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1 **Protein removal from waste brines generated during ham**
2 **salting through acidification and centrifugation**

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27 **ABSTRACT**

28 The salting step in food processes implies the production of large quantities
29 of waste brines having high organic load, high conductivity and other pollutants
30 with high oxygen demand. Direct disposal of the residual brine implies
31 salinization of soil and eutrophication of water. Since most of the organic load of
32 the waste brines comes from proteins leaked from the salted product,
33 precipitation of dissolved proteins by acidification and removal by centrifugation
34 is an operation to be used in waste brine cleaning.

35 The aim of this study is optimizing the conditions for carrying out the
36 separation of proteins from waste brines generated in the pork ham salting
37 operation, by studying the influence of pH, centrifugal force and centrifugation
38 time.

39 Models for determining the removal of proteins depending on the pH,
40 centrifugal force and time were obtained. The results showed a high efficacy of
41 the proposed treatment for removing proteins, suggesting that this method
42 could be used for waste brine protein removal.

43

44 **Keywords:** waste brine, protein removal, protein precipitation, ham salting,
45 acidification.

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52 **1. INTRODUCTION**

53 Dry-cured ham is the most important processed meat product in Spain and
54 well known worldwide for its excellent sensory characteristics (Toldrá, 2010).

55 The manufacturing process of dry-cured ham may vary depending on the
56 traditions of each area of production (Toldrá, 2010), however there are some
57 common stages: pre-conditioning of the raw material, curing, salting, post-
58 salting or settlement, drying, aging or maturation and refinement (Barat et al.,
59 2004). The process generates solid and liquid waste (sewage). The dry-salting
60 step is mainly accomplished in plastic or metallic containers that allow the
61 drainage of the generated brine (Barat et al., 2006). The waste brine is
62 composed primarily by water, minerals, blood, proteins and other soluble
63 compounds (Barat et al., 2006). The waste brine exceeds most of the limits
64 permitted by law for direct disposal, and thus it must be treated before disposal.
65 Nevertheless, the treatment of the waste brine can't be done through
66 conventional treatments because of its very high conductivity as a consequence
67 of the high salt content (Barat et al., 2006). Thus it must be managed as a
68 special waste, with an increase in the production cost in addition to the
69 environmental impact.

70 Figure 1 shows the general dry-salting process of Spanish dry-cured ham,
71 where the wastes generated during the process have been highlighted.

72 Figure1.

73 Barat et al. (2006) estimated the production of saturated residual brine
74 during Spanish dry-cured ham production in the year 2003, which was in the

75 range from 29000 to 31700 m³ / year, corresponding to nearly the 10% of the
76 weight of the raw hams.

77 Due to the large variety of stages involved in the overall process, the
78 residual brine has a high content of pollutants. The levels of chlorides, chemical
79 oxygen demand (COD), nitrate and total suspended solids obtained exceeded
80 the limits established by law (L.BOP, 1995) (Barat et al., 2006) for their direct
81 discharge, as they are likely to cause harmful effects to the environmental
82 status of waters. The main problems are related to eutrophication due to the
83 presence of salts such as nitrates and phosphates; unfavourable oxygen
84 balance due to the presence of organic compounds, and soil and water
85 salinization due to the high electrical conductivity, as a consequence of the high
86 concentration of salts (Buckley et al., 1987).

87 Waste brines coming from ham salting are rich in proteins, since the raw
88 ham contains around 20% of proteins, free amino acids, dipeptides, and
89 nucleotides (Warris, 2003). The proteins found in the brine are soluble in
90 concentrated salt solutions and myofibrillar type (Lawrie, 1998) such as actin,
91 tropomyosin, troponin, α -actinin, β -actinin, myosin, protein C, protein M. Most
92 proteins are denatured at relatively low temperatures (<60 °C) and also in acidic
93 conditions, a fact used to produce protein precipitation in the brine to treat
94 (Cheftel, 1989).

95

96 *1.1 Waste brine treatment alternatives*

97 To minimize the environmental impact of waste brines, various techniques
98 have been used such as natural evaporation, forced evaporation, or vacuum
99 evaporation (Diez et al., 2000). One disadvantage of this approach is that the

100 residual solid obtained must be discharged as a special polluting waste, and the
101 high consumption of resources, especially energy.

