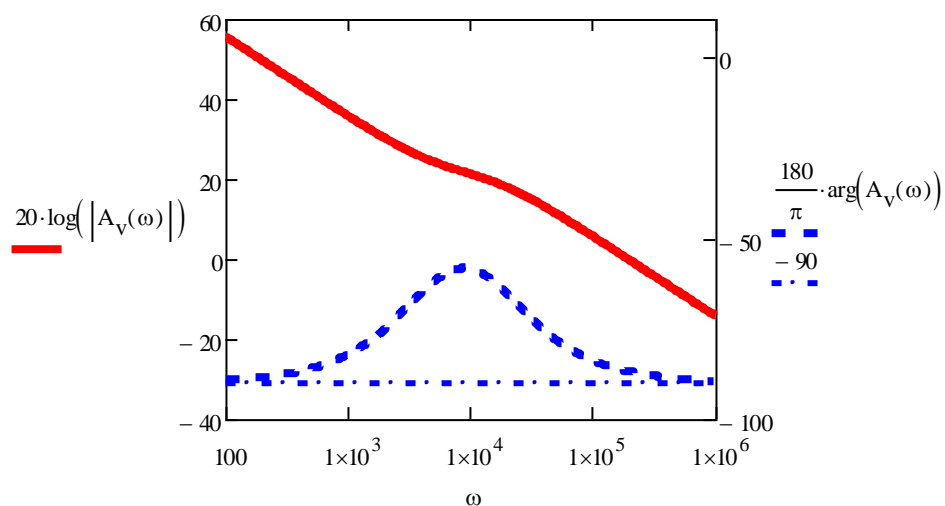
$$T_V(\omega) = G_{vc}(\omega) \cdot A_V(\omega) \cdot \text{beta} \quad |T_V(\omega_{cv})| = 1$$

$$|G_{vc}(\omega_{cv})| \cdot \left| \frac{\omega_{p0cv}}{j \cdot \omega_{cv}} \cdot \frac{\left(1 + j \cdot \frac{\omega_{cv}}{\omega_{zcv}}\right)}{\left(1 + j \cdot \frac{\omega_{cv}}{\omega_{pcv}}\right)} \right| = 1$$

$$\omega_{p0cv} := \frac{\omega_{cv}}{|G_{vc}(\omega_{cv})|} \cdot \frac{\left| \left(1 + j \cdot \frac{\omega_{cv}}{\omega_{pcv}}\right) \right|}{\left| \left(1 + j \cdot \frac{\omega_{cv}}{\omega_{zcv}}\right) \right|}$$

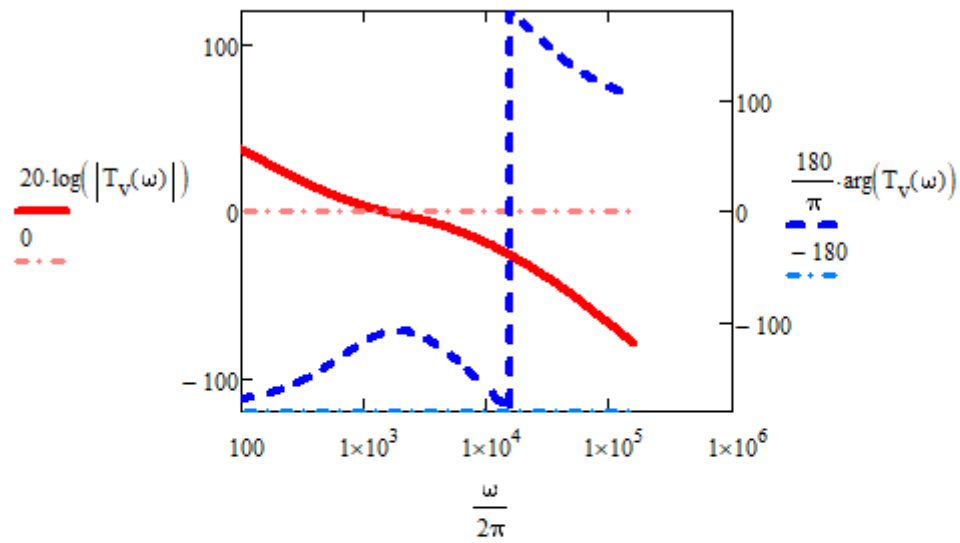
$$\omega_{p0cv} = 60.929 \frac{\text{krad}}{\text{s}}$$

$$A_V(\omega) := \frac{\omega_{p0cv}}{j \cdot \omega} \cdot \frac{\left(1 + j \cdot \frac{\omega}{\omega_{zcv}}\right)}{\left(1 + j \cdot \frac{\omega}{\omega_{pcv}}\right)}$$