102 Another alternative technique is the regeneration of the brine for reuse
103 (Barat et al., 2005). This approach consists in the removal of the existing
104 organic nature solutes in the brine (Cuartas et al., 2007) with the consequent
105 recovery of usable substances that currently are discarded (Bes-Pía et al.,
106 2008). Because most of the organic pollution of the brine are proteins, the aim
107 of this work is the study of protein removal by acidic precipitation and
108 centrifugation, as a pre-treatment before filtration stages, allowing the increase
109 in the yield of the filtration processes and delaying the fouling of membranes
110 (Lee et al., 2004).

111

112 **2. MATERIALS AND METHODS.**

113 **2.1 Waste brine**

114 The waste brine used in this study was obtained from a dry-cured ham
115 processing plant. A total of 50 kg of drained brine from salting containers
116 containing hams with a weight ranging from 11 to 12 kg were collected for the
117 study.

118

119 **2.2 Brine characterization analysis**

120 The main physicochemical properties of the waste brine were determined, as
121 well as those of the main parameters related to their polluting load.

122 Those determinations were: chloride, pH, conductivity, total solids, chemical
123 oxygen demand (COD), nitrates and fats.

124 A 1:2000 dilution of the brine was done to determine the chloride content by
125 means of a chloride analyzer (CIBA Corning Mod 926) (Barat et, al., 2006). A
126 dilution of 1:1000 was used for determination sample pH and conductivity, and
127 was measured with a pH meter CRISON® model MM 40 (CRISON Instrument
128 SA, Barcelona, Spain) with a PT100 sensor for temperature compensation.

129 The COD measurement was carried out by photometric determination of the
130 chromate concentration two hours after oxidation with potassium dichromate,
131 sulphuric acid and silver sulphate, using a photometer NANOCOLOR model
132 300D (Macherey-Nagel GmbH & Co. KG) and Test 0-33 (NANOCOLOR COD
133 300 - DIN 34409-H41-1 and in accordance with ISO 15705). Since chloride
134 content higher than 1500 mg/L causes interference in the method, it was
135 necessary to dilute the sample (dilution 1:50 v/v). For the determination of
136 nitrates in the brine a photometer NANOCOLOR®300D(Macherey-
137 Nagel GmbH& Co. KG) was used, with the kit reagents and Test 0-
138 64 (NANOCOLOR® Nitrate 50. DIN 38 405-D9-3). This analysis is based on
139 the photometric determination with 2,6-dimethylphenol, in a mixture of sulfuric
140 /phosphoric acid. A dilution of 1:2000 brine was done to ensure that the sample
141 is within the range where there was no interference, both from chlorine and
142 nitrite. Total solids in the brine were determining by means of the method APHA
143 2540 B and fat content was determined using an automatic unit Soxhlet™ 2055
144 (APHA 5520D, 1998) FOOs, Hillerod, Denmark.

145 Analytical determinations were done in triplicate and the Statgraphics®Plus
146 5.1 software was used to do the statistic of the obtained results.

147

148 **2.3 Acidification and centrifugation experiments**

149 Denaturation of proteins in the residual brine was carried out by means of
150 acidification (Lawrie, 1998). Considering that the isoelectric point of proteins is
151 in the range of pH from 4.5 and 5 (Flores, 1997), the waste brine pH was
152 adjusted from the initial brine pH (6.2 ± 0.01) to 2, 3, 4 and 5 by means of
153 concentrated hydrochloric acid (5N) to avoid dilution and introducing elements
154 that are not naturally present in the brine.

155 Protein removal from the acidified brine was studied by means of
156 centrifugation. Four centrifugation times were used in the study (5, 10, 15 and
157 20 minutes) and 5 centrifugation speeds (1000, 3000, 6000, 10000 and 15000
158 rpm).

159 A factorial design was used (80 combinations) and three replications were
160 done at every combination. At every studied point, 15 milliliters of the acidified
161 brine solution were used.

162 At every point, the collected pellet was weighted, and its moisture
163 determined by drying at 104°C for 24 hours (according to the official standard
164 ISO R-1442). The salt content of the dehydrated pellet was calculated
165 considering that the salt concentration of the retained liquid of the pellet was the
166 same than that of the supernatant.

167 The centrifugation of the brine was done by means of a BL MEDIFRIGER®
168 7001085 centrifuge. The relative acceleration at every centrifugation speed was
169 determined by means of equation 1:

$$170 \quad \text{RCF} = 0.0000118 \cdot r \cdot v^2 \quad (1)$$

171 where:

172 RCF = Relative acceleration in g; $\text{RCF}_{\text{maximum}} = 19584 \text{ g}$

173 r = Radius of rotation ($r = 8.2 \text{ cm}$)

174 v = Spin speed (rpm); Spin speed maximum = 15000 rpm

175 Table 1 shows the equivalence between spin speed and relative
176 acceleration (RCF) calculated by means of equation 1.

177

178 **Table 1**

179

180 **2.4 Protein content in brine**

181 Total protein content in the supernatant was determined by means of the
182 bicinchoninic acid method (microplate) (Laemmli, 1970).

183

184 **2.5 Statistical analysis**

185 The experimental design and statistical analysis of the results was carried
186 out by analysis of variance (ANOVA) using Statgraphics Plus 5.1 software
187 package (Statistical Graphics Corp.), the confidence level chosen was 95%.

188 When the factors were significant, we analyzed the differences between the
189 various levels by contrast analysis using the LSD test. In all cases a
190 significance level of 95% was used.

191

192 **3. RESULTS AND DISCUSSION.**

193 **3.1 Waste brine characterization**

194 The characteristic parameters of the waste brines used in the study can be
195 seen in table 2.

196

197 **Table 2.**

198 The maximum values accepted by Spanish Laws (R.D.606/1993) for direct
199 disposal of effluents are shown in the third column of table 2. As it can be
200 observed, all the analyzed parameters had higher values than the accepted by
201 laws for direct disposal. As stated in the introduction section, the most
202 remarkable fact is the big contamination with organic compounds combined with
203 the very high conductivity of the waste brines.

204 Considering that all the chlorides present in the brine come from the NaCl
205 use for ham salting, it can be confirmed that the residual brine collected from
206 the salting containers is saturated as expected. In addition to the very high salt
207 content of the brine, a significant concentration of nitrates was determined,
208 which indicates the partial leakage of the used nitrates in the nitrification stage.

209

210 **3.2. Influence of pH and time for a constant speed**

211 A model of the experimental precipitate weight fraction obtained (weight of
212 collected precipitate/weight of brine) after centrifugation at every processing
213 condition was obtained by means of a nonlinear regression analysis. The
214 mentioned model was obtained at every centrifugation speed as a function of
215 pH and time.

216 Table 3, shows the obtained models and the regression coefficients at a 95%
217 confidence when using 1000, 3000, 6000, 10000 and 15000 r.p.m.,
218 respectively.

219

220 **Table 3**

221

222 It can be observed a good fitting of the model for all the other experimental
223 conditions except for 1000 r.p.m.. In all cases the obtained precipitate was
224 dependant of pH and centrifugation time. In case of centrifugation at 1000 r.p.m.
225 the bad fitting was due the very low precipitate collected at any pH or
226 centrifugation time.

227 The response surfaces obtained from the fitted models for 3000, 6000, 10000
228 and 15000 rpm can be observed in figure 2.

229

230 **Figure 2.**

231

232 As a general behaviour, it is observed that the collected pellet increased with
233 centrifugation time and with the decrease in pH. As expected, the collected
234 pellet at a pH of 5 was very small, and it would consist in other compounds than
235 denatured proteins. When lower the pH, a higher denaturation of the proteins is
236 expected, and the results confirm this point. Nevertheless, the increase in the
237 collected pellet when pH decreased from 3 to 2 was very small. That difference
238 was even smaller when increasing the centrifugation speed.

239 Figure 3 shows the protein concentration in the supernatant of the residual
240 brine after centrifugation at 6000 rpm and 5 minutes depending on the used pH.
241 A sharp decrease in the protein content is observed when the pH is reduced
242 from 5 to 4, while no significant differences were observed between pH 2 and 3.

243

244 **Figure 3**

245

246 Attending to that result, it seems that a pH of 3 would be the best value to be
247 employed in an industrial treatment, since the protein separation is quite high,
248 as much as at pH 2, with less acid to be added, lower dilution of the waste
249 brine and better preservation of the equipment than with pH 2. It is known that
250 at low pH values the corrosion rate increases exponentially with pH decrease
251 (DOE-HDBK-1015, 1993).