$$T_V(\omega) := G_{VC}(\omega) \cdot A_V(\omega) \cdot \text{Beta}$$

+



Dado $\omega_{\text{crossover}} := 1 \frac{\text{krad}}{\text{s}}$

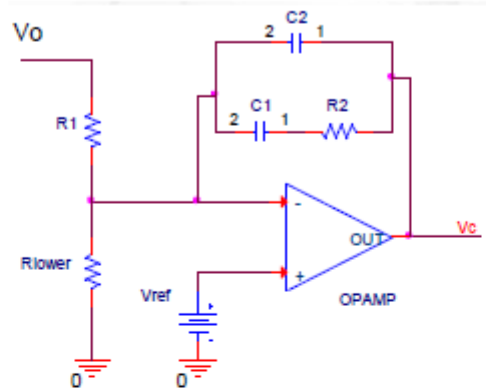
$$|T_V(\omega_{\text{CV}})| = 1$$

$$\omega_{\text{crossover}} := \text{Find}(\omega_{\text{CV}})$$

$$f_{\text{crossover}} := \frac{\omega_{\text{CV}}}{2\pi} = 1.4 \cdot \text{kHz}$$

$$\text{MF}_{\text{crossover}} := \arg(T_V(\omega_{\text{CV}})) + 180^\circ = 70^\circ$$

Regulador tipo 2 con 1 AO:



$$(C2 < C1) \quad R_{1v} := 10k\Omega$$

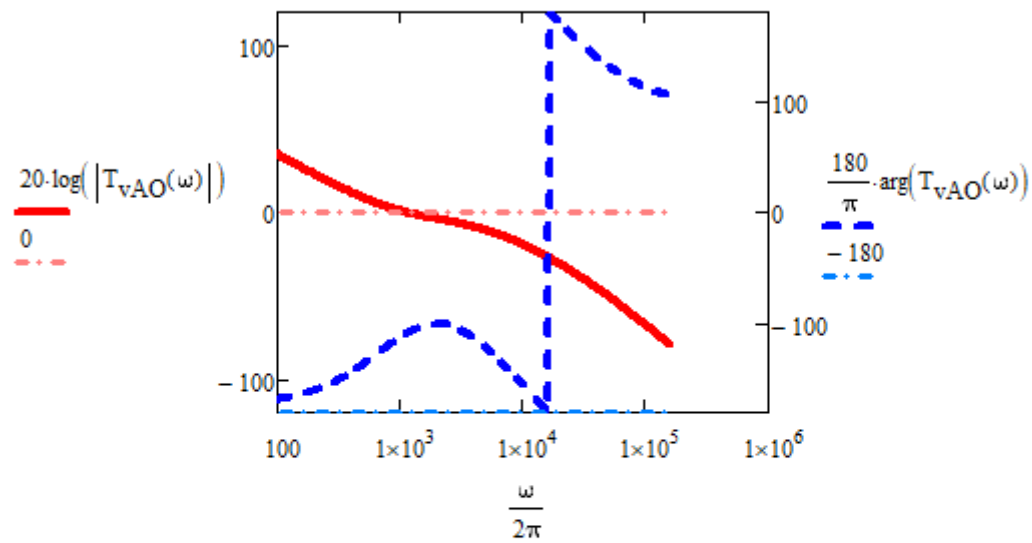
$$\omega_{p0cv} = \frac{1}{R_{1v} \cdot (C_{1v} + C_{2v})} \quad C_{1v} := \frac{1}{R_{1v} \cdot \omega_{p0cv}} = 1.641 \cdot nF$$

$$\omega_{zcv} = \frac{1}{C_{1v} \cdot R_{2v}} \quad R_{2v} := \frac{1}{C_{1v} \cdot (\omega_{zcv})} = 123.814 \cdot k\Omega$$

$$\omega_{pcv} = \frac{(C_{1v} + C_{2v})}{R_{2v} \cdot C_{1v} \cdot C_{2v}} \quad C_{2v} := \frac{C_{1v}}{\omega_{pcv} \cdot R_{2v} \cdot C_{1v}} = 513.653 \cdot pF$$

$$R_{LOWER1} := V_{ref} \cdot \frac{R_{1v}}{V_o - V_{ref}} = 1.163 \times 10^3 \Omega$$

$$T_{vAO}(\omega) := G_{vc}(\omega) \cdot A_{vAO}(\omega) \cdot \text{Beta}$$



Dado $\omega_{\text{crossover}} := 1 \frac{\text{krad}}{\text{s}}$ $|T_{vAO}(\omega_{\text{cv}})| = 1$

$\omega_{\text{crossover}} := \text{Find}(\omega_{\text{cv}})$ $f_{\text{crossover}} := \frac{\omega_{\text{cv}}}{2\pi} = 1.092 \cdot \text{kHz}$

$\text{MF}_{\text{crossover}} := \arg(T_{vAO}(\omega_{\text{cv}})) + 180^\circ = 70.198^\circ$