252 When the centrifugation speed increased, the maximum weight fraction of
253 collected pellet was achieved at shorter time. In some experimental conditions
254 (6000 rpm and pH 2), a decrease of the collected pellet can be observed when
255 the centrifugation time increases. It could be explained by the compaction of the
256 pellet, thus reducing the retained brine in the pellet and as a consequence of
257 that the water content. To confirm this hypothesis, the protein content in the
258 supernatant at a pH 3 and the dry pellet were determined.

259 In the previous figure it can be observed that the maximum precipitate
260 fraction obtained at centrifugation speeds of 3000, 6000 rpm at pH values 2 and
261 3, was achieved at 20 and 5 minutes, respectively.

262 Figure 4 shows the total quantity of dry pellet collected after centrifugation
263 and the percentage of removed protein from the supernatant working at pH 3 for
264 5 and 20 minutes. As it can be seen, the maximum protein removal from the
265 brine was close to 90% of the initial content. This value is an asymptotic one
266 and no significant differences were observed depending on the centrifugation
267 time. Attending to this observation, it seems that a further protein cleaning
268 should have to be attained by using filtration techniques.

269 On the other hand, when the quantity of collected dry solid is analyzed, it is
270 confirmed an initial increase in the collected pellet when the centrifugation

271 speed increases simultaneously with the increase in protein removal from the
272 brine. Nevertheless, once a maximum value is achieved, a decrease in the
273 collected dry pellet is observed, even maintaining the quantity of removed
274 proteins, and confirming the mentioned hypothesis that points out towards a
275 compactation of the pellet when the centrifugation speed and time increases,
276 with no increase in the protein removal.

277

278 **Figure 4**

279

280 **3.3 Influence of centrifugation time and speed to pH 3.**

281 As mentioned in the previous section, it was considered the pH 3 as the
282 optimum for protein removal. That's why the study of the influence of
283 centrifugation time and speed was done at that pH value. The wet pellet weight
284 fraction collected at pH 3 (with standard deviation bars) depending on the
285 centrifugation speed and time can be observed in figure 5.

286

287 **Figure 5**

288

289 As a general pattern it can be observed that the collected pellet achieved the
290 maximum values at centrifugation speeds of 6000 and 10000 rpm, with a drastic
291 decrease at a centrifugation rate of 15000 rpm, pointing out to the compaction
292 of the collected pellet occurred with time and increasing centrifugation speed.

293 Figure 6, shows the collected wet pellet at pH 3 at every centrifugation time,
294 depending on the centrifugation speed. It can be clearly seen that no influence of
295 centrifugation time exists at a centrifugation speed of 1000, probably because it

296 was a too small speed for collecting the denatured proteins. On the contrary, a
297 clear influence of centrifugation time was observed form 3000, 6000 and 10000
298 rpm speeds, with a common behaviour, reaching a maximum in the collected
299 pellet at a certain time, and decreasing the collected pellet at further time, due to
300 the compaction action previously mentioned. In case of 15000 rpm, the maximum
301 compaction would be achieved before the 5 minutes, indicating that no benefits
302 would be achieved at longer centrifugation times except for a reduction of the
303 retained brine in the precipitate.

304

305 **Figure 6**

306

307 It can be seen that for the same centrifugation time, the maximum collected
308 pellet is achieved at lower centrifugation speed than the maximum one, giving
309 support to the compaction of the brine, which was independent of time for the
310 maximum speed.

311

312 **4. Conclusions.**

313 The use of acidification of residual brine coming from pile salting during
314 Spanish dry-cured ham production is an effective technique for protein removal.

315 The best pH value to be used in an industrial process seems to be 3,
316 because a large quantity of proteins is removed while the pH is no very low. The
317 industrial processing should have to be followed by the neutralization of the
318 supernatant.

319 The obtained results indicate that almost 90% of the proteins from the brine
320 can be removed by acidification followed by centrifugation. A further protein

321 removal from the brine should have to be achieved by using filtrating
322 techniques, which efficiency could be highly improved as a consequence of the
323 previous treatment through acidification and centrifugation. Further studies are
324 needed to confirm this aspect.

325

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329 C02).

330

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395 **Figure index**

396 Figure1. General process for the preparation of Spanish dry-cured ham
397 (adapted from Toldrá and Aristoy, 2010).

398 Figure 2. Evolution of the wet pellet weight fraction (x^{pp} g/g) as a function of pH
399 and centrifugation time (t) for 3000 (a), 6000(b), 10000(c) and 15000 rpm (d)

400 Figure 3. Protein concentration in the supernatant of acidified brine after
401 centrifugation at 6000 rpm for 5 minutes.

402 Figure 4. Percentage of protein removal from the supernatant and collected dry
403 pellet different centrifugation speeds at 5 (a) and 20 (b) minutes.

404 Figure 5. Evolution of the wet pellet weight fraction (g/g) (with standard
405 deviation bars) at different centrifugation time and speed at pH 3.

406 Figure 6. Evolution of the pellet weight fraction (g/g) colleted for constant
407 centrifugation times at different centrifugation speed and pH 3.

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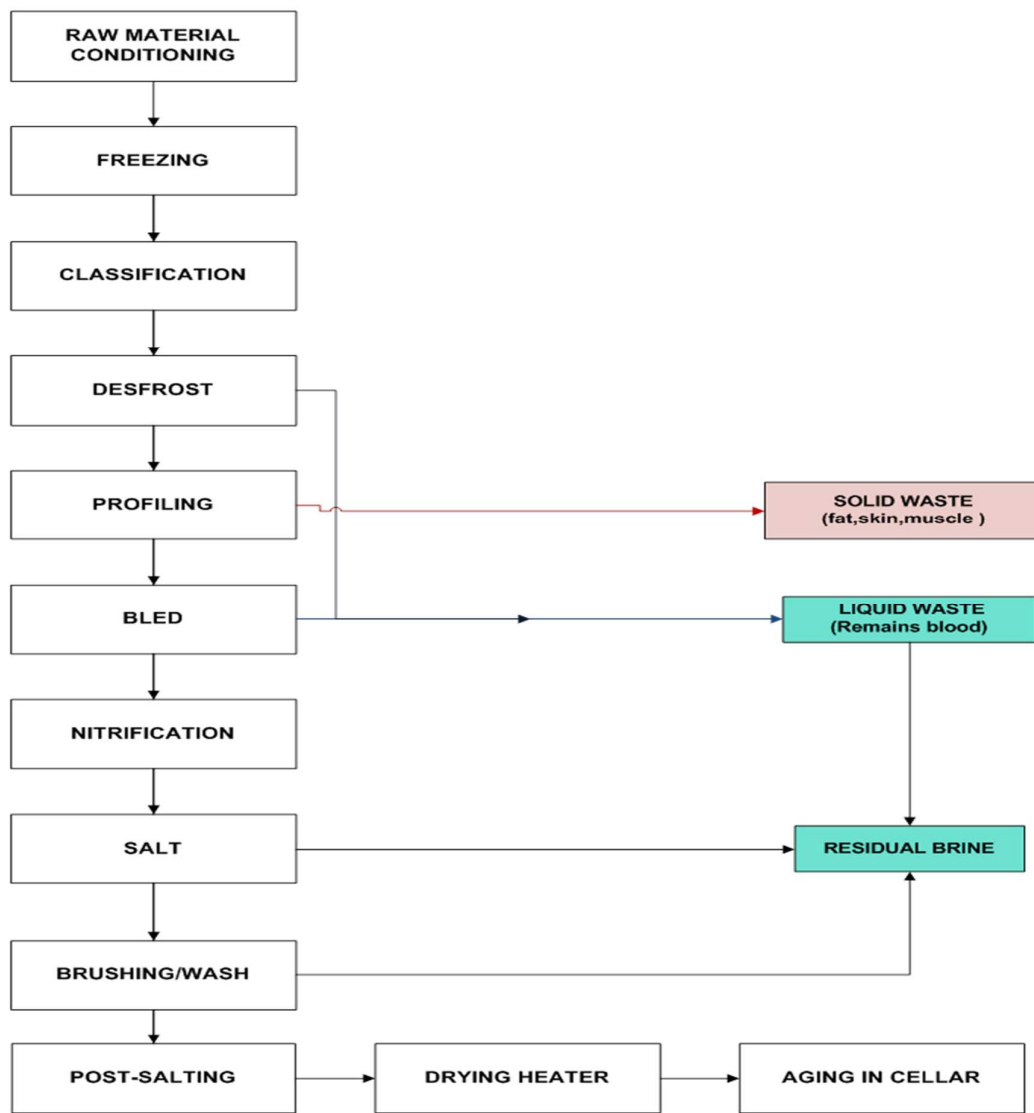
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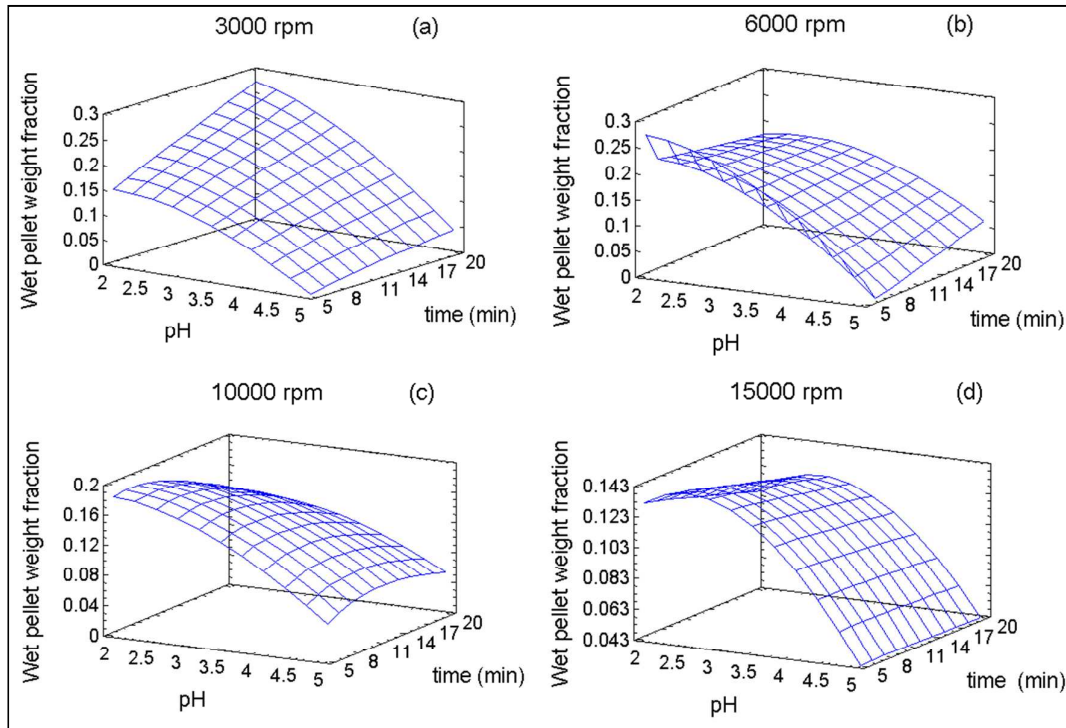
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430 **Figure 2**



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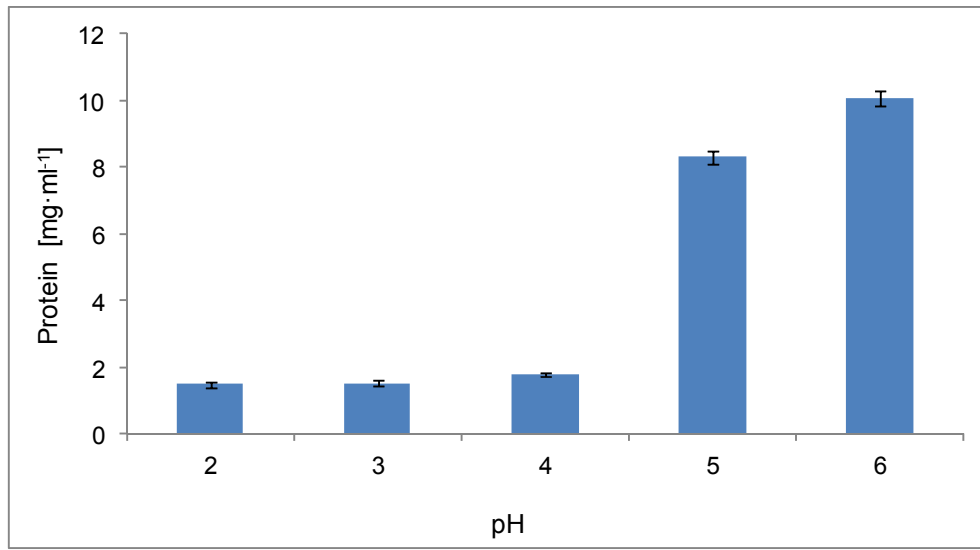
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441 **Figure 3**

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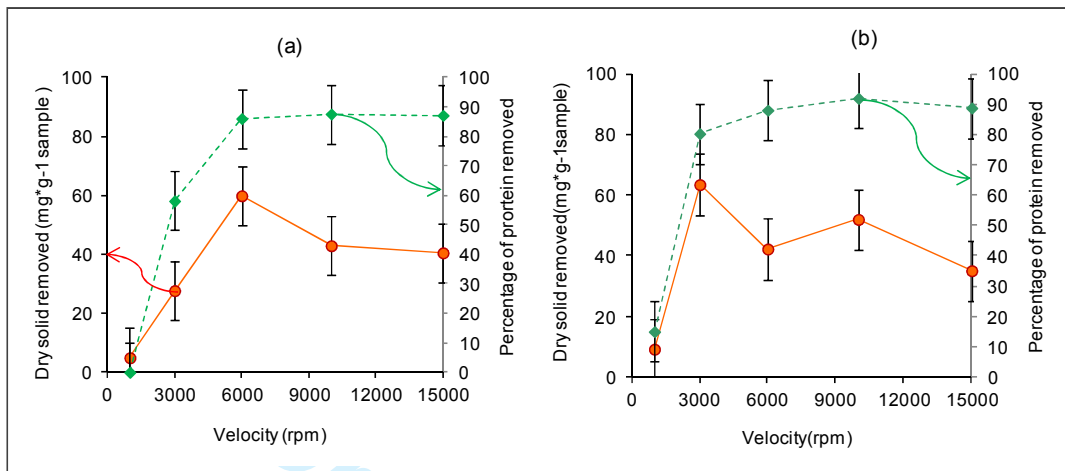
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460 **Figure 4.**



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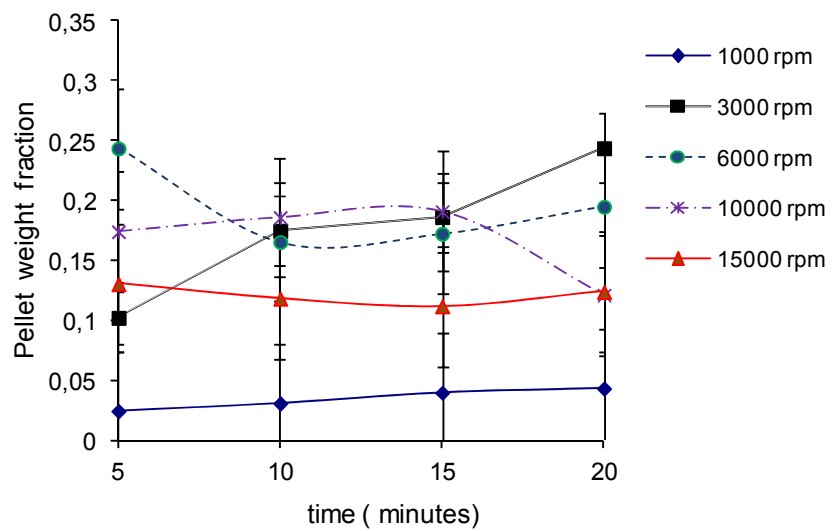
479 **Figure 5**

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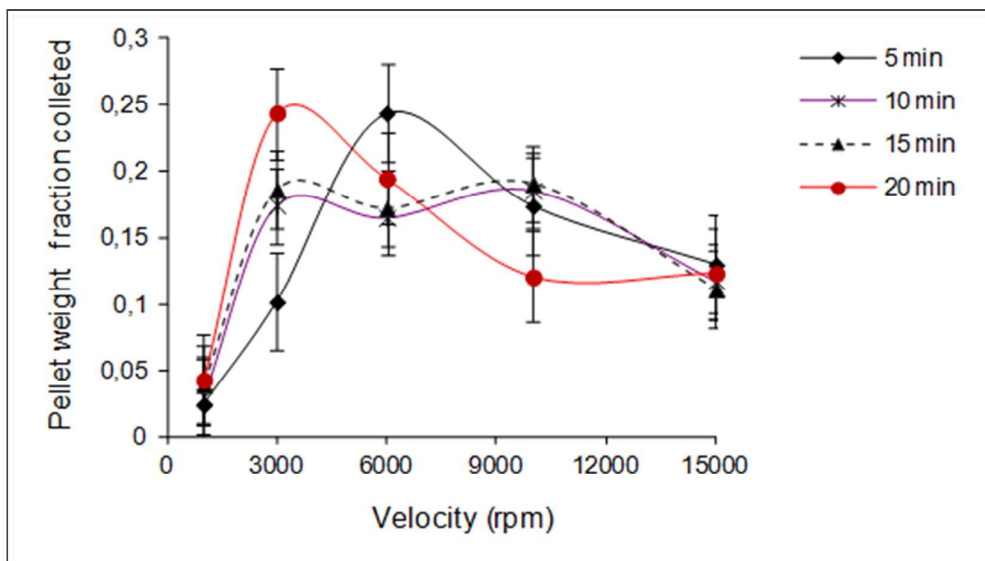
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497 **Figure 6**

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515 Index table

516 Table1. Equivalence of spin speed used in the experiments and relative
517 acceleration (g)

518 Table 2. Physicochemical properties of the waste brine used in the study.

519 Table 3. The models and the regression coefficients at different velocities

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Peer Review

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541 **Table 1**

Spin speed (rpm)	1000	3000	6000	10000	15000
Relative acceleration (g)	92	825	3300	9168	20627

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562 **Table 2**

Analysis	Values of analysed waste brine	Maximum accepted values for disposal from Spanish Laws (R.D. 606/1993)	Analytical method
pH	6.2 ± 0.01	5.5 - 9.5	pH meter CRISON MM40
Conductivity [mS/cm]	582 ± 7	5000	pH meter CRISON MM40
Chloride [g/L]	175.5 ± 0.5	2	Chloride Analyzer SHERWOD 926
COD [mg/L]	25867 ± 2013	500	Photometer Nanocolor Test DQO 300
Solids [mg/L]	11650 ± 240	300	Method 2540-B
Nitrates [mg/L]	470 ± 1.2	20	Photometer Nanocolor Test NO ₃ -50
Fat [mg/L]	381 ± 20	40	Soxtec System 2055 Tecator

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571 **Table 3**

rpm	Model*	Regression coefficient (R ²)
1000	$x^{pp} = 28.14 \cdot pH^{0.56} - 0.24 \cdot t^{-0.26} + 7.62 \cdot 10^{-4} \cdot pH \cdot t - 0.11 \cdot pH - 4.09 \cdot 10^{-3} \cdot t$	7.2
3000	$x^{pp} = 0.63 \cdot pH^{0.64} - 0.29 \cdot t^{-0.06} - 1.89 \cdot 10^{-3} \cdot pH \cdot t - 0.30 \cdot pH + 0.01071 \cdot t$	89.9
6000	$x^{pp} = 2.64 \cdot pH^{0.95} + 3.29 \cdot 10^9 \cdot t^{-15.44} + 25,48 \cdot pH \cdot t - 2.43 \cdot pH - 7.83 \cdot 10^{-3} \cdot t$	88.8
10000	$x^{pp} = 1.45 \cdot pH^{0.94} + 0.18 \cdot t^{0.96} + 1.51 \cdot 10^{-3} \cdot pH \cdot t - 1.31 \cdot pH - 0.16 \cdot t$	78.2
15000	$x^{pp} = 1.01 \cdot pH^{0.832} - 0.22 \cdot t^{-0.004} + 5.50 \cdot 10^{-4} \cdot pH \cdot t - 0.72 \cdot pH - 0.00287 \cdot t$	91.0

572 * (x^{pp} = wet pellet weight fraction – g/g –, t = time (min))

